

# Nanofluid Flow and Heat Transfer between a Stationary Nonpermeable Disk and a Permeable Rotating Shrinking Disk with Radiation and Heat Generation Effects

Rusya Iryanti Yahaya<sup>1,\*</sup>, Norihan Md Arifin<sup>1,2</sup>, Fadzilah Md Ali<sup>1,2</sup>, Siti Suzilliana Putri Mohamed Isa<sup>1,3</sup>

<sup>1</sup> Institute for Mathematical Research, Universiti Putra Malaysia, 43400 Serdang, Selangor, Malaysia

<sup>2</sup> Department of Mathematics and Statistics, Universiti Putra Malaysia, 43400 Serdang, Selangor, Malaysia

<sup>3</sup> Centre of Foundation Studies for Agricultural Science, Universiti Putra Malaysia, 43400 Serdang, Selangor, Malaysia

ARTICLE INFO	ABSTRACT
Article history: Received 22 May 2022 Received in revised form 20 October 2022 Accepted 31 October 2022 Available online 20 November 2022	The flow between bounded surfaces is known as internal flow. The internal flow between disks has many significant applications, such as gas turbine rotors, rotating machinery, food processing technology, and air cleaning machines. In the current study, the nanofluid flow between two disks, nonpermeable and stationary, and the other permeable, rotating and shrinking, is analysed. The governing partial differential equations and boundary conditions are proposed with the inclusion of radiation and heat generation effects. Then, similarity transformations are utilised in deriving the nonlinear ordinary differential equations and boundary conditions for computation
Keywords: Nanofluid; internal flow; shrinking disk; thermal radiation; heat generation	using the bvp4c solver. Multiple solutions are obtained, and only the first solution is stable. The combination Mn-ZnFe <sub>2</sub> O <sub>4</sub> /C <sub>2</sub> H <sub>6</sub> O <sub>2</sub> nanofluid is found to produce the lowest magnitude of skin friction coefficient and the highest heat transfer rate.

#### 1. Introduction

Choi and Eastman [1] proposed nanofluid, which is composed of nanometer-sized particles (*e.g.*, metallic nanoparticles, metallic oxide nanoparticles, and nanotubes) suspended in a base fluid (*i.e.*, conventional heat transfer fluid such as water, ethylene glycol, and engine oil). Following the pioneering work by Maxwell [2], this study was done to find a better heat transfer fluid with high thermal conductivity. Applications of nanofluid range from manufacturing processes to biomedical applications, such as in heat exchangers, as a coolant in nuclear systems and automobiles, drug delivery systems, medicine, nanorefrigerants, sunscreen products, magnetic sealing, and building heating systems [3-6]. Researchers conducted various studies on the external and internal flows of the nanofluids to identify the flow behaviour and thermophysical properties of this fluid [7-16].

External flow is unbounded flow over a surface, while internal flow is a flow between bounded surfaces, for example, through a pipe, duct, or channel with confining walls. Fluid flow between

\* Corresponding author.

E-mail address: rusyairyanti@gmail.com

rotating disks was initially studied by Batchelor [17]. In this work, it was predicted that a boundary layer would form on both disks, and the main body of the fluid would rotate. However, Stewartson [18] found that the boundary layer only forms on the rotating disk, with the main body of fluid being essentially stationary when the disks rotate in a different direction or one of the disks is static. Later, Mellor *et al.*, [19] presented a theoretical and experimental study on the flow between a stationary and a rotating disk. Then, Narayana and Rudraiah [20] extended this study by considering a uniform suction on the static disk. Next, Lopez [21] considered a corotating cylinder surrounding the stationary and rotating disk and studied the fluid flow in this geometry. Kavenuke *et al.*, [22] then produced approximate solutions for flow between an impermeable stationary disk and a porous rotating disk. Further extension of this study was conducted by Upadhya *et al.*, [23] by considering nanofluid, as the working fluid, in the presence of a magnetic field and internal heating. Numerical solutions were generated in this study. Bilal *et al.*, [24] recently expanded this study with a nanofluid containing gyrotactic microorganisms and magnetic nanoparticles. The radial wall friction along the gyrating disk was found to be elevated by heat generation. Meanwhile, the augmentation of the chemical reaction boosted the mass transfer rate in the internal flow of the nanofluid.

The present study will analyse the nanofluid flow between two disks, with one disk stationary while the other is rotating and shrinking. This study is extended from Kavenuke *et al.*, [22] and Upadhya *et al.*, [23] to the case of a nanofluid and shrinking disk. Partial differential equations and boundary conditions that govern this flow problem will be simplified and solved numerically in MATLAB. The results, represented by tables and graphs, will be scrutinised and discussed.

