



Influence of Environment-Friendly Fuel Additives and Fuel Injection Pressure on Soot Nanoparticles Characteristics and Engine Performance, and NO_x Emissions in CI Diesel Engine

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ABSTRACT

Next generation of fuels and injection technology system are growing attention in the transportation sector. The effects of castor oil of biodiesel (C30D) and two conditions (500 bar and 1000 bar) of fuel injection pressure (FIP) on soot nanoparticles characteristics and NO_x emissions were performed in a direct injection (DI) diesel engine. The results showed that size distributions of soot particulate decreased from C30D combustion by 43.62% compared to the diesel combustion for different FIP. Furthermore, the soot particle number concentration decreased more with 1000 bar of FIP compared with 500 bar for both fuels tests. The combustion of C30D decreased the average number of primary particles (n_{po}) by 44.35% compared with diesel. For an injection pressure, it was observed that high injection pressure (1000 bar) significantly decreased the n_{po} by 11.6 nm and 25.4 nm compared to the 500 bar by 22.4 nm and 33.2 from C30D and diesel, respectively. In addition, the average diameter of soot primary particle (d_{po}) was smaller by 47.68% during C30D combustion than to the diesel combustion for all conditions of injection pressure. In case of engine performance, the BTE, BSFC increased from the C30D combustion compared with diesel under different FIP. It is indicated that increasing injection pressure improved the engine performance for C30D and diesel. In contrast, the high injection pressure and C30D increased the NO_x emissions by 21.37% compared with diesel fuel.

1. Introduction

The objectives of the world are substituting fossil fuels by alternative fuels to reducing the pollutant emissions to meet the standard emissions regulations. It well known that the compression ignition (CI) engine produces high level of soot and NO_x emissions that effect on both environment and health [1]. To confront technology, climate, and renewability challenges, different blends of fuels derived from a large variety of feedstock will be available in the future such as biodiesel-diesel blends and alcohol-diesel blends. Recently, the world's depending on use of biodiesel as alternative to conventional petroleum resources due to its environmentally friendly solution, positive health

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effects, and increasing popularity of alternative fuels [2,3]. It is reported that co-firing palm oil waste with coal can reduce the SO_x, NO_x, and greenhouse gas [4]. Also, it is considered a cost-effective option with the rapid depletion of fossil fuel reserves over the world. The effects of alternative fuels on performance and emissions of diesel engines have been extensively reviewed in previous studies [5,6]. In terms of emissions, stringent environmental regulations increased on NO_x and PM encourage the authors to develop the new generation fuels. Therefore, many studies have been documented on results of NO_x and PM emitted from the oxygenated fuels combustion in diesel engines [7,8]. Zulkurnai *et al.*, [9] stated that the NO_x and soot decreased from combustion of ethanol-diesel blend which contribute in better engine performance and better environmental future. Most of studies reported that the soot emissions decreased as the percentage of biodiesel content increased in the fuel-blend [10]. PM emissions decreased by 73–83% from the combustion of three pure methyl esters such as methyl-palmitate, methyl-oleate, and methyl-laurate compared with diesel fuel combustion as presented in Knothe *et al.*, [11]. They found that this trend due to the absence of aromatic compounds in biodiesel compared to those present in diesel fuel. The impacts of alternative fuels formulation on soot characteristics were investigated, especially for soybean-derived biodiesel and alcohol-diesel blends [12]. They suggested that the important factor influencing the oxidation rate is surface oxygen content. The oxidative reactivity of soot and combustion process are affected by the fuel composition and the engine operating parameters [13]. In single-cylinder diesel engine, different ethanol percentages generated the soot particles with a similar nanostructure compared to the diesel soot. It was found that the oxygenated fuels increase the soot reactivity of particulate matter (PM) at high concentration of oxygen content in fuel properties [14]. In addition, higher active surface area of soot particles was observed during the combustion of alcohol-diesel blends [15]. The sooting propensities of hydrocarbon fuels have been studied by Westbrook *et al.*, [16] for oxygenated fuel additives. It was found that the sooting propensity decreased from the oxygenated functional groups (ethers, esters, and alcohols). The effect of adding oxygenates into the fuel on the suppression of the sooting propensity has been modelled by Westbrook *et al.*, [16] in diesel engines. The soot formation can be initiated due to the lack of oxygen in the fuel-rich premixed flame ignition followed by quenching. It is reported that the high injection pressure increases the oxidation rate of soot particles and promotes the soot reactivity [17]. Prior works have reported that oxygenated fuels (i.e., fuel-bonded oxygen) decreased the soot emissions and improved the combustion characteristics [18]. It is reported that the soot particles have different oxidative reactivity and nanostructural order from the combustion of acetylene, Benzene, and ethanol [19]. More reactive and a more amorphous structure of soot particles were found from Benzene compared with acetylene. It is stated that the soot particles formed as aggregate structures or single particles according to the images of transmission electron microscopy (TEM) [20]. The morphological properties of soot particles are diameter of primary particles (n_{po}), number of primary particles (n_{po}) and size of primary particles (d_{po}). In previous work, it was observed that using a bioethanol-diesel blend can decrease the PM in a diesel engine. This trend is related to the various factors of fuel properties such as reduced aromatic content, fuel-borne oxygen, and lower fuel C/H mass ratio. As shown in the literature, the nanostructure of soot particles depends on the residence time and temperature [21]. At high temperature, the size of soot particles decreased because of the higher rate of soot particles oxidation [22]. It is stated that the soot aggregate sizes and spherule sizes increased during the high condition of engine conditions of exhaust temperature and engine load. Due to the shorter residence time of particle surface growth, the size of soot particles is smaller under higher engine speed [23]. The engine parameters of injection pressure, temperature, engine load and speed, and injection timing are effects on soot formation [24]. It is reported that FIP is an important parameter of engine operating conditions that affects soot emissions and engine

