

# Characteristic Performance Comparison of Schottky Diodes for RF Energy Harvesting

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#### **1. Introduction**

Radio frequency energy harvesting (RFEH) has been the researchers' focus due to the implementation of large number of wireless devices [1, 2] and the advanced use of wireless technology [3]. RFEH is the process of converting the electromagnetic waves into useful and manageable electric power [4, 5], where the source can be from ambient or dedicated RF energy [6], [7]. Generally, ambient RF energy from WIFI and cellular network might be sufficient to low power electronic devices [8, 9]. Even though the power generated in RFEH is small compared to other EH [10, 11], the bright side is the energy is always there, it has been continuously radiated in the environment, thus no effort needed to create the source [12].

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Quadband rectifier were proposed in previous works [3, 7, 13, 14] using HSMS2850 Schottky diode, where efficiency varies from 30% to 70% by a single stage voltage doubler. While works in [4, 15, 16], used SMS3670 in their proposed rectifier circuit resulted in minimum efficiency of 45%. A frequency-dependent multiple antenna that enables the harvester to fully exploit all available frequency bands, including 0.94, 1.81, 2.42 and 2.90 GHz frequency bands using a single-series diode topology [3]. The design yields 0.797 V output voltage and 55.5%, 52.5%, 66.52%, 52.9% and 65.5 % PCE at -27dBm input power. A voltage doubler rectifier is designed to operate at 2.4 GHz frequency band resulting to an output of 1.6 V and 45% PCE at 5 dBm input power [15].

In work [17], a voltage doubler circuit is designed and implemented with the help of microstrip transmission lines, used for impedance matching between the antenna and the rectifier for the optimum power transfer from the antenna to the load for the operation dual bands of universal mobile telecommunication service and WIFI, covering 2.15 and 2.45 GHz frequency bands the design yield an output of 0.96 V and 42% PCE at 0 dBm input power. A simple impedance matching network by using Smith chart utility in [12] was designed for each frequency band according to the impedance found at each band. These frequencies cover 0.9, 1.8, 2.1 and 2.45 GHz. The rectifier circuit is voltage doubler which generates 1.662, 1.422, 1.333, and 1.587 V output voltage and 74.846%, 66.974%, 64.486%, and 61.407% at each frequency at the input power of 0dBm, respectively. [14] used transmission Line as Input Impedance matching network operates at 900 MHz using voltage doubler rectifying circuit. The circuit produces a 0.6 V and 44.30% PCE at 0 dBm input power. On the other hand, CMOS based rectifiers were designed in works [18, 19], however, the designs were complex and face many challenges, such as, high threshold voltage and body effect of the CMOS transistors.

The focus on this work is on a simple single voltage doubler using HSMS2860 diode. Prior to rectifier design, a characterization on the diode component is done to verify the diode characteristics. Next, the comparison between a mathematical model and simulation is presented. Finally, a single stage voltage doubler is presented and analyzed based on the diode characteristics and mathematical model. Wireless communication technologies such as ISM, GSM, and LTE/4G/5G frequency bands are deemed probable candidates for RFEH [20]. Due to the growth of wireless communication and current developments toward 5G technology, all the analysis done in this paper are based on 700 MHz frequency band of 5G communication technology.

## **2. Diode Modelling**

Diode-based rectifier circuits are the most popular because they have a lower forward voltage drop than CMOS circuits [6]. The diode is an important component of the rectifier circuit as it influences the conversion efficiency of the rectifier circuit. Most researchers used Schottky diodes in high frequency and RFEH applications in their works due to their low threshold voltage drop such as, SMS7630, HSMS2820, HSMS2850, and HSMS2860 [1, 3, 5, 7, 13]. In this paper, HSMS2860 Schottky diode is chosen for modeling with its junction capacitor, series resistance, and voltage threshold voltage of 0.18 pF, 6 Ω, and 0.65 V respectively. The diode linear equivalent circuit has been modeled using Advanced Design Systems (ADS) as shown in Figure 1(a). The Rs is the series resistor, Cj is the junction capacitance, and the Rj is the junction resistance calculated using Eq. (1), where n is equal to 1.08 and the saturation current (Is) is 50 nA.

