

# Investigation of Inner Elliptical Pin-Fins Configuration on Magnetoconvective Heat Transfer

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#### ABSTRACT

This paper deals with Lattice Boltzmann computation of two-dimensional incompressible flow past two heat elliptical sinks vertically attached to the horizontal walls of a cavity in the presence of magnetic field. A two dimensional nine-velocity square lattice Boltzmann (D2Q9) model is used. The obtained results show that the applied Lattice Boltzmann method (LBM) can effectively capture vortex shedding structures and other features inside such complex flow. The present study has been carried out for Hartmann numbers with panoply of heat sinks location. Results show that the heat sinks positions greatly influence the heat transfer rate depending on the Hartmann number.

#### Keywords:

Lattice Boltzmann method; D2Q9 model; convection; Heat transfer; MHD; curved boundary; elliptical sinks

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#### 1. Introduction

Natural convection in MHD (magneto hydrodynamic) cavities is an important phenomenon in engineering systems and in various industries of high-performance insulation for packed sphere beds, grain storage, float glass production, buildings, injection molding chemical catalytic reactors, airconditioning in rooms, cooling of electronic devices and geophysical problems. Extensive research studies using various numerical simulations were conducted into natural convection [1-24]. Some of the latter works have acquired a basic understanding of free convection flows and heat transfer characteristics MHD free convection flows because those configurations can be encountered in numerous problems with industrial and technological interest, covering a wide range of basic sciences such as nuclear engineering, fire research, crystal growth, astrophysics and metallurgy. In MHD free convection flows, the balance is achieved by inertial, viscous, electromagnetic and buoyancy forces, rendering the solution more complicated.

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In order to simulate such engineering complex configuration with mixed boundary conditions and in the presence of internal elliptical heat sinks placed at different positions on the south and the north walls of the MHD cavity, the Lattice Boltzmann Method (LBM) is used. It is to be known that the (LBM) is a new method for simulating fluid flow and modeling physics in fluids. It has been applied extensively within the last decade. Based on kinetic theory for simulating fluid flows and modeling the physics in fluids [25-32], it becomes a powerful, effective and easy numerical method, for simulation of complex flow problems with different boundary conditions [33, 34].

In comparison with the conventional CFD methods, the LBM isbased on the microscopic models, mesoscopic kinetic equations. The macroscopic dynamics of a fluid is the result of collective behavior of many microscopic particles in the system. The LBM has been proved to recover the Navier-Stokes equation by using the Chapman-Enskog expansion. The major advantage of this method is its explicit feature of the governing equation, easy for parallel computation and easy for implementation of irregular boundary conditions. To our best knowledge, no previous study on effects of elliptical heat sinks on natural convection in an MHD cavity with the LBM had already been studied so far. The main aim of this paper is to study this complex configuration in cavity filled with liquid gallium (Pr=0.025) and a pure fluid (Pr=0.7) and also to highlight the ability of the LBM for solving problems with various complex boundary conditions. The qualitative effects of Hartmann number on horizontal velocity, vertical velocity streamlines, isotherms, mean square velocity and pressure are investigated.

# 2. Mathematical formulation

# 2.1 Study Cases

The considered model is shown in Figs.1-3. It displays a two-dimensional cavity with side length of H. the semi elliptical obstacles are with a radius (r) equal to the semi minor axis (a) and (b) the semi major axis equal to 0.25H. The left vertical is maintained at high temperature ( $T_H$ ) while the three other walls are insulated and impermeable to mass transfer. The cavity can be filled with a liquid gallium with Pr number of 0.025 or a non MHD fluid (Pr=07). The gravitational acceleration acts downward. The uniform external magnetic field with a constant magnitude  $B_0$  is applied in the transverse x-direction. It is assumed that the induced magnetic field produced by the motion of an electrically conducting fluid is negligible compared to the applied magnetic field. Thermo-physical properties of the fluid are assumed to be constant, and the density variation in the buoyancy force term is handled by the Boussinesq approximation. The flow is two-dimensional, laminar and incompressible; in addition, it is assumed that the viscous dissipation and Joule heating are neglected.