performance [25]. Increasing FIP and using alternative fuels are a good way to inhibit the soot formation and reduce engine emissions in diesel engine [26,27]. Agarwal *et al.*, [27] stated that the smaller size of PM is more harmful for human health and environment. Harris and Maricq [28] reported that the large soot particles decreased with increasing FIP. To comply with the stringent global emission, FIP is efficient ways to achieve these requirements. High fuel injection pressures can reduce the PM emissions and keep NO_x emissions in moderate level [29]. It is reported that combination of high injection pressure and biodiesel leads produce lower level of smoke opacity and engine emissions [26,30]. The complicated nature of soot particles formation leads to more studies about the characteristics of soot particles. The details of the combined effect of alternative fuel and injection pressure on the soot emissions in the literature were much more limited. Therefore, the present work addresses the impacts of alternative fuel additives on characteristics of soot nanoparticles and engine performance in CI diesel engine. Furthermore, study the effect of fuel injection pressure (FIP) on the soot nanoparticles characteristics (n_{po} and d_{po}) for all fuels tests.

2. Experimental

2.1 Engine Setup

During experiments, four-cylinder, direct injection diesel engine was employed as shown in Figure 1. Table 1 listed the main characteristics of the research engine. To generate load, eddy current dynamometer was used by equipped with engine. LabView program was used to manage the time-based data acquisition. A series of National Instruments FieldPoint modules were used to read the analog signals from thermocouples, pressure transducers, and emissions data. In each test, the FieldPoint modules is collecting the data every 1 s during a 3-min period. The pressure transducers (AVL GU12P) were used to measure the pressure traces. The signal from the pressure transducers was amplified using Kistler type 5010. At a resolution of 0.1 crank angle degrees, the traces of pressure were recorded and averaged over 200 cycles. The data of pressure trace was used to calculate the ROHR using a thermodynamic diagnostic model.

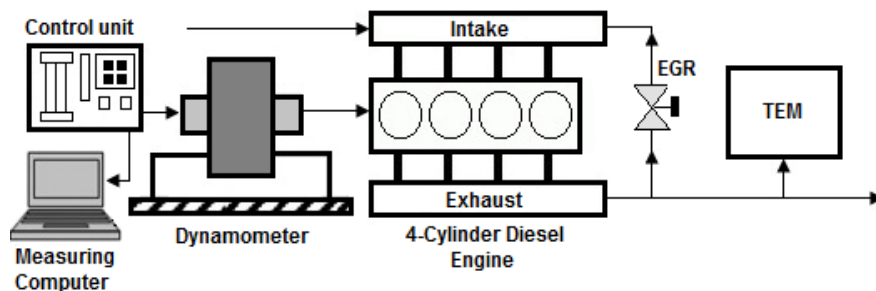


Fig. 1. Schematic of the experimental installation

Table 1
 Characteristics of diesel engine

Parameters	Specifications
Engine type	Diesel engine
Cylinders number	4
Bore (mm)	84
Stroke (mm)	90
Rod length (mm)	162
Compression ratio	16.1
Displacement (cc)	499
Engine speed range (rpm)	2000
Maximum rated torque	320 Nm at 1800 min ⁻¹

