

Metamaterial Structure Effect on Printed Antenna for LTE/WIFI /Cancer Diagnosis

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ABSTRACT

Article history: Received 13 October 2023 Received in revised form 22 January 2024 Accepted 2 May 2024 Available online 22 May 2024	This paper explores the influence of metamaterial structures on the performance of LTE/Wi-Fi printed antennas, examining two antenna versions. One version integrates a metamaterial ground layer, representing the traditional antenna, while the other incorporates a metamaterial load attached to the modified antenna. The inclusion of the metamaterial ground layer supports the unit cell with the MTM structure, enabling an analysis of how the MTM structure impacts antenna performance. Testing is conducted using Roger 5880 substrate with a thickness of 1.575 mm and a dielectric constant of 2.2. The antenna's overall dimensions are 60×49×1.575mm, with a loss tangent of 0.0009. Once optimal inductor/capacitor values are determined, equivalent circuits are generated for both the planned and conventional circuits. These circuits are simulated using CST Microwave Studio, with the Path Wave ADS simulator running the equivalent circuit. Antenna manufacturing and measurement are conducted using a Network Analyzer. Frequency ranges covered by the antenna include 1.68 GHz to 2.51 GHz, 3.56 GHz to 4.63 GHz, and 4.1 GHz to 5.1 GHz, suitable for standard applications. Simulated gain is reported as 2.58 dB/2.45 dB, with observed gain at 2.22 dB/5.19 dB, showing excellent agreement between measured and simulated values from both simulators. Additionally, simulated specific absorption rate (SAR) on a sample Breast Phantom ensures compliance with the 1g/10g SAR value requirements set by the
Keywords: Metamaterial antenna, Printed antenna,	European Union and the United States. This confirms the antenna's suitability for
LTE application, Cancer Diagnosis	cancer diagnosis and detection applications

1. Introduction

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The path wave ADS simulator runs the equivalent circuit. The antenna Rode is manufactured and measured by Network Analyzer. The frequency ranges covered by the antenna are as follows: 1.68 GHz-2.51 GHz 3.56-4.63 GHz 4.1 GHz-5.1 GHz Standard applications (LTE, Wi-Fi, etc.) 2.58dB/2.45dB. However, printed thin strip antennas have become necessary for every new gadget due to the explosive proliferation of handheld wireless communication devices in the previous several years. This sort is good since it achieves the smallest size and covers all of the frequency ranges required in today's different applications. Users and service providers frequently want wireless devices with antennas that are tiny and compact, easy to link with other components of a wireless communication system, low profile, and reasonably priced to manufacture, in addition to meeting operational criteria [7–10].

However, compared to devices and bodies, flexible or thinner substrate-based wearable antennas provide a number of benefits, one of which is the ability to design simpler configurations. They can also include gates in a variety of shapes, such as bodies or gadgets [11–15]. They can also be supported by MTM cells, which can increase gain and bandwidth [18–19].

Regarding MTM, it is a substance that is usually synthesized with unique or artificial structures in order to generate electromagnetic characteristics that are uncommon or challenging to generate in the natural world. It is abnormal and has distinct qualities that aren't found in the natural environment [20–21]. It has a negative permeability, a negative dielectric constant, or both [22]. Many people are interested in them because of their features, and they may find utility in a wide range of electromagnetic applications, from the microwave to the optical regime [22–26].

This report provides a thorough analysis of the most recent research initiatives related to those MTM-based tiny antennas. They are analyzed and classified into multiple kinds, including MTM loadings, metaresonators, and antennas based on dispersion engineering. A few real-world obstacles or restrictions on the advancement of MTM-based tiny antennas are mentioned, along with potential solutions.