$$
R_{j} = \frac{8.33 \times 10^{-5} nT}{l_{b} + l_{s}}
$$

(1)

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The I-V curve plot under forward biased is illustrated in Figure 1(b) where it is calculated at temperature (T) of 298K. It showed that the forward biased voltage is increase as the current is increase and reached saturation above 100 mA forward current. Figure 2(a) show a simple impedance matching network for a 700 MHz circuit with a 65 nH inductor in series with the Schottky diode. A lumped element of 100 pF of load capacitance were placed at the output. The circuit is simulated in ADS software, and it well matched at 700MHz with a return loss of -50 dB as shown in Figure 2(b). Harmonic balance tool in ADS were used to simulate the circuit performance in term of output power, where the result is shown in Figure 2(c). The input power was varied from -50 dBm to 0 dBm, and the voltage output reached 1V for -7 dBm input power. The analysis continues further with comparison between mathematical calculation with circuit simulation in the next section.



**Fig. 2.** (a) HSMS-2860 detector circuit (b) S-parameter result (c) Input power versus output voltage

#### **3. Performance Comparison by Mathematical Model and ADS Simulation**

The diode performance based on power conversion efficiency (PCE) is analyzed using Eq. (2). The mathematical equations are modeled in *Scilab* numerical computational software. The A, B, and C in equation to is calculated using Eq. (3). Vj, Rs, and  $C_{10}$  represent voltage across the diode, series resistance, and junction capacitance at zero bias respectively. RL,  $\theta_{\text{on}}$ , and C<sub>i</sub> represent load resistance, forward bias turn on angle, and junction capacitance. Table 1 consists of SMS7630, HSMS2820, HSMS2850, and HSMS2860 diodes parameters used in the mathematical model.

$$
\eta(\%) = \frac{100}{1 + A + B + C} \tag{2}
$$

where A, B and C can be calculated in Eq. (3)

$$
A = \frac{R_L}{\pi R_S} \left( 1 + \frac{V_j}{V_{DC}} \right)^2 \left[ \theta_{on} \left( 1 + \frac{1}{2\cos^2 \theta_{on}} \right) - 1.5 \theta_{on} \right], B = \frac{R_L R_S C_j^2 \cdot \omega^2}{2\pi} \left( 1 + \frac{V_j}{V_{DC}} \right) \left[ \frac{\pi \cdot \theta_{on}}{\cos^2 \theta_{on}} + \tan \theta_{on} \right],
$$
  
\n
$$
C = \frac{R_L}{\pi R_S} \left( 1 + \frac{V_j}{V_{DC}} \right) \frac{V_j}{V_{DC}} \left[ \tan \theta_{on} - \theta_{on} \right]
$$
\n(3)

where,

$$
\tan \theta_{\text{on}} - \theta_{\text{on}} = \frac{\pi R_{\text{S}}}{R_{\text{L}}(1 + \frac{V_{\text{j}}}{V_{\text{DC}}})}
$$
(4)

$$
C_j = C_{j0} \sqrt{\frac{V_j}{V_j + V_{DC}}} \tag{5}
$$





The result from the mathematical model is shown in Figure 3 for output range from 0 to 5 Vdc. It can be noticed that HSMS2820 and HSMS2860 have almost an identical power conversion efficiency (PCE) result of 60% as illustrated in Figure 3(a). This can be attributed to their junction threshold voltage and series resistance being identical with a difference in junction capacitance. Whereas Figure 3(b) is the close-up version of Figure 3(a) to observe the output range from 0 to 0.5 Vdc. Noticeable that the SMS7630 and HSMS2850 perform better from 0 to 0.2 Vdc, as they have lower junction voltage. while HSMS2820 and HSMS2860 shows a better PCE at 0.4 Vdc.