2.2 Test Fuels and Equipment

In the current work, three different fuels were used to produce a variety of soot emissions in the exhaust. The baseline fuel and alternative fuel were diesel fuel and ethanol-blend, respectively. The biodiesel is produced from the castor oil as renewable sources. The fuel blend is prepared by mixing 70% of diesel and 30% of castor oil (C30D). The property information and specifications of tests fuels were listed in Table 2. The water-cooling system was used to control and monitor the fuel temperature for all fuels tests. The exhaust gas emissions analyser (type AVL 444) with recording software was used to measure the engine emissions (NO_x). The soot nanoparticles characteristics were investigated using a 200-kV field-emission transmission electron microscopy (TEM). The high-resolution bright images of soot nanoparticles were taken by TEM. At high magnification (500,000) of TEM has been adjusted for all images of soot samples. The ultrasonically was used to disperse soot samples soot samples for 60 min [31]. This method was used by Al-Qurashi and Boehman [32]. Matlab software was used to analyse the characteristics of soot particles [20]. The engine operating conditions were 1800 rpm, 4 bar, for engine speed and IMEP, respectively. The FIP was 550 bar and 1000 bar to study the effect of fuel formulation and injection strategy on the soot nanoparticles characteristics of diesel engine.

Table 2
Properties of diesel fuel and C30D

Properties	Diesel	C30D
Cetane Number	53.2	-
Bulk Modulus (MPa)	1410	1564
Density at 15 °C (kg/m^3)	824.1	864.2
Kinematic Viscosity at 40 °C (cSt)	2.7	4.26
Lower Calorific Value (MJ/kg)	42.11	40.73
Upper heating value (MJ/kg)	44.5	43.62
Lubricity at 60 °C (μm)	312	202
C (wt%)	87.24	81.13
H (wt%)	14.86	12.87
O (wt%)	0	5.16
90% Distillation (°C)	329	342

3. Results and Discussion

3.1 Size Distribution of Soot Particulate

The size distributions of soot particulate are measured for C30D and diesel under 500 bar and 1000 bar of FIP as shown in Figure 2. It can be seen that soot particle number concentration decreased with high injection pressure for C30D and diesel fuel. This could have been due to the enhance air-fuel mixing and smaller droplet of fuel that causes a better oxidation rate of soot particulate. These results are agreement with previous studies [33,34]. A comparison of fuels, it can be observed that the size distribution of soot particles decreased from C30D combustion by 43.62% compared to the diesel as depicted in Figure 2. Furthermore, the distributions were displaced towards lower diameter values and decreased and the total concentration of particulate decreased during the combustion of C30D compared with the diesel. It is suggested that the higher viscosity and higher oxygen content of C30D could be effect on particle number concentration [35]. Saxena *et al.*, [36] reported that the biodiesel decreased the total particle number concentration compared to the conventional diesel fuel. Also, lower particle number concentration (38%) produced from biodiesel compared to the diesel [37]. The combustion of C30D decreased the size distribution of soot particles

for both conditions of FIP compared with diesel. In addition, the soot precursor species production can be reduced depending on the ester structure of castor oil [38]. Figure 2 show that the high injection pressure and higher viscosity of biodiesel and lead to better fuel atomization, which decreased the total number of soot particles. Fayad [12] reported that the insufficient oxygen to burn the fuel and fuel-rich premixed ignition are promote the soot formation during the combustion process. The better fuel atomization and spray characteristics with high injection pressure and higher density of C30D could be decrease the particle number emission [39,40]. It can be observed that the size distribution of soot particulate shifted to the nucleation mode with 1000 bar compared with 500 bar (accumulation mode) as shown in Figure 2.