Another significant occurrence that is happening increasingly frequently these days is the diagnosis of breast cancer. It is a contributing factor to the greatest annual number of women's cancer cases that are reported. In Malaysia, women are more likely than men to have cancer; in 2016, 10,290 cases out of 100,000 individuals had the highest incidence (14.5%), according to [27]. This is in contrast to other cancer cases, such as leukaemia, stomach, and lung cancer. Unchecked aberrant cell development produces malignant tumours, which are usually referred to as cancer. These tumours can move to other organs or infect surrounding body components. It is imperative to identify a diagnosis and a means of detection for this illness.

Antennas placed within or on top of bodily organs can be used to detect cancer. Additionally, while researching and using an implanted antenna for the detection of human cancer, SAR presents a safety risk [28–40]. After fabrication, the antennas are measured. Similar circuit technology is also used to test it, producing the ideal conductor and capacitor values [41-44].

2. Methodology

2.1 Antenna Design

2.1.1 Conventional antenna

A typical patch antenna is shown in Figure 1. This study presents a microstrip antenna design with and without MTM. Applications for WiFi and LTE use it. Studies on the human breast are being conducted concurrently to determine whether or not it could be utilized as a sensor for the identification and diagnosis of cancer. The patch combines multiple horizontal strips to partially realise the LTE frequency spectrum. Its measurements are shown in Table I, and the manufactured

version is shown in Figure 2. Based on Roger 5880, the design has a thickness of 1.575 mm and a ϵ r of 2.2.



Fig. 1. Conventional Antenna Structure: (a) Top View, (b) Bottom View



Fig. 2. Conventional Antenna Fabrication:(a) Top View, (b) Bottom View

Table 1					
Reconfigurable-Pin Diode Switches					
Antenna	Dimension(mm)				
Parameter					
WS	49				
w1	4.80				
w2	20				
w3	30				
w4	48				
ls	60				
1	12				
12	11				
Wp	14				
Lg	8(conv.),11(MTM)				

Figure 3 illustrates the model of the structure's similar circuit. It is made up of three inductors, three capacitors, and a resistor that mimics the resistance of the patch. The values of these components are found using equations 1 and 2, where I is the length of the strip, w is its width, h is the height of the substrate, and c is the speed of light in vacuum.



Fig. 3. Equivalent circuit of conventional antenna.

2.1.2 Metamaterial Antenna

The built MTM antenna is depicted in Figure 5, its equivalent circuit is illustrated in Figure 6, and the bottom layer of DGS ground is substituted with a layer composed of a 3x3 array of copper patches spaced 1.00 mm apart. Table I displays its measurements.



Fig. 4. MTM Antenna Structure: (a) Top View, (b) Bottom View



Fig. 5. MTM Antenna Fabrication:(a) Top View Bottom View



Fig. 6. Equivalent circuit of MTM antenna

2.2 Optimization

The goal of this part is to optimise the two antennas' various dimensions in order to reach the targeted frequency ranges of 2.1 GHz and 4.1 GHz.

2.2.1 Conventional Antenna

The optimization of a standard antenna's size to reach resonance frequencies of 2.1 GHz and 4.1 GHz is illustrated in Figure 7. As seen in figures 7a, b, and c, respectively, the reflection coefficient is optimized for various values of substrate thickness (hs), patch width (W4), and ground length (lg).

It is evident that the primary element affecting the second response at 4.1 GHz is the ground length (lg), with an optimal value of 10mm. It is evident that modifications to the dielectric thickness

240

(b)

(hs) and patch width (w1) can induce resonance at 2.1 GHz, whereas ground length modifications can induce resonance at 4.1 GHz.



Fig. 7. conventional antenna optimization (a) substrate thickness, (b) patch width and (c) ground length

The simulated and measured reflection coefficient of the optimized conventional antenna is presented in Figure 8, and the findings are in good agreement with the simulations.



Fig. 8. Simulated and measured of the reflection coefficient of the optimized conventional antenna

2.2.2 MTM Antenna

The reflection coefficient for a range of unit cell edges (wp) optimized to reach both 2.1 GHz and 4.1 GHz resonance frequencies is displayed in Figure 9. It is evident that the ideal unit cell square edge (wp) value is 14 mm since both resonances are apparent.