**Fig. 1.** Configuration 1 and mixed boundary conditions



**Fig. 2.** Configuration 2 and mixed boundary conditions



**Fig. 3.** Configuration 3 and mixed boundary conditions



Fig. 4. The standard  $D_2Q_9$  lattice for velocity and temperature mode

### 2.2 Numerical Method: Lattice Boltzmann Method (LBM)

A scheme of the standard D2Q9 (Figure 4) for flow and for temperature LBM method are used in this work [33-34] hence only brief discussion will be given in the following paragraphs, for completeness. The governing equations for MHD free convection are written in terms of the macroscopic variable depending on horizontal and vertical positions respectively as: Continuity equation

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

Momentum equations

$$\rho(u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}) = -\frac{\partial p}{\partial x} + \mu(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2}) + F_x$$
(2)

$$\rho(u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y}) = -\frac{\partial p}{\partial y} + \mu(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2}) + F_y$$
(3)

**Energy equation** 

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}\right)$$
(4)

where  $v = \mu / \rho$  is the kinematic viscosity,  $F_x$  and  $F_y$  are the body forces at horizontal and vertical directions respectively and they are defined as follows [25]:

$$F_x = R(v\sin\gamma\cos\gamma - u\sin^2\gamma) \tag{5}$$

$$F_{y} = R(u\sin\gamma\cos\gamma - v\cos^{2}\gamma) + \rho g\beta(T - T_{m})$$
(6)

where the Ha number is defined as

$$Ha = L B_x \sqrt{\sigma / \mu} \tag{7}$$

In the LBM the total force is:

$$F = F_x + F_y \tag{8}$$

$$F_{x} = 3w_{k} \rho \Big[ R \left( v \sin \gamma \cos \gamma \right) - u \sin^{2} \gamma \right) \Big]$$
(9)

$$F_{y} = 3w_{k}\rho \begin{bmatrix} g_{y}\beta(T-T_{m}) \\ +R(u\sin\gamma\cos\gamma) - v\cos^{2}\gamma \end{bmatrix}$$
(10)

where  $R = \mu H a^2$  and  $\gamma$  is the direction of the magnetic field.

The functional density, velocity and temperature in the mesoscopic approach are:

$$\rho(\mathbf{r},t) = \sum_{k} f_{k}(\mathbf{r},t)$$
(11)

$$\mathbf{u}(\mathbf{r},t) = \sum_{k} \mathbf{c}_{k} f_{k}(\mathbf{r},t) / \rho(\mathbf{r},t)$$
(12)

$$T = \sum_{k} g_{k}(\mathbf{r}, t)$$
(13)

## 3.3 Solution Method and Algorithm

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To ensure that the code simulates an approximated incompressible regime, the characteristic velocity of the flow ( $V = \sqrt{g\beta_T H(T_w - T_w)}$ ) at the free convection regime must be compared with the fluid speed of sound c<sub>s</sub>. In the present study, the characteristic velocity is selected as 0.1 of sound speed. By fixing Ra number  $Ra = \beta g_y H^3 \Pr(T_H - T_C)/v^2$ , Pr number  $\Pr = \alpha v$  and Mach number (Ma = u/c), the kinematic viscosity  $v = Ma Hac_s \sqrt{\Pr/Ra}$  and thermal diffusivity  $\alpha$  are deduced. Nusselt number Nu is one of the most important dimensionless parameters in describing the convective and thermic heat transport. For the example, the local Nusselt number and the average value at the left side wall are calculated as;

$$Nu_{y} = -\frac{H}{T_{H} - T_{C}} \frac{\partial T}{\partial x} \bigg|_{x=0}$$
(14)

$$Nu_{av} = \frac{1}{H} \int_{0}^{H} Nu_{y} dy$$
<sup>(15)</sup>

In the following section, we present the steps that must be executed for the numerical implementation:

- Input constant parameters.

-Calculate the relaxation times.

- Initialize the temperature, and velocity fields for the entire computational domain and the equilibrium distribution functions.

- Calculate the current distribution function for propagation of temperature and velocity.

- Propagate all current distribution functions to the neighbor lattices in all directions.

- Impose the boundary conditions.