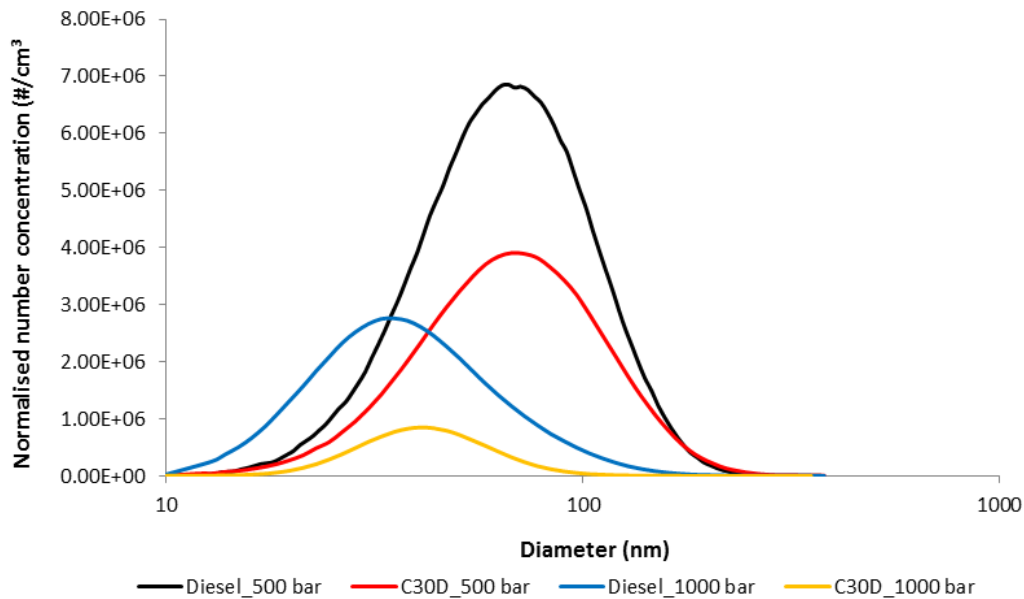


Fig. 2. Effect of FIP and C30D on size distribution of soot nanoparticles

3.2 Number of Soot Primary Particle (n_{po})

Figure 3 presents the effect of C30D and different fuel injection pressures on number of primary particle (n_{po}). The results from this figure show that the C30D combustion decreased the number of primary particles (n_{po}) compared with diesel combustion. Figure 5 gives general characteristics of soot agglomeration can be measured through analysis TEM images. The average number of primary particles decreased from C30D combustion by 44.35% compared with diesel for different FIP. The oxygen content in C30D and incorporation of the injection pressure leads to boost the oxidation rate of soot particles result in decreasing the total number of particulates. In addition, the effective combustion of C30D has high potential in reducing the number of soot primary particle by increasing the oxidation rate during the combustion. From the literatures, it was found that oxygen-born in the biodiesel contributes in more complete combustion and decrease the soot particles number because the available oxygen in the combustion region [41,42]. Furthermore, the reduction in number of particles could be due to the decrease the collisions of soot particles and more aggregation. The increase FIP of 1000 bar inhibited n_{po} by 11.6 nm and 25.4 nm compared with 500 bar by 22.4 nm and 33.2 from C30D and diesel, respectively, as shown in Figure 3. It is thought that FIP associated with decreases the resident time for soot formation and decreases the soot precursors formation into the cylinder [13,43].

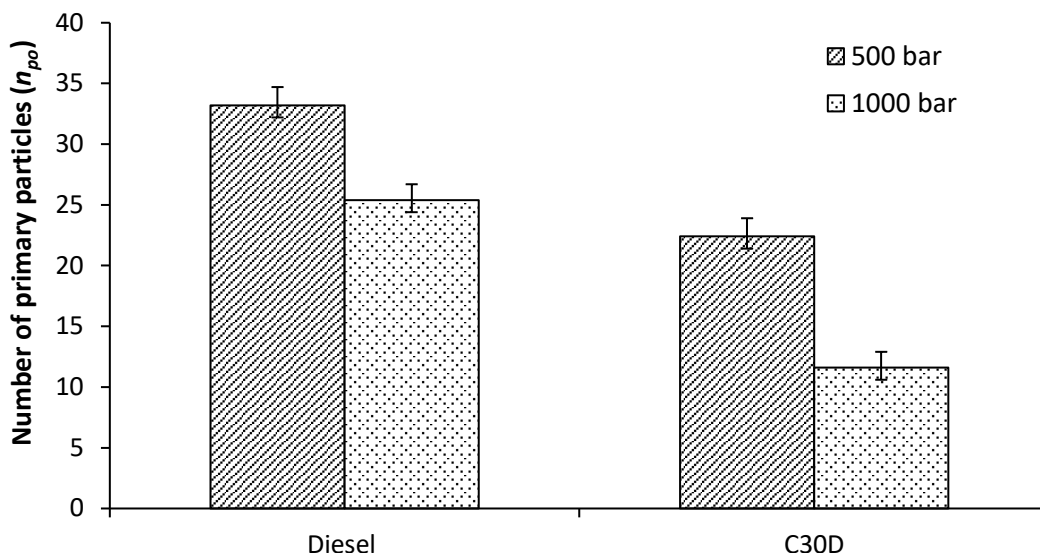


Fig. 3. Effect of FIP and C30D on number of primary particles n_{po}

3.3 Diameter of Soot Primary Particles (d_{po})

It is well known that the important parameter to evaluate health and environmental effects is size of soot particles [44]. The smaller size of soot particles is more potentially be suspended a longer time in the air, while the larger size of soot particles is more reactive. Thus, these smaller particles can penetrate into the alveolar regions and bronchi. The results of d_{po} were found according to the TEM images in Figure 5 using Matlab code. The diameter of soot primary particles (d_{po}) from combustion of C30D and diesel is shown in Figure 4 for different FIP. According to the Figure 4, the C30D decreased the average d_{po} by 47.68% compared with diesel for both conditions of FIP. The main reasons for that are lower rate of soot production, soot growth, and soot formation as well as enhance the oxidation rate of soot particles during the combustion of C30D. These results are highly similar with results obtained by previous studies for biodiesel and butanol blends [12,20,45,46]. It can be observed that the increasing the injection pressure decreased the average d_{po} compared for both fuels (Figure 4). The shorten time of soot growth and improved soot oxidation rate (high combustion temperature) under high FIP leads to produce smaller d_{po} during the combustion process.

