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# Effect of Moisture on Static and Fatigue Strength of Rubberwood/ Recycled Polypropylene Composites

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### ABSTRACT

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While the field of plant fibre composites is experiencing rapid growth in research and development, there are still essential considerations that must be addressed before these materials can be adopted by industries for structural applications. One of the primary concerns revolves around their durability. This study aims to assess how moisture affects the static and fatigue behaviour of a rubberwood/recycled polypropylene composite. The specimens were exposed to a humid environment at 23 °C in water immersion for 30 days. Quasi-static and tension-tension fatigue tests were carried out. Results show that exposure to moisture has caused a significant decrease in their initial quasi-static strength and stiffness. The fatigue strength, on the other hand, has been enhanced. The fatigue strength coefficient decreases by more than half after ageing, suggesting a less pronounced decrease in maximum stress as the number of cycles increases. The fatigue hysteresis loop and evolution of the secant modulus of non-aged composite show more pronounced fatigue damage when compared to the aged composite.

## 1. Introduction

Research and advancements in plant fibre composites are experiencing rapid growth, especially in sectors like automotive and plastics industries, construction, and end-use industries due to their affordability, versatility in design, and favourable environmental characteristics [1-4]. Wood polymer composites (WPC) primarily consist of wood flour, frequently sourced from timber industry waste materials. Wood flours are blended with polymeric materials using a compounding process to create a robust and stable composite system that offers a promising alternative to traditional timber. The thermoplastic can be sourced from post-consumer products [5] as part of an effort to mitigate plastic waste in the environment. As interest in utilizing cellulosic fibre composites across a broad spectrum of applications grows, certain applications may subject these composites to cyclic or alternating loads

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during their operational lifespan. Structural materials frequently encounter fatigue failures even before reaching their tensile strength [6-10]. The mechanical degradation of the materials under cyclic loading occurs cumulatively and differs from static loading. Thus, the application of WPC composites in structural materials presents significant challenges due to their fatigue reliability under varying load conditions.

Wood fibre as such rubberwood used in this study is a lignocellulosic material and thus can be also vulnerable to moisture absorption, particularly in humid environments or when immersed in water [11]. Moisture absorption can have a substantial influence on the performance of organic materials, resulting in changes in their chemical and physical attributes, which in turn can have an impact on their mechanical and thermal properties [12,13]. Although the impact of moisture has been thoroughly examined under static conditions [14-16], the information and understanding of its combined effects with moisture under dynamic loading onto WPC particularly rubberwood remains relatively limited. Therefore, considering factors like moisture in conjunction with fatigue loading is imperative to comprehensively assess and model the effects of service loads and conditions on prospective materials, ensuring the integrity of fatigue design for safety. In this study, we aim to explore how moisture affects the fatigue characteristics of rubberwood/recycled polypropylene composite to understand the complex behaviour of the materials.

## **2. Methodology**

### *2.1 Composite Material and Specimen Preparation*

The materials used in this study are rubberwood / recycle PP (rPP) pellets with the optimised composition of rPP (50.3 wt.%), rubberwood flour (37.5%), calcium carbonate (7 wt.%), MAPP (3.9 wt.%), UV (0.2 wt.%), lubricant (1 wt.%). The manufacturing process of the pellet and specimens is fully detailed in our previous study [8,9]. The rubberwood/ recycled composite plate was cut into dumbbell-shaped for tensile test (ASTM D638).

### *2.2 Conditioning and Hydrothermal Ageing*

Prior to any test, the sample was pre-conditioned at 50% RH at a laboratory temperature of 23°C and labelled as unaged condition. A portion of the specimens was subsequently submerged in distilled water at room temperature (23°C) for a maximum duration of 30 days. The samples were intermittently removed and weighed using a precision electronic balance accurate to 0.01 g. Finally, it was oven-dried until their mass equilibrium was reached. The specimen then is conditioned again at 50% RH at 23 °C prior to the test, the sample is known as the water-aged state.