## 2. Mathematical Formulation

Consider a steady nanofluid flow between a stationary nonpermeable disk (lower disk) and a permeable rotating shrinking disk (upper disk). The stationary and rotating disks are separated by a distance l, as shown in Figure 1, where  $(r, \varphi, z)$  are cylindrical coordinates with r – axis measured in the vertical direction and z – axis measured in the horizontal direction. However, the angle  $\varphi$  will not appear in the mathematical formulation due to rotational symmetry, and the distance l is very small compared to the radii of the disks [22]. Meanwhile, the upper permeable disk rotates about the z – axis with a velocity  $\Omega \varepsilon$ , where  $\Omega$  is the angular velocity and  $\varepsilon$  ( $0 < \varepsilon \leq 1$ ) is a regulator which controls the rotation of the disk. The rotation occurs when  $\varepsilon > 0$  and is at rest for  $\varepsilon = 0$ . Here,  $w_0$  is the constant mass flux velocity with  $w_0 > 0$  for suction and  $w_0 < 0$  for injection. Thermal radiation and internal heating effects are considered in the heat transfer analysis.



Fig. 1. Physical model and coordinate system

Under these assumptions, the following set of boundary layer equations governing the flow of water ( $H_2O$ ) and ethylene glycol ( $C_2H_6O_2$ ) suspended by cobalt ferrite (CoFe<sub>2</sub>O<sub>4</sub>) and Mn-Zn ferrite (Mn-ZnFe<sub>2</sub>O<sub>4</sub>) nanoparticles can be expressed as [23]

$$\frac{1}{r}\frac{\partial(r\,u)}{\partial\,r} + \frac{\partial\,w}{\partial\,z} = 0,\tag{1}$$

$$u \frac{\partial u}{\partial r} + w \frac{\partial u}{\partial z} - \frac{v^2}{r} = -\frac{1}{\rho_n} \frac{\partial p}{\partial r} + \frac{\mu_n}{\rho_n} \left[ \left( \frac{\partial}{\partial r} \left( \frac{u}{r} \right) \right) + \frac{\partial^2 u}{\partial z^2} \right], \tag{2}$$

$$\frac{u}{r}\frac{\partial(r\,v)}{\partial\,r} + w\,\frac{\partial\,v}{\partial\,z} = \frac{\mu_n}{\rho_n}\left[\left(\frac{\partial}{\partial\,r}\left(\frac{v}{r}\right)\right) + \frac{\partial^2v}{\partial\,z^2}\right],\tag{3}$$

$$u \frac{\partial w}{\partial r} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho_n} \frac{\partial p}{\partial z} + \frac{\mu_n}{\rho_n} \left[ \frac{1}{r} \frac{\partial w}{\partial r} + \frac{\partial^2 w}{\partial z^2} \right],\tag{4}$$

$$u \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} = \frac{k_n}{\left(\rho C_p\right)_n} \left[ \frac{1}{r} \frac{\partial T}{\partial r} + \frac{\partial^2 T}{\partial z^2} \right] - \frac{1}{\left(\rho C_p\right)_n} \frac{\partial q_r}{\partial z} + \frac{Q_0}{\left(\rho C_p\right)_n} \left(T - T_2\right), \tag{5}$$

along with the boundary conditions given by

• he nonpermeable stationary disk at z = 0

$$u(r,0) = 0, \quad v(r,0) = 0, \quad w(r,0) = 0, \quad T(r,0) = T_1.$$
 (6)

• The permeable rotating shrinking disk at z = l

$$u(r,l) = 0, \quad v(r,l) = r \,\Omega \,\lambda, \quad w(r,l) = \varepsilon \,w_0, \quad T(r,l) = T_2.$$
 (7)

In the above equations, u, v, and w are the velocity components along the  $r - , \varphi - \phi$ and z –directions, respectively. The nanofluid temperature is given by T, while the temperature of the lower and upper disks is  $T_1$ and  $T_2$ respectively. Meanwhile, ,  $Q_0$  is the heat generation/absorption coefficient, p is the pressure,  $q_r$  is the radiation heat flux, and  $\lambda$ (< 0) is the shrinking parameter.