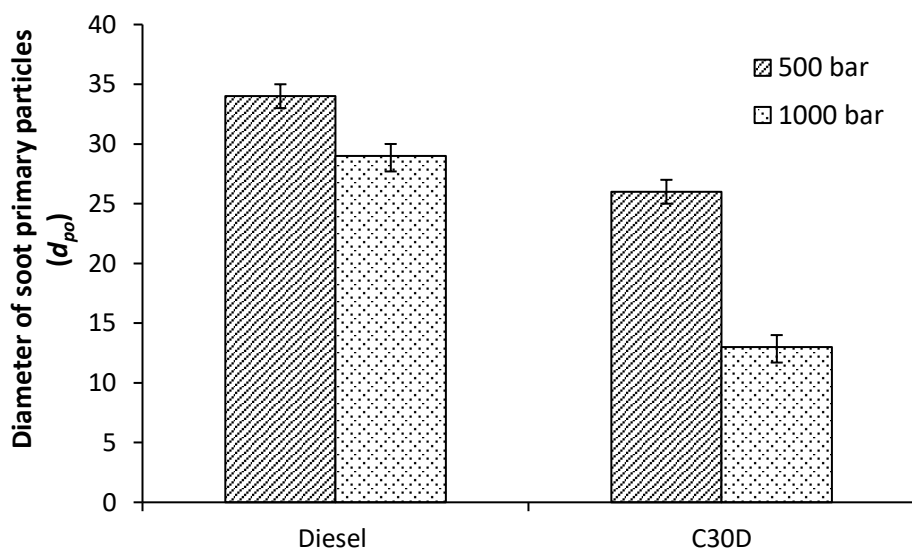


Fig. 4. Effect of FIP and C30D on diameter of primary particles d_{po}

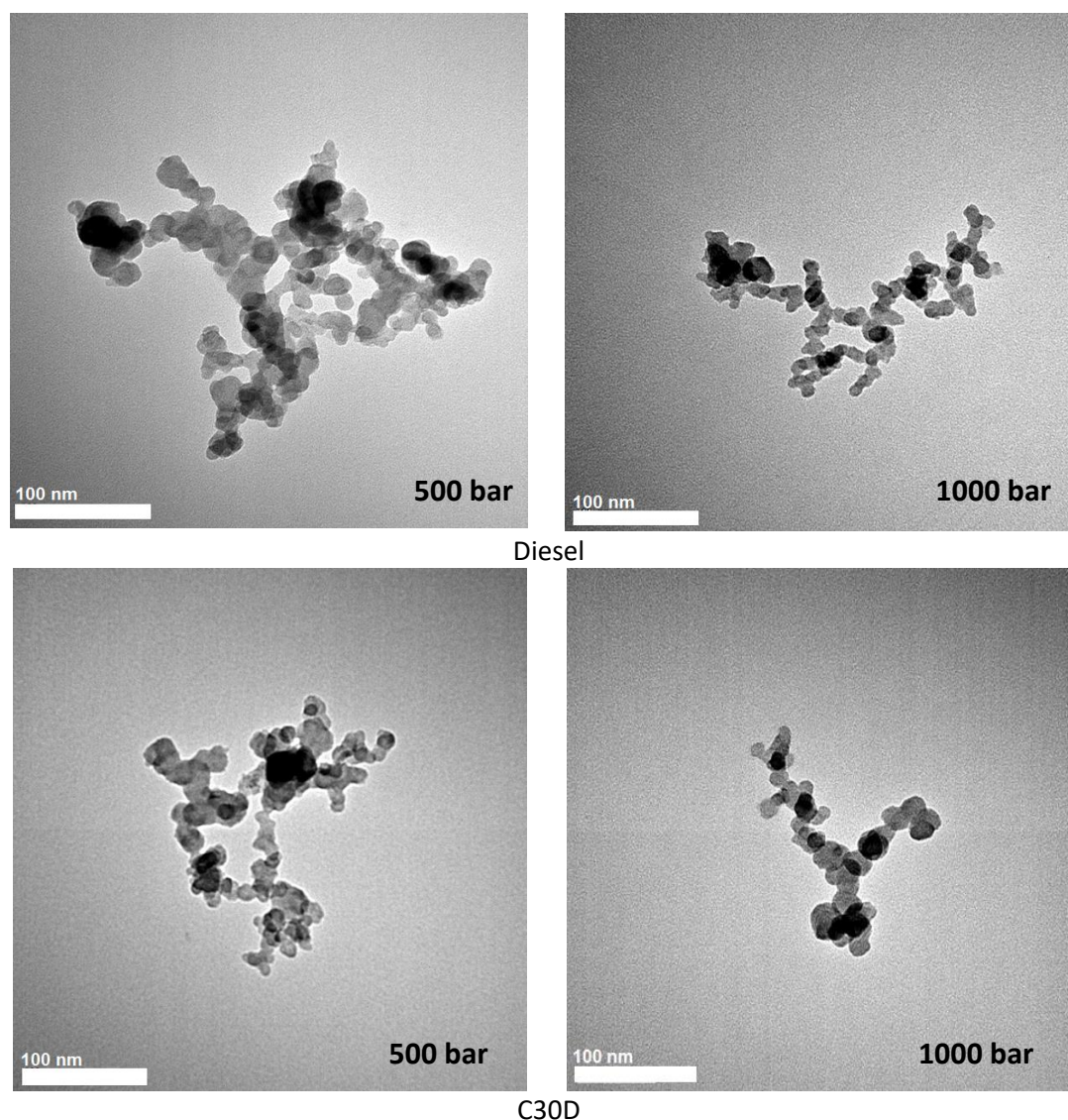


Fig. 5. Soot agglomerates images for diesel fuel and C30D under 500 bar and 1000 bar of injection pressure

3.4 Brake Thermal Efficiency and Brake Specific Fuel Consumption

The effects of C30D and FIP on BTE are shown in Figure 6. It can be found that the BTE increased during the combustion of C30D by 32.5% compared with diesel by 30.4% for different FIP. The higher oxygen content of C30D compared with diesel causes complete combustion which improves the thermal efficiency. It