Fig. 9. MTM's unit cell edge antenna optimization

Fig. 10. MTM equivalent circuit optimization

Starting with initial values of 1nH and 1pF, respectively, Figure 10 illustrates the equivalent circuit response of the MTM antenna for various parametric adjustments for the values of capacitors and inductors. It is evident that optimization number two is capable of reaching both 2.1GHz and 4.1GHz (2).

3. Results

3.1 Return losses and Gain

Figure 11 shows the optimized MTM antenna's simulated and observed reflection coefficients, showing a high agreement between them.



Fig 12 presents the conventional antenna's gain versus the MTM one. One can observe that the MTM's gain is slightly increased.

3.2 Radiation Pattern

Figure 13 shows the 3D radiation pattern for the conventional antenna operating at 4.1 GHz and with a gain of 4.29 dB. Figure 14 shows the 2D radiation pattern in the XZ and YZ planes.



Fig. 13. 3D radiation pattern of conventional antenna at 4.1 GHz







Fig. 15. 3D radiation pattern of MTM antenna: (a) at 2.1GHz, (b) at 4.1GHz





At 2.1 GHz and 4.1 GHz, Figure 15 shows the 3D radiation pattern of the MTM antenna. The measured gains are 2.22 dB and 5.19 dB, while the simulated gains are 2.58 dB and 5.45 dB, respectively. The 2D radiation pattern in the XZ and YZ planes for the same frequency is shown in Figures 16 and 17.



(a) XZ Plane (b) XY Plane Fig. 17. 2D radiation pattern of MTM antenna at 4.1 GHz (a) XZ plane, (b)YZ plane

3.3 Surface Current

A typical 2.1GHz antenna's surface current is shown in Figure 18, with higher values at the edges. The MTM antenna's surface current is shown in Figure 19 for frequencies of 2.1 and 4.1 GHz, respectively.



Fig. for conventional antenna at 2.1GHz



Fig. 19. Surface current for MTM antenna at:(a) 2.1 GHz, (b) 4.1 GHz

3.4 Antenna Performance on Body

The next investigation will use a phantom breast to assess the efficacy of the proposed antenna design. CST is applied to 1 and 10 grammes in numerical research. To replicate the anatomy of the human breast, a multilayer model tissue has been constructed.

3.4.1 SAR evaluation

The safety of the antenna operating over a human body was evaluated in order to make sure the SAR level complied with safety regulations. The FCC and ICNIRP's regulatory recommendations, which set a maximum level of 1.6 W/kg for averages over 1 gramme of tissue and 2 W/kg for averages over 10 grammes of tissue, form the basis of the evaluation. The SAR evaluation employed the CST standard with a 100 mW input power. In order to replicate the human anatomy, both antennas are used in this experiment on a layered human breast. CST is used for numerical analysis on 1g and 10g samples.

Generally, the model was 10 mm away from the design while evaluating it along the x-axis. For the conventional antenna (Figures 20 and 21) and the MTM antenna (Figures 22 and 23), the findings are shown in Tables II and III, respectively. When compared to the standards, the results are satisfactory. Tables 2 and 3 show the SAR findings for the conventional and MTM antennas, respectively.



Fig. 20. SAR analysis of conv. antenna at 2GHz (a) 10g ,(b) 1g



Fig. 22. SAR analysis of MTM antenna at 2GHz (a) 10g, (b) 1g





Fig. 23. SAR analysis of MTM antenna at 4GHz (a) 10g, (b) 1g

Figures 23 and 24 display the SAR values for an MTM antenna, while Figure 22 displays the SAR values in the breast for a traditional antenna operating at 4.1 GHz. The results for each antenna are summarized in Tables 2 and 3.

