

# Radiation Shielding Properties of Aluminosilicate Glass Systems using Phy-X Software

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ARTICLE INFO	ABSTRACT
Article history: Received 15 June 2023 Received in revised form 29 October 2023 Accepted 15 November 2023 Available online 16 January 2024 Keywords: Aluminosilicate glasses; Phy-X software; radiation shielding materials;	In this work, we studied the radiation shielding properties of aluminosilicate glasses with constant SiO <sub>2</sub> content. By applying Phy-X software, we calculated different radiation attenuation factors for the chosen glasses. The linear attenuation coefficient (LAC) for the chosen CaO–Al <sub>2</sub> O <sub>3</sub> –SiO <sub>2</sub> glass systems showed an exponential decrease as the energy changes from 0.015 to 15 MeV. For the glass with composition of 35CaO-SAl <sub>2</sub> O <sub>3</sub> -60SiO <sub>2</sub> , the LAC decreases from 29.80 to 1.279 cm <sup>-1</sup> between 0.015 and 0.05 MeV. The LAC decreases with the increase in the Al <sub>2</sub> O <sub>3</sub> content. The minimum LAC is found for the glass with the composition of 20CaO-20Al <sub>2</sub> O <sub>3</sub> -60SiO <sub>2</sub> . The effective atomic number ( $Z_{eff}$ ) was reported, and we found that the highest $Z_{eff}$ is occurred at 0.015 MeV and varied between 14.55 and 16.09. The Z <sub>eff</sub> decreases when we replaced the CaO by Al <sub>2</sub> O <sub>3</sub> . The half value layer was reported and we discussed the impact of the density of the glasses on the HVL values. In the low energy range, the HVL values are small and the different compositions have close HVL. For E>0.08 MeV, the HVL is higher than 1 cm for all glasses, while for E> 0.2 MeV, the HVL becomes higher than 2 cm for all glasses. The glass with composition of 35CaO-5Al <sub>2</sub> O <sub>3</sub> -60SiO <sub>2</sub> has better attenuation

#### 1. Introduction

Aluminosilicate glasses have excellent thermal and mechanical features, so they are used in different applications. One of these applications is the radiation shielding field. Radiation shielding materials are materials designed to attenuate the X-ray and gamma radiations or other types of radiation [1-3]. These materials are used to protect the human and environment from the hazard of the ionizing radiation. Lead and concrete are the two most popular materials used as radiation shields [4,5]. In addition, glasses in the current days are widely in the radiation shielding applications for many reasons. Glasses can be produced in different ways such as melt quenching method. Glasses are transparent materials, so we can use glasses in radiological rooms. We can easily modify the composition of the glasses in order to get effective glasses in radiation protection [6-8]. All these reasons encourage the researchers to develop glasses in radiation protection utilizations [9]. There

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are three methods to investigate the radiation shielding properties of the glasses: experimental method, theoretical method and simulation method [10]. In the experimental method, we need a suitable setup, which basically includes the samples, a detector, and the radioactive sources (such as Co-60, Cs-137 etc.). In the theoretical method, we use some basic equations and formulas to calculate some factors which describe the interactions between photons and the glasses. These factors are called attenuation factors. Some software can also be used to evaluate the attenuation factors such as WinXcoma and Phy-X software. In the simulation method we can use Monte Carlo simulation to simulate the interaction between the photons and the shield [11-15]. Using any of these previous methods, the researcher can determine the linear attenuation coefficient (LAC), the radiation protection efficiency (RPE) and other related factors. High LAC and RPE values for any glass are an indication of good radiation attenuation, so it is important to prepare glasses with high LAC and RPE values [16,17]. In contrast, a low half value layer is preferable in practical applications. In the literature, different research groups reported the LAC, RPE and other attenuation factors for borate, silicate, phosphate and other kinds of glasses [18]. In general, the previous works showed that one simplest way to enhance the radiation shielding performance is to use heavy metal oxides. Also, we can increase the thickness of the glass to get suitable radiation shielding materials [19,20]. In this work, we used theoretical method to study the radiation shielding properties of aluminosilicate glasses with constant SiO<sub>2</sub> content. Recently, there has been a growing attention in the development of new glass systems for gamma ray shielding utilizations. Glasses composed of SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and CaO have been investigated for their potential applications in different field. However, the majority of the previous works have focused on varying the concentration of  $SiO_2$  in the glass composition, while in this study, we maintain a constant amount of SiO<sub>2</sub> content (60 mol%) and change the concentration of CaO and Al<sub>2</sub>O<sub>3</sub>. This allows us to isolate the impacts of Al2O3 and CaO on the gamma ray attenuation features of the glasses, giving new insights into the effect of these compounds in the attenuation of the photons.