is reported that the BSFC and LHV are a function of improve the thermal efficiency [12,47]. Also, it is mentioned that BTE increased with increasing the biodiesel in the fuel blend due to increase the oxygen content in the fuel blend [48]. The combustion efficiency increased from these effects. In case of injection pressure, the increasing FIP slightly improve the BTE for both fuels. Furthermore, the BTE increased with 1000 bar by 34.3% and 32.6% compared with 500 bar by 30.7% and 28.8% for C30D and diesel fuel, respectively.

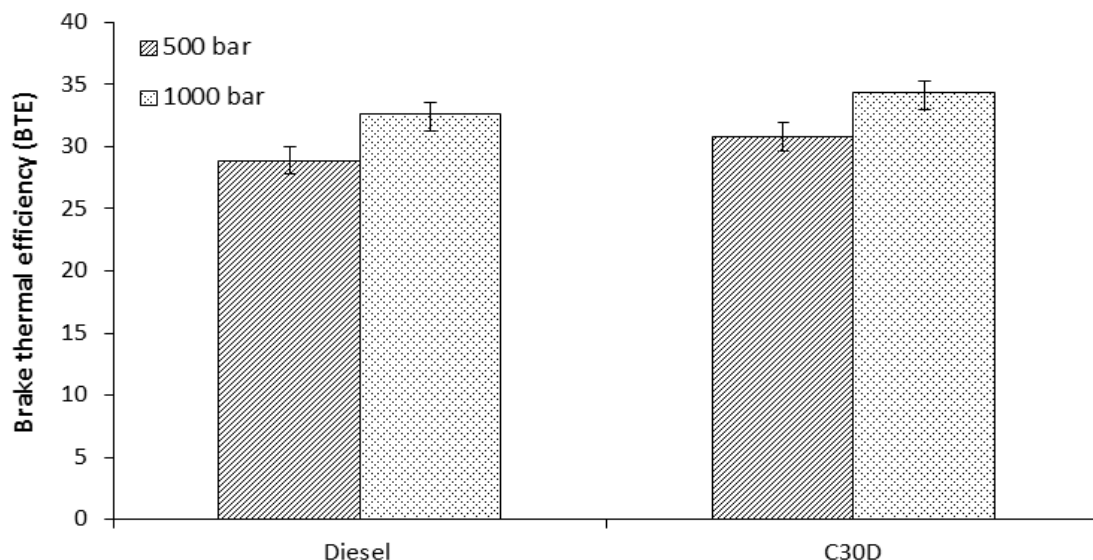


Fig. 6. Effect of FIP and C30D on brake thermal efficiency (BTE)