### *2.2 Mechanical Testing*

Servopulser Shimadzu fatigue machine (Japan) with a capacity of 20 kN load cell was used to assess the static and fatigue performance of the rubberwood-based composite for both untreated and water-exposed samples. For the determination of the ultimate tensile strength of both untreated and treated specimens, a quasi-static test was conducted at a rate of 2 mm/min. Subsequently, fatigue testing was conducted using a tension-tension stress control mode, ranging from 40% to 80% of the ultimate tensile strength of the composite material. During the fatigue tests, a stress ratio (R) of 0.1 and a frequency of 4 Hz were maintained. The tests were continued until fracture occurred or, in cases where failure did not transpire, run-outs were designated after 1.5 million loading cycles.

Five sets of samples are repeated for each test level. All test was performed in air at ambient temperature as described in our previous study [8].

### 3. Results

#### 3.1 Quasi-Static Tensile Testing

The quasi-static properties for unaged and water-aged composites. For the unaged, the mean value for the ultimate tensile strength (UTS), elastic modulus and strain at failure, respectively 26.33 MPa, 1.69 GPa  $\pm$  0.16 and 1.59 %, similar to those reported by Srivabut *et al.*, [5]. Exposure of the composite to moisture has induced a significant decrease in their initial ultimate tensile strength and stiffness approximately - 53% and 56% respectively as reported in our preliminary study [17]. The degradation in the rubberwood/recycled PP composites is possibly due to the plasticizing effect of water as well as damage due to ageing [10,13,17]. In terms of the strain observed at the point of failure, a noticeable 18% increase was observed in the water-aged specimen. This change is consistent with the notion that water has a plasticizing effect on the amorphous carbohydrates present in the rubberwood fibres [18].

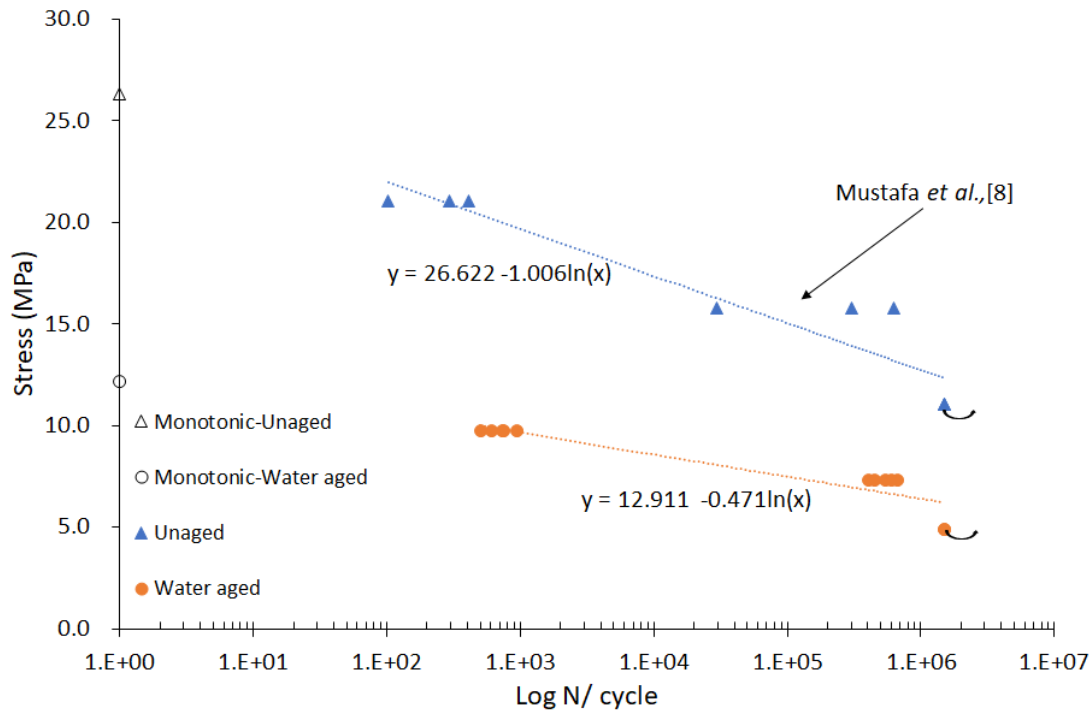
#### 3.2 Fatigue Testing

The stress and number of cycle (S-N) curves, from the tensile-tensile fatigue tests for both unaged and water-aged composite, are shown in Figure 1. Results show a gradual reduction in fatigue strength as the number of fatigue cycles increases for both conditions. The relationship between fatigue strength and the number of cycles follows the logarithmic equation (Eq.1).

$$S_{\max} = \alpha - \beta \ln (N) \quad (1)$$

where N represent the number of cycles at failure,  $S_{\max}$  is the ultimate tensile stress,  $\alpha$  is the ultimate strength for a single cycle and  $\beta$  is the fatigue strength coefficient of the material.