- Calculate the current temperature and velocity field for the entire computational domain and the current equilibrium distribution functions using the current temperature and velocity fields

- The error convergence is checked, if the error doesn't satisfies the convergence criterion, go to step

# 4. Results and Discussion

Figures 5 and 6 highlight the great influence of the positions of the heat sinks, with three proposed different configurations, on the flow intensity by the modification of the temperature distribution and the streamlines inside the cavity (Pr=0.7 and  $Ra = 10^5$ ). For the first configuration, the cold zone is located at the bottom of the cavity next to cold wall, for the third configuration I the cold zone is located at the top of the cavity next to cold wall and for the second one, the cold zone is located symmetrically in the medium of the cavity next to the right wall (Fig. 5). The position and the size of these cold zones influence the flow intensity in the cavity (Fig. 6)



**Fig. 5.** isotherms for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Pr=0.7 for different configurations of heat sink's positions



**Fig. 6.** isotherms for aspect ratio AR=10 (a=r and b=0.25H) when  $Ra = 10^5$  and Pr=0.7 for different configurations of heat sink's positions

Figures (7-12) shows the qualitative effect of the Hartmann (Ha=0, absence of MHD) and (Ha=150) number with a high Rayleigh number (Ra= $10^5$ ) in the case of liquid gallium, on the horizontal velocity (fig. 7), the vertical velocity (Fig. 8), the streamlines (Fig. 9), the isotherms (Fig. 10), the mean square velocity (Fig. 10) and the pressure (Fig. 11) of the liquid gallium with Pr=0.025. This simulation is for a specific placement configuration of the heat sinks (configuration 1).



**Fig. 7.** Isotherms for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Pr=0.025. (configuration 1)

The isotherms show, for all Hartmann number, the same patterns while for the streamlines a great variation is highlighted. In fact, a circular big cell in clockwise rotation is formed inside the cavity for Ha=0 that increase and extend differently when Hartmann increase (Figs. 8-11). We notice also that, the presence of heat sinks produces inactive areas next to the right vertical wall (Fig. 7). We highlight an intense temperature gradient between the hot wall and the cold semi elliptical sinks,

indicating strong heat transfer rate in this region. The patterns of pressure are highly influenced by increasing Hartmann number (Fig. 12).



**Fig. 8.** Streamlines for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Pr=0.025. (Configuration 1)



**Fig. 9.** Horizontal velocity for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Pr=0.025. (Configuration 1)



**Fig. 10.** Vertical velocity for aspect ratio AR=10 (a=r and b=0.25) when Ra =  $10^5$  and Pr=0.025. (Configuration 1)



**Fig. 11.** Mean square velocity for aspect ratio AR=10 (a=r and b=0.25H5) when Ra =  $10^5$  and Pr=0.025. (Configuration 1)



**Fig. 12.** Pressure for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Pr=0.025. (Configuration 1)

Figure 13 show the local Nusselt number along the hot wall for  $Ra=10^5$ , Ha= 0 Pr=0.7and Pr=0.025 respectively. The results show that for a high Rayleigh number, the local Nusselt number increase with the decrease of Prandtl number in the absence of magnetic effect.



**Fig. 13.** Variation of the local Nusselt number for e for aspect ratio AR=10 (a=r and b=0.25H) when Ra =  $10^5$  and Ha=0. (Configuration 1)

# 5. Conclusions

The present study considered steady state, laminar, two-dimensional MHD free convection within a liquid gallium filled square enclosure in the presence of in-plane magnetic field for mixed boundary conditions in the presence of semi elliptical heat sinks.

In the present paper the effects of the positions of semi elliptical heat sinks and Hartmann number has been analyzed with LBM. This investigation demonstrated ability of LBM for simulation such complex engineering configuration. In addition, this method helps to obtain stream function and isotherm counters smoothly. This investigation was performed for various positions of semi elliptical heat sinks and Hartmann number and we deduce that The heat sinks positions greatly influence the heat transfer rate depending on the Hartmann number for a high Rayleigh number of Ra=10<sup>5</sup>. Besides in the absence of MHD effect the local Nusselt number increase with the decrease of the Prandtl number.

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