The influences of C30D and FIP on the BSFC are presented in Figure 7. It can be seen that the C30D combustion increase the BSFC compared diesel for 500 bar and 1000 bar of injection pressure. The lower heating value and calorific Value of C30D lead to increase the BSFC, which is consistent with previous study [13]. In addition, similar results were found by other authors [49,50]. For all fuels, the similar trend was observed with FIP as shown in Figure 7. Furthermore, it can be noticed that the BSFC decreased with 1000 bar of fuel injection pressure compared with 500 bar for both fuels. The smaller fuel particle diameters and slight delay admission during the combustion result in decrease the BSFC [47]. At higher FIP, the BSFC decreased due to the better fuel atomization and lesser fuel going to cylinder [51]. On the other hand, longer ignition delay and enlarge of fuel particle diameter with 500 bar of FIP causes higher BSFC. The values of BSFC decreased by 0.2348 kg/kW h and 0.21485 kg/kW h for 1000 bar and increased by 0.2948 kg/kW h and 0.2549 kg/kW h during the combustion of C30D and diesel, respectively.

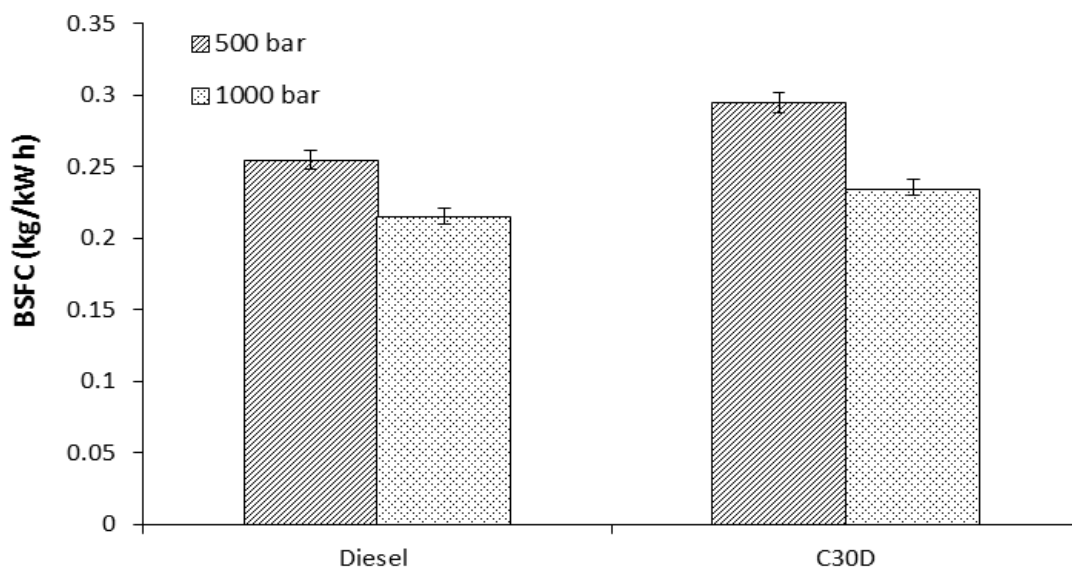


Fig. 7. Effect of FIP and C30D on brake specific fuel consumption (BSFC)

3.4 Exhaust Gas Temperature (EGT)

Figure 8 depicts the effect of C30D and diesel fuel on EGT for 500 bar and 1000 bar of FIP. As observed in this figure, the EGT increased from the combustion of C30D and diesel with increasing the FIP. This could be due to the faster combustion rates from increasing the FIP which result in an increase the EGT (Figure 8) [13]. A comparison of fuels, the EGT significantly increased during the C30D combustion compared with diesel for variable FIP as presented in Figure 8. The EGT was enhanced due to the presence oxygen-born in castor oil properties (Table 2) which improved the combustion temperature and pressure [20,52]. The mixture of fuel–air could be improved due to increasing the injection pressure from 500 bar to the 1000 bar, which in turn leads to complete combustion [53]. In addition, high injection pressure produces smaller droplets of fuels and enhances the fuel distribution to reach the better combustion.