The  $\beta$  parameter for the unaged specimens is equal to 1.0. However, upon examination of the aged specimens, a noticeable decrease in maximum stress within the low-cycle range is apparent when compared to their unaged counterparts. To illustrate, after 1000 cycles, the maximum stress following ageing measures is approximately 9.6 MPa, a significant reduction from the 21.6 MPa observed before ageing. Additionally, it's noteworthy that at higher fatigue cycle counts, the aged specimens exhibit a notably prolonged fatigue life compared to the unaged specimens. At 60% UTS, the average fatigue life of the unaged and aged composite is 321,000 and 536,000 cycles. From these findings, we can conclude that hydrothermal ageing, while causing a decrease in static rigidity and strength, actually enhances fatigue resistance as shown by the reduced value of the  $\beta$  parameter, which drops to 0.47. This phenomenon is likely attributed to improved damage tolerance resulting from fibre swelling and potentially led to improvement of the matrix/fibre interface [19].



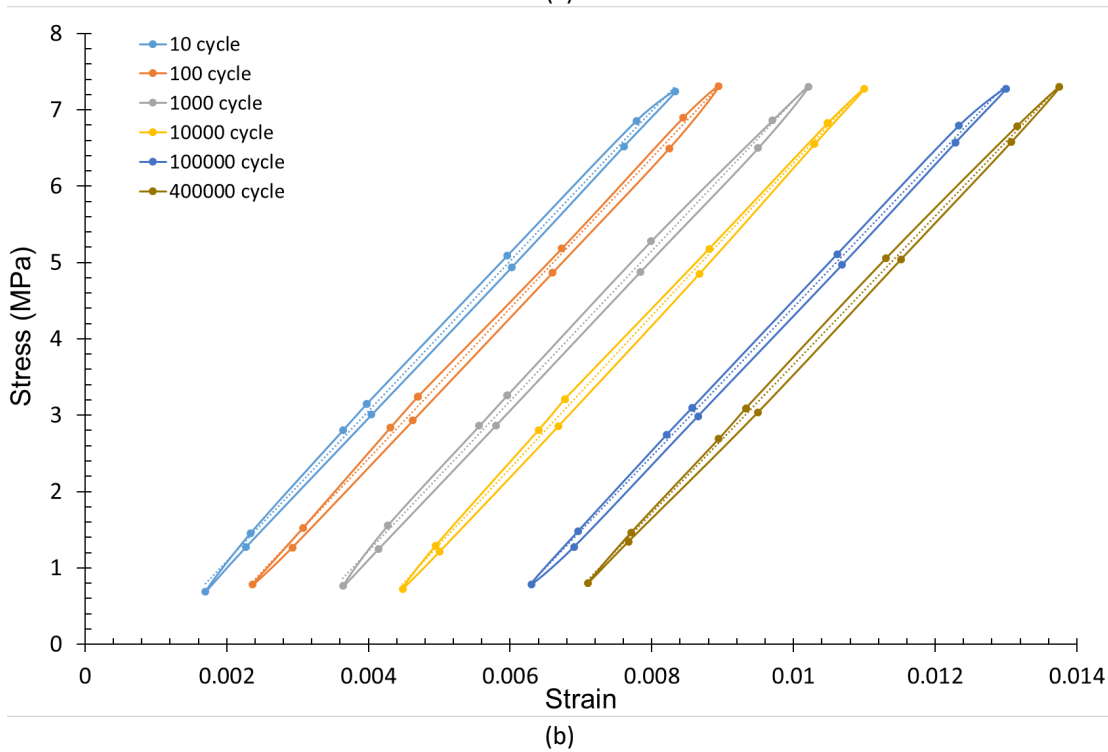
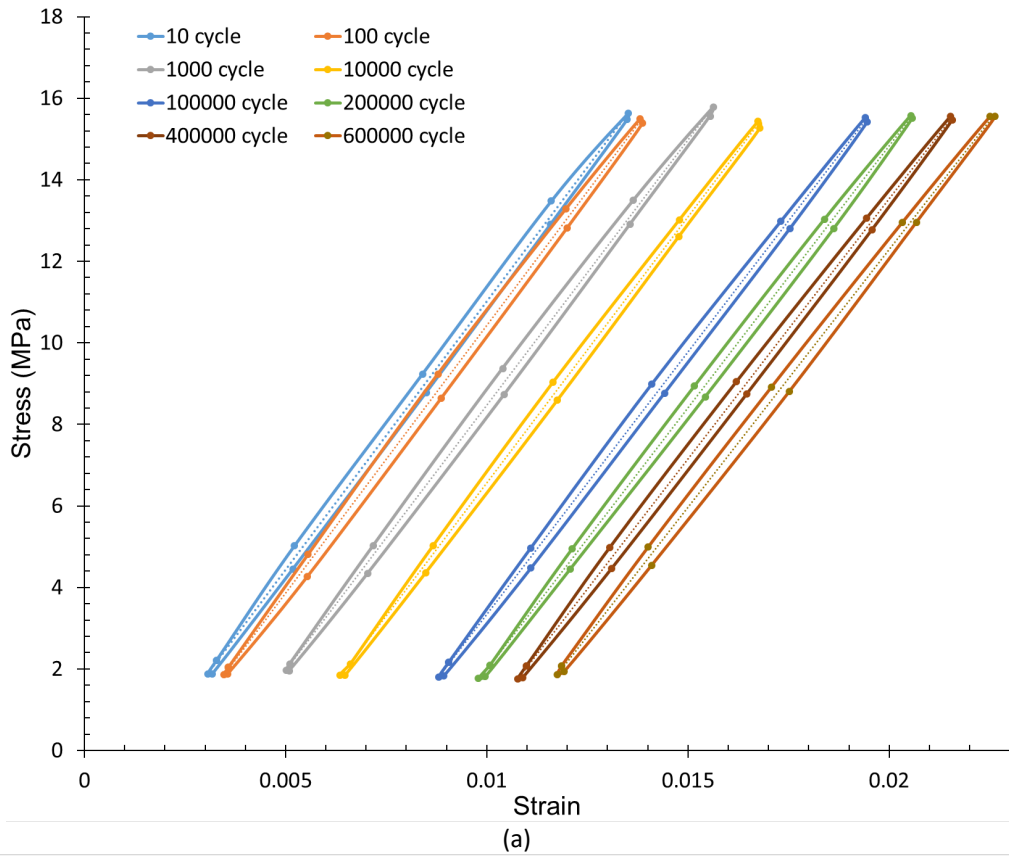
**Fig. 1.** S–N curves of the rubberwood /recycled PP composite collected before and after water ageing (arrows indicate run-out)