## 2. Materials and Methods

In this work, we aimed to calculate the radiation shielding factors for aluminosilicate glasses with constant SiO<sub>2</sub> content. The selected glasses were previously prepared by Takahashi *et al.*, [21]. In their work, they reported the thermal and structural properties of these glasses. We extended this previous work, and evaluated the basic radiation shielding properties of these glasses. The following is the composition of the glasses:

S1: 35CaO-5Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>, density=2.73 g/cm<sup>3</sup>

S2: 30CaO-10Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>, density=2.69 g/cm<sup>3</sup>

S3: 25CaO-15Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>, density=2.65 g/cm<sup>3</sup>

S4: 20CaO-20Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>, density=2.62 g/cm<sup>3</sup>

For the determination of radiation attenuation factor, we used Phy-X software [22].

Phy-X software is highly useful in the radiation shielding field since we can determine the attenuation factors for any sample at different energy region. This software works by taking in the composition of the materials and their respective densities. The energy range desired can then be specified, using a general spectrum or specific radioisotopes that are commonly used in such testing. The needed factors are then chosen, which the software determines and provides as its output to be discussed

The linear attenuation coefficient (LAC or  $\mu$ ) is a basic factor in the radiation shielding study. The LAC can be determined using Lambert-Beer Law

$$I = I_0 e^{-\mu x} \tag{1}$$

where x is the thickness of the sample.

The half value layer is another useful shielding factor. It represents the thickness of the shielding materials in which  $I_0$  changes to 0.5 $I_0$ . We can use the next formula for the calculation of HVL

$$HVL = \frac{\ln(2)}{LAC}$$
(2)

The reciprocal of LAC is defined as the mean free path. Namely

$$MFP = \frac{1}{LAC}$$
(3)

The thickness of the materials needed to shield most of the incoming photons (i.e.,  $I_0$  becomes 0.1I<sub>0</sub>) is called the tenth value layer. Mathematically

$$TVL = \frac{\ln 10}{LAC}$$
(4)

By determining both the HVL and TVL values of a medium, radiation shielding designers can develop space-efficient shields.

The effective atomic number (Zeff) of a material is calculated as

$$Z_{eff} = \frac{\sum_{i} f_{i} A_{i} \left(\frac{\mu}{\rho}\right)_{i}}{\sum_{j} f_{j} \frac{A_{j}}{Z_{i}} \left(\frac{\mu}{\rho}\right)_{i}}$$
(5)

Details about the attenuation factors can be found elsewhere [23-29].