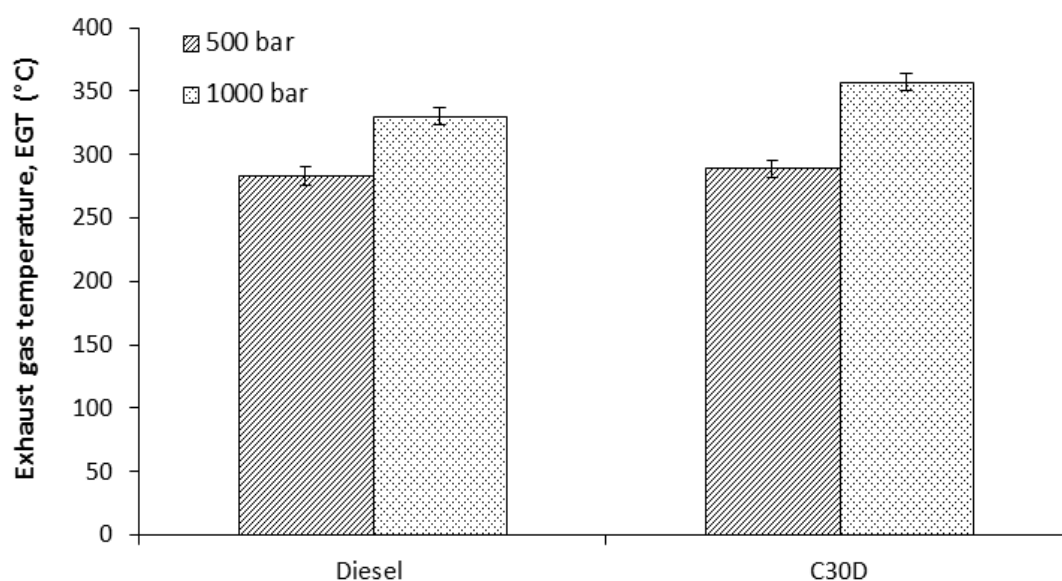


Fig. 8. Effect of fuel injection pressure and C30D on exhaust gas temperature (EGT)

Figure 9 shows the results of NO_x emissions for C30D and diesel under both conditions of FIP. In general, the NO_x emissions for C30D and diesel with increasing the FIP as presented in Figure 9. This is due to increase the combustion temperature (Figure 8) with high injection pressure, as a consequence starts NO_x emissions increase [26]. The fuel particle diameter decreased with high FIP result in an increase of combustion temperature, which in turn increases the NO_x formation. For both FIP, the NO_x emissions increased during the combustion of C30D by 17.62% than to the diesel (Figure 7). This could have been due to the oxygen content in C30D that enhance the formation of NO_x emissions [54,55]. Prior work reported that the chemically bound oxygen content in oxygenated fuels promote the NO_x formation [56]. The current results are agreement with previous experimental studies that cited in the introduction and results.

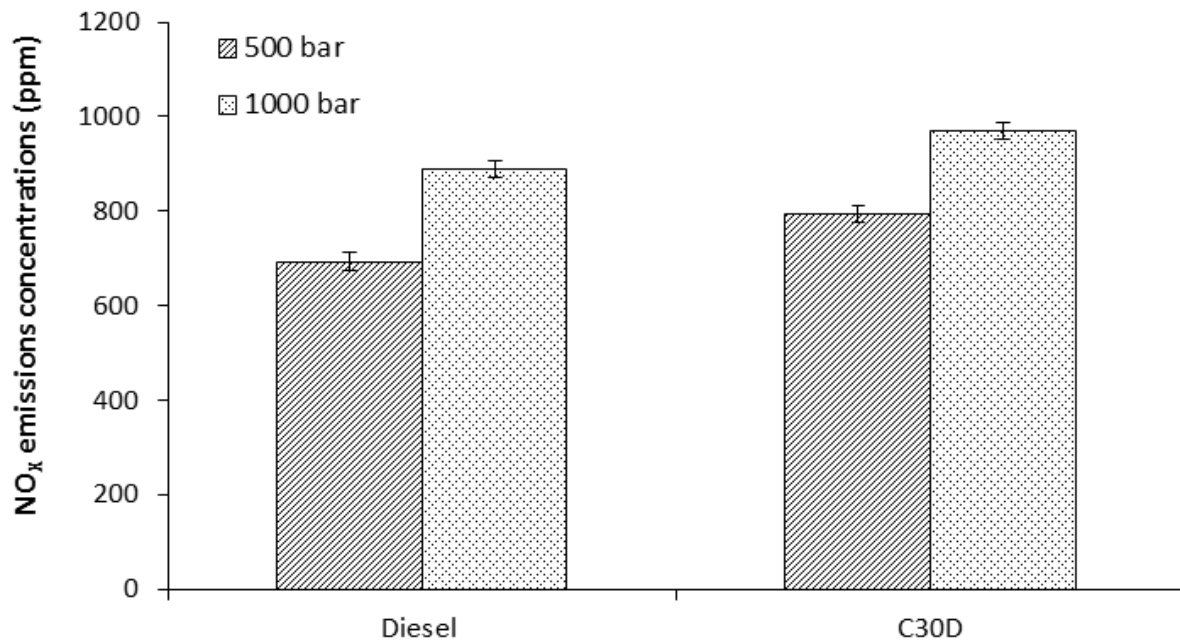


Fig. 9. Effect of FIP and C30D on NO_x emissions

4. Conclusions

The influences of C30D and fuel injection pressures of DI diesel engine on soot nanoparticles characteristics and NO_x emissions were experimentally investigated in this study. The main conclusions of this experimental research were summarized as follows

- i