Further,  $\mu$  is the dynamic viscosity,  $\rho$  is the density, k is the thermal conductivity, and  $\rho C_p$  is the effective heat capacity with  $C_p$  as the heat capacity at constant pressure

$$\frac{\mu_{n}}{\mu_{f}} = \frac{1}{(1-\phi)^{2.5}},$$

$$\rho_{n} = (1-\phi) \rho_{f} + \phi \rho_{s},$$

$$\frac{k_{n}}{k_{f}} = \frac{k_{s} + 2 k_{f} - 2 \phi (k_{f} - k_{s})}{k_{s} + 2 k_{f} + 2 \phi (k_{f} - k_{s})},$$

$$\left(\rho C_{p}\right)_{n} = (1-\phi) \left(\rho C_{p}\right)_{f} + \phi \left(\rho C_{p}\right)_{s}.$$
(8)

Here, the suffixes n, s, and f represent the nanofluid, nanoparticles, and base fluid, respectively. Table 1 contains the thermophysical properties of the base fluids and nanoparticles. Meanwhile, the nanoparticle volume fraction is  $\phi$ . Table 1

inermophysical properties of	water,	etnylene glycol,	$COFe_2O_4$ and	IVIN-ZNFe <sub>2</sub> O <sub>4</sub>
nanoparticles [25]				
Properties	Water	Ethylene glycol	CoFe <sub>2</sub> O <sub>4</sub>	Mn-ZnFe <sub>2</sub> O <sub>4</sub>
Thermal conductivity, $k$ [W/m K]	0.613	0.349	3.7	5
Heat capacity, $\mathit{C}_p$ [J/kg K]	4 179	2 382	700	800
Density, $\rho$ [kg/m <sup>3</sup> ]	997.1	1 116.6	4 907	4 900
Prandtl number, Pr	6.96	204	-	-

Thermonbysical properties of water ethylene glycol CoEe-O, and Mn-ZnEe-O

From the Rosseland approximation, the radiative heat flux,  $q_r$  can be expressed as follows

$$q_r = -\frac{4\sigma^*}{3k^*}\frac{\partial T^4}{\partial y},\tag{9}$$

with  $\sigma^*$  and  $k^*$  denote the constant of Stefan-Boltzmann and the coefficient of mean absorption, respectively. Using the Taylor series and ignoring higher-order terms,  $T^4$  is expanded about  $T_{\infty}$  to obtain  $T^4 \approx 4T_\infty^3 T - 3T_\infty^4$ . Then, Eq. (5) can be written as

$$u \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} = \frac{1}{\left(\rho C_p\right)_n} \left[ \left( k_n \left( \frac{1}{r} \left( \frac{\partial T}{\partial r} \right) + \frac{\partial^2 T}{\partial z^2} \right) + \frac{16 \sigma^* T_2^3}{3 k^*} \frac{\partial^2 T}{\partial z^2} \right) \right] + \frac{Q_0}{\left(\rho C_p\right)_n} \left[ (T - T_2) \theta(\eta) \right]$$
(10)

It is suitable to introduce the following similarity variables [23]

$$u = r\Omega f'(\eta), \quad v = r \Omega g(\eta), \quad w = -2 w_0 f(\eta), \quad \theta(\eta) = \frac{T - T_2}{T_1 - T_2},$$
$$p = -\frac{1}{2} \rho_f r^2 \Omega^2 A + \rho_f w_0^2 P(\eta), \quad \eta = \frac{z \Omega}{w_0},$$
(11)

where the prime denotes differentiation with respect to  $\eta$  and A is an arbitrary constant, and substituting (11) into Eqs. (2) to (4), and (10), we obtain the following ordinary (similarity) differential equations

$$\frac{1}{Re}\frac{\mu_n/\mu_f}{\rho_n/\rho_f}f'''' + 2ff''' + 2gg' = 0,$$
(13)

$$\frac{1}{Re} \frac{\mu_n / \mu_f}{\rho_n / \rho_f} g'' + 2fg' - 2gf' = 0, \tag{14}$$

$$\frac{1}{PrRe} \frac{1}{\left(\rho C_p\right)_n / \left(\rho C_p\right)_f} \left(\frac{k_n}{k_f} + \frac{4}{3} Rd\right) \theta^{\prime\prime} + 2f \theta^{\prime} + \frac{Q \theta}{\left(\rho C_p\right)_n / \left(\rho C_p\right)_f} = 0,$$
(15)

subject to the boundary conditions

$$\begin{cases} f(0) = 0, \ f'(0) = 0, \ g(0) = 0, \ \theta(0) = 1, \\ \theta(1) = 0, \ f'(1) = 0, \ g(1) = \lambda, \ f(1) = -\varepsilon/2. \end{cases}$$
(16)

Here, Pr is the Prandtl number, Re is the Reynolds number, Rd is the radiation parameter, and Q is the heat generation/absorption parameter, which are given by

$$Pr = \frac{(\mu C_p)_f}{k_f}, \quad Re = \frac{w_0^2}{\Omega v_f}, \quad Rd = \frac{4 \sigma^* T_2^3}{k_f k^*}, \quad Q = \frac{Q_0}{\Omega (\rho C_p)_f}, \quad (17)$$

where  $\nu = \mu / \rho$  is the kinematic viscosity.