## 3. Results and discussion

We plotted the linear attenuation coefficient (LAC) for the chosen CaO–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass systems with a constant amount of SiO<sub>2</sub> (60 mol%) in Figure 1. Apparently, the LAC values show an exponential decrease as the energy changes from 0.015 to 15 MeV. The rate of this decrease is very fast between 0.015 and 0.06 MeV, while it shows a slight decrease at higher energies. The quick decrease in LAC at the first few energies can be explained according to the dominance of the photoelectric effect. For example, for the glass with composition of 35CaO-5Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>, the LAC decreases from 29.80 to 1.279 cm<sup>-1</sup> between 0.015 and 0.05 MeV. While, between 0.1 and 0.4 MeV, the LAC for the same sample is decreased only from 0.511 to 0.264 cm<sup>-1</sup>. The trend in LAC at higher energies can be explained by Compton scattering and pair production. We can see from Figure 1 that the LAC decreases with the increase in the Al<sub>2</sub>O<sub>3</sub> content. Since all glasses contain constant amount of SiO<sub>2</sub> (60 mol%), the increase in the Al<sub>2</sub>O<sub>3</sub> content (or decrease in CaO content) causes a decrease in the density from 2.73 to 2.62 g/cm<sup>3</sup> which causes the reduction in the LAC due to the addition of Al<sub>2</sub>O<sub>3</sub>. The minimum LAC is found for the glass with a composition of 20CaO-20Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>. The LAC for

this glass at 0.015, 0.03, 0.1, 0.5, 1 and 10 MeV are respectively 21.59, 3.143, 0.463, 0.228, 0.166 and 0.060 cm<sup>-1</sup>.



**Fig. 1.** The linear attenuation coefficient for the CaO $-Al_2O_3-SiO_2$  glass systems with constant amount of SiO<sub>2</sub> (60 mol%)

In Figure 2, we plotted the results of the effective atomic number ( $Z_{eff}$ ) for the glasses with constant SiO<sub>2</sub> content. The highest  $Z_{eff}$  is found at 0.015 MeV and is equal to 16.09, 15.60, 15.09 and 14.55 for the S1 to S4 glasses respectively. The  $Z_{eff}$  at 0.02 MeV is in the order of 14.46-16.01 which is smaller than the  $Z_{eff}$  obtained at 0.015 MeV. Since the photoelectric effect is very important at low energy region, we can explain the highest  $Z_{eff}$  values for these glasses at low energy range. The  $Z_{eff}$  decreases with increasing the energy and reached the minimum values of 11.02 (for S1) and 10.50 (for S4). The minimum values of the effective atomic number at this energy can be explained according to Compton scattering. For E>1 MeV, we found a slight increase in the  $Z_{eff}$ , where the  $Z_{eff}$  values for S1 and S4 are 11.71 and 11.00 at 15 MeV. Moreover, we can see that the concentration of CaO and  $Al_2O_3$  is also affected the  $Z_{eff}$ . The  $Z_{eff}$  decreases when we replaced the CaO by  $Al_2O_3$  and this is expected since the atomic number of Ca is higher than that of Al. For this reason, we found that the  $Z_{eff}$  decreases as we move from S1 to S4. Accordingly, the glass with a composition of 35CaO-SAl\_2O\_3-60SiO\_2 has better attenuation performance than the other glasses in this study.



**Fig. 2.** The effective atomic number for the CaO–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass systems with constant amount of SiO<sub>2</sub> (60 mol%)

The half value layer for the chosen CaO–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass systems with constant amount of SiO<sub>2</sub> (60 mol%) is exhibited in Figure 3. In real utilizations, a smaller HVL is needed and we can get this by increasing the density of the sample. For the four selected glasses, the profile of HVL is similar, and this is expected since these glasses contain the same compounds, but the difference in the HVL between the samples is due to the change in the concentrations of CaO and Al<sub>2</sub>O<sub>3</sub> between these glasses. For low energy, the HVL values are small and the different compositions have close HVL. Numerically, the HVL for the glasses with 5, 10, 15 and 20 mol% Al<sub>2</sub>O<sub>3</sub> is 0.023, 0.026, 0.029 and 0.032 cm (this is at 0.015 MeV). For these glasses but at 0.03 MeV, the HVL values are 0.163, 0.180, 0.200 and 0.221 cm. For E>0.08 MeV, the HVL becomes higher than 1 cm for all glasses. Also, for E> 0.2 MeV, the HVL becomes higher than 2 cm for all glasses. While for E>0.5 MeV, the HVL for these glasses respectively. Moreover, S1 glass has a smaller HVL than S2-S4 glasses, while the highest HVL is found for S4. It is known that the HVL has an inverse relation with the density, so the S1 glass which possesses the highest density has a thinner HVL than the rest of the samples.