Figure 4 shows the simulation circuit, it is a simple single series diode with one transmission line. Diode simulation model is similar to the mathematical model parameters in addition to N, and M, ideality factor, and grading coefficient respectively. RL is 50  $\Omega$  for both simulation and mathematical model. The simulation is conducted in ADS software. The results obtained can be seen in Figure 5(a), where the input power is in the range of -30 to 40 dBm. It can be observed that the results of PCE are lower than the mathematical model. This difference can be ascribed to the mathematical model's

utilization of only three parameters for each diode and its assumption of nearly ideal conditions concerning losses. Furthermore, the simulation model has a transmission line that operates as impedance matching that will introduce losses to the circuit. Similar pattern to mathematical model can be seen, where the highest diode results belong to HSMS2860, and lowest belong to HSMS2850.



Fig. 3. Power conversion efficiency calculated from mathematical model (a) Vdc 1 to 5V (b) Vdc 0 to 0.5V



**Fig. 4.** Single diode in ADS simulation circuit



**Fig. 5.** Single diode in ADS simulation result (a) High input power (b) Low input power

Figure 5(b) show the plot of simulation results for low input power from -30 to 0 dBm, respectively. It can be noticed that HSMS2850 and SMS7630 has a higher PCE for lower power input voltage, as mentioned in [18] the HSMS2850 has a better result in low power application in contrast to HSMS2860 which shows a better result with higher input power voltage for mathematical model and simulation. Both mathematical and simulation show similar trend on the PCE where HSMS2860 and HSMS2820 is suitable for high input power, while HSMS2850 and SMS7630 are preferable for low power rectifier circuit.

## **3. Voltage Doubler**

The basic components of the voltage doubler rectifier topology include two Schottky diodes and two capacitors [16]. The voltage doubler is a single voltage multiplier circuit, where the output is double from the input. The capacitor C1 and C2 active in one of the positive and negative cycle, which double the output voltage. Figure 6(a) shows the simulation circuit of a single voltage doubler with a simple matching network consisting of a shunt capacitor and a series inductor. Unlike a single series or shunt diode topology, the voltage doubler will get a higher PCE as shown in Figure 6(b) because it converts a full wave signal. Figure 6(c) shows the output voltage, roughly twice the input voltage (Vin), therefore  $V_{\text{out}} = 2V_{\text{in}}$  [12]. For the proposed circuit, the PCE maximum at 21 dBm input power with PCE of 87%. To increase the output voltage, the voltage doubler stages can be increased and become a voltage multiplier. Depending on the stages the voltage will multiply but losses will increase due to the increased number of components [4].



**Fig. 6.** (a) Voltage doubler simulated in ADS (b) Power conversion efficiency versus input power (c) Output voltage versus input power

## **4. Conclusions**

RFEH system purpose is to harvest the ambient RF power from RF Energy sources. The diode is an important component of the rectifier circuit and influences the PCE of the rectifier circuit which influences the overall RFEH system quality and effectiveness. In this work, the HSMS2860 Schottky diode is chosen for modeling in ADS. The diode is characterized with I-V curve and efficiency at 700MHz frequency. Next, a mathematical model and simulation model with a single diode configuration is analyzed to determine the input power range suitable for a selected Schottky diodes namely, SMS7630, HSMS2820, HSMS2850, and HSMS2860. The results show that for high input power, HSMS2860 has a PCE of 60% using the mathematical model and 53% using the simulation model. For low input power SMS7630 and HSMS2850 showed a better efficiency result of approximately 20% at 0.1 Vdc. The variation of mathematical and simulation came from some of the spice parameters were neglected during mathematical analysis, plus with the nonlinearity in the diode characteristic and a transmission line has been introduced for impedance matching which introduced additional losses. From the results we can determine the suitable application for the Schottky diode. Additionally, a single stage voltage doubler is simulated using ADS with a simple matching network consisting of a shunt capacitor and a series inductor. Upgrading from a single series or shunt diode topology to voltage doubler produces higher PCE as it covers both positive and negative cycle of input signal. The output voltage of a voltage doubler roughly twice the input voltage if components loss is neglected. Cascading the voltage doubler stages into multiple stage to become a voltage multiplier, can increase the output. Depending on the stages the voltage will multiply but losses will increase due to the increased number of components.

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