#### 4. Results and Discussion

In the present study, water- and ethylene glycol-based nanofluids containing cobalt ferrite  $(CoFe_2O_4)$  and Mn-Zn ferrite (Mn-ZnFe<sub>2</sub>O<sub>4</sub>) nanoparticles are considered. Only the first solution is determined to be stable and physically significant, based on the stability analysis of multiple solutions carried out in the prior studies [26–28]. The physical quantities of interest for these nanofluids are tabulated in Table 2. As noted in Table 2, the CoFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O nanofluid produces the largest magnitude of skin friction coefficient, followed by the Mn-ZnFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O, CoFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>, and Mn- $ZnFe_2O_4/C_2H_6O_2$  nanofluids. Based on these observations, the combination of Mn-ZnFe<sub>2</sub>O<sub>4</sub> nanoparticle with  $C_2H_6O_2$  produces the most efficient nanofluid for this flow problem, as it has the lowest magnitude of skin friction coefficient and the highest heat transfer rate. Next, the axial velocity profile in Figure 2a shows that the Mn-ZnFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> nanofluid has the highest velocity near the stationary impermeable disk. However, near the permeable rotating disk, CoFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O nanofluid exhibits the highest axial velocity compared to the other nanofluids. Meanwhile, the Mn- $ZnFe_2O_4/C_2H_6O_2$  and  $CoFe_2O_4/C_2H_6O_2$  nanofluids have the highest radial velocities near the stationary and rotating disks, respectively, as shown in Figure 2b. At the same time, in Figure 2c, the Mn-ZnFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> nanofluid shows the highest tangential velocity near the stationary and rotating disks. From Figure 2d, the  $CoFe_2O_4/C_2H_6O_2$  and  $Mn-ZnFe_2O_4/H_2O$  nanofluids have the highest and lowest temperature profiles, respectively.

#### Table 2

Coefficients of skin friction (radial and tangential directions) at the lower and upper disks when  $\phi = 0.2$ ,  $\lambda = -1$ ,  $\varepsilon = 1$ , Re = 9, Rd = 0.3, and Q = 0.1

Nanofluid	$\frac{\mu_{hn}}{\mu_f}f''(0)$		$\frac{\mu_{hn}}{\mu_f}g'(0)$		$\frac{\mu_{hn}}{\mu_f}f''(1)$		$\frac{\mu_{hn}}{\mu_f}g'(1)$	
	(lower disk)		(lower disk)		(lower disk)		(upper disk)	
	First	Second	First	Second	First	Second	First	Second
	solution	solution	solution	solution	solution	solution	solution	solution
$CoFe_2O_4/H_2O$	-35.62302	-3.32474	-29.23075	1.58930	9.22210	13.75794	51.70404	-22.26607
$Mn - ZnFe_2O_4/H_2O$	-35.47872	-3.32798	-29.11240	1.59553	9.11525	13.74935	51.56424	-22.28368
$CoFe_2O_4/C_2H_6O_2$	-21.53147	-3.67576	-17.68497	2.23249	2.94548	13.12263	37.10216	-24.34233
$Mn - ZnFe_2O_4/C_2H_6O_2$	-21.37439	-3.68210	-17.55654	2.24338	2.92835	13.11506	36.91246	-24.38100



**Fig. 2.** Profiles of (a) axial velocity, (b) radial velocity, (c) tangential velocity, and (d) temperature for various nanofluid when  $\phi = 0.2$ ,  $\lambda = -1$ ,  $\varepsilon = 1$ , Re = 9, Rd = 0.3, and Q = 0.1

# 5. Conclusions

The nanofluid flow between a nonpermeable stationary disk and a rotating permeable shrinking disk is scrutinised in this study. Various nanofluids such as the CoFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O, Mn-ZnFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O, CoFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>, and Mn-ZnFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> are considered as the working fluid in this flow problem. Dual solutions are generated from numerical computation. The combination Mn-ZnFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> nanofluid has the lowest magnitude of skin friction coefficient and the highest heat transfer rate. The temperature profile of the ethylene-glycol-based nanofluids (*i.e.*, CoFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub> and Mn-ZnFe<sub>2</sub>O<sub>4</sub>/H<sub>2</sub>O and Mn-ZnFe<sub>2</sub>O<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>).

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