**Fig. 3.** The half value layer for the CaO–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass systems with constant amount of SiO<sub>2</sub> (60 mol%)

The tenth value layer values for the selected glasses at 0.1, 0.5 and 1 MeV were reported and presented in Figure 4. The TVL values increase as the energy increases from 0.1 to 1 MeV. This suggests that the thickness of the glasses must be increased to shield the photons with higher energies. Numerically, the TVL at 0.1 MeV is in the range of 4.97-4.5 cm, so we need a layer of thickness of around 5 cm in order to shield most of the incoming radiation with energy of 0.1 MeV. When it comes to radiation with energy of 0.5 MeV, we found that the TVL lies within the range of 9.64-10.09 cm. So, we need a thicker layer to block most of the radiation with energy of 0.5 MeV. The TVL for these glasses when the energy of the radiation is 1 MeV increases to 13.26-13.87 cm. So, the thickness of the glass is an important factor to be considered when we use the glasses in high energy radiation shielding applications.

The MFP is also determined and plotted in Figure 5. The MFP is small at the low energy range, ranging from 0.034 to 0.046 cm at 0.015 MeV, from 0.076 to 0.106 cm at 0.02 MeV and from 0.235 to 0.318 cm at 0.03 MeV. Thereafter, the MFP starts increasing and reaches to about 1 cm at 0.06 MeV. When the energy reached 0.1 MeV, we found that the MFP was on the order of 2 cm. With the increase in energy, the MFP continues to increase and reaches around 4 cm at 0.4 MeV. At 3 MeV, we found that the MFP is very high and equals to 10.01 cm for S1 and 10.52 cm for S2. The maximum MFP is determined at 15 MeV and equal to 16.36 cm for S1 and 17.71 cm for S4. Also, we found that the MFP increased with the addition of  $Al_2O_3$ . So, the sample with high  $Al_2O_3$  content has high MFP. This is because the MFP has an inverse relation with the LAC, so when we added  $Al_2O_3$ , the LAC decreases and the MFP increases.



Fig. 4. The tenth value layer values for the selected glasses at 0.1, 0.5 and 1  $\,\rm MeV$ 



Fig. 5. The mean free path for the selected glasses at 0.1, 0.5 and 1  $\,\rm MeV$ 

# 4. Conclusion

We reported the radiation attenuation parameters of aluminosilicate glasses with constant SiO<sub>2</sub> content with the help of Phy-X software. The LAC for the CaO–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> glass systems showed an exponential decrease with increasing the energy from 0.015 to 15 MeV. The maximum LAC is found for the glass with the composition of 35CaO-5Al<sub>2</sub>O<sub>3</sub>-60SiO<sub>2</sub>. Also, this sample showed the highest Z<sub>eff</sub> and the minimum HVL. The maximum Z<sub>eff</sub> for the chosen glasses lies in the range of 14.55 and 16.09, while the minimum Z<sub>eff</sub> is in the order of 10.50-11.02. We investigated the thickness of the glasses needed to shield 50% of the incoming photons and reported this thickness at different energy levels. At low energy, we found that the HVL is varied between 0.023 and 0.032 cm at 0.015 MeV. At 0.03 MeV, the HVL values are 0.163, 0.180, 0.200 and 0.221 cm. For E> 0.2 MeV, the HVL becomes higher than 2 cm for all glasses. Also, for E>0.5 MeV, the HVL for these glasses is higher than 3 cm. The maximum HVL is reported at 15 MeV and equal to 11.34, 11.66, 11.99 and 12.28 cm for the S1 to S4 glasses

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