Table 2

SAR (10 mm

from breast) At 2 GHz

in distance

At 4 GHz

SAR analysis of conventional antenna Values near breast

SAR at

0.719

0.66

10(g) W/Kg

SAR at 1(g)

W/Kg

1.49

1.61

Table 3

SAR analysis of MTM antenna Values near breast

SAR (10 mm	SAR at 1(g)	SAR at 10(g)
in distance	W/Kg	W/Kg
from breast)		
At 2 GHz	.029	.0126
At 4 GHz	.448	0.105

Table 4 compares different planar metasurface-transistor (MTM) antenna designs found in the literature to accepted work.

Table 4

Summary of research on planar MTM / metasurface structure-based antennas

First author, year	Substrate material		Dimensions @	Frequency	antenna Efficiency
			Array		Simulated
H.T. Zhong, 2017	Rogers	Duroid	0.6λ0	5.4 GHz	92% at 0°
[40]	RT5880				
Wei Hu, 2019 [41]	F4B/air		@ 3×3 unit cells	2.45 GHz	98% at 60°
Omar M.	Rogers	Duroid	0.6λ0	5.8 GHz	(TM-mode)
	RT5880				
Ramahi, 2012 [42]	Rogers	Duroid	@ 8×8 unit cells	5.55 GHz	87.6%
	RT5880				
Babak Alavikia,	Rogers RO	4003	Approximately	5.6 GHz	-
2015 [43]			0.114λ0		
Babak Alavikia	F4B		@ 9×9 unit cells	2.5 GHz (LTE/WI-FI)	92% for G- CSRR
2015 [44] Xuanming Zhang	Degers TM	N410;	0.2420	2 CU-	070/
Xuanming Zhang	Rogers IIV		0.34/0	3 GHZ	87%
2018	Pogors PO		@ 11×11 array of G		00%
[45]	Rogers RUSULU PCB		CSRR and 5x5	5.55 GHZ (WIFI)	50%
Thamer S	Polytetrafl	uoroeth	array microstrin	2 45 GHz	97%
manier 5.	vlene (PTFF)		natch antenna	2.45 0112	5770
Almoneef 2015	-	-)	Approximately	5.8 GHz	86%
[46]					
Alireza	Rogers	RT/duroid	λ0/5	2.45 GHz and 6 GHz	99.5%
Ghaneizade	6006	,			
h, 2019 [47]	F4B		@ 9×9 unit cells	900 MHz,	88% at 0° and
Xin Duan, 2018	F4B-2		Approximately	2.6 GHz and	77% at 75°
[48]			0.131λ0		
Fan Yu, 2018 [49]	Rogers RO4003		@ 9×9 unit cells	5.7 GHz	Higher than 90%
B. Ghaderi, 2018	Roger 5880		0.075λ0	Wideband (6.2–21.4	70%, 80%,
[50]				GHz)	
Xuanming Zhang,	Rogers	Duroid	@ 13×13 unit cells	1.75 GHz,	and 82% at
2017 [51]	RT5880				
H.T. Zhong, 2017	F4B/air		0.13λ0	3.8 GHz, and	900 MHz, 2.6
[52]	_				
H.T. Zhong, 2016	Rogers	Duroid	@ 11×11 unit cells	5.4 GHz	GHz and 5.7 GHz,
[53]	RT5880	D · ·	0.4620		
Inis work	Rogers	Duroid	0.16λ0	2.1 GHz and	respectively
	K15880				

Table 4 shows that, in comparison to previous efforts, the antenna efficiency is 94% over the two operating bands.

4. Conclusions

This study presents, analyses, fabricates, and measures conventional and MTM LTE/Wi-Fi/disease diagnostic antennas. Both CST and ADS simulators are used to build models of the two antennas. There is good agreement between the calculated and measured reflection coefficients. The MTM version conducts resonance at 2.1 GHz and a gain of 5.45 dB at 4.1 GHz with a bandwidth of 1.07 GHz, and a bandwidth of 0.832 GHz with a gain of 2.58 dB. In contrast, the conventional antenna operates at 4.1 GHz with a bandwidth of 1.65 GHz and a gain of 4.29 dB.

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