Figure 2 shows the hysteresis loop captured during the tension-tension fatigue test for both non-aged and water-aged rubberwood/recycled polypropylene (PP) composites. During cyclic loading, the material demonstrates a hysteresis loop resembling an ellipse. This phenomenon stems from both the viscoelastic properties of the polymer matrix and the friction occurring between surfaces that are debonded and delaminated.

The slope of the load-displacement curve, measured from the highest peak to the lowest peak (known as the secant modulus,  $E$ ), decreases as the material progresses from the initial first cycle (with the value  $E_1$ ) to cycle  $N$  ( $E_N$ ), indicating a reduction in stiffness, a phenomenon referred to as stiffness degradation. Additionally, the load-displacement curve may also shift due to the cyclic creep of the polymeric matrix.

Notably, it can be observed that, in both types of composites (non-aged and aged), the load-displacement curve shifts along the positive strain axis during the last cycle. As cyclic loading persists under fixed amplitude load control, the materials progressively become more compliant, leading to alterations in the amplitude of fatigue strains. This observation suggests significant creep has occurred.

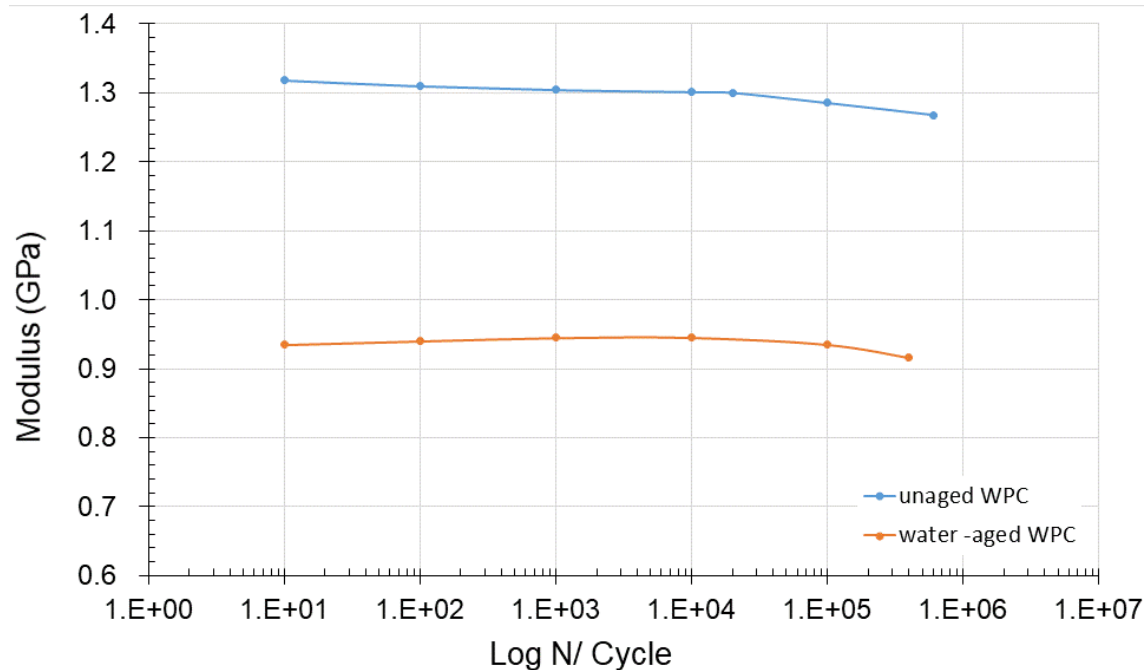
In the case of non-aged wood-polymer composites (Figure 2a), the hysteresis loop is observed to become more open as the cycles progress. Conversely, for the aged composite (Figure 2b), the hysteresis loops of the first and last cycles appear almost identical, suggesting that very little volumetric damage occurred in the composite system before failure [6].



**Fig. 2.** Typical hysteresis loops before (a) and after (b) water ageing at different lifetime cycle fractions for a given dynamic stress (60% UTS)

The evaluation of composite stiffness under cyclic loading calculated from the hysteresis loop (Figure 2) is plotted in Figure 3. Stiffness degradation in composites serves as an indicator of the onset of crack propagation within the composite and a weakening of the bond between the fibres and the

matrix. In theory, as the number of cyclic loading cycles increases, the density of cracks in the transverse direction tends to rise due to matrix splitting along the fibres. This damage hampers the effective transfer of load between the fibres, potentially leading to fibre failure before reaching the maximum stress observed in monotonic tensile tests, similar to those reported by Cadavid *et al.*, [20]. Consequently, the resistance to fatigue and the secant modulus tends to decrease with increasing fatigue life cycles [21,22].



**Fig. 3.** The secant modulus with fatigue life cycle tests before (a) and after (b) water ageing for a given dynamic stress (60% UTS)

#### 4. Conclusions

Comprehensive data regarding the mechanical behaviour, particularly the fatigue performance of wood polymer composite in ambient as well as influence by moisture is currently scarce. The objective of this study was to present fatigue data for rubberwood/ recycled PP both in ambient and water ageing. Exposure to moisture has caused a significant decrease in initial ultimate tensile strength and stiffness approximately - 53% and 56%. The composite also becomes more ductile, increasing strain at failure by 18%. However, the presence of moisture led to improvement in their fatigue resistance. The fatigue strength coefficient of the material is nearly halved following water ageing, in comparison to unaged specimens. The fatigue hysteresis loop revealed that the non-aged composite exhibits a more expansive area, greater tensile creep, and more pronounced fatigue damage when compared to the aged composite. Thus, despite the high susceptibility of this composite to water, it demonstrates good resistance to ageing even under challenging conditions. However, it can be improved through the application of coatings that can prevent or mitigate water absorption when the material is submerged or exposed to liquid water. These research findings should be factored into the design of bio-based composite structures and when estimating their long-term durability and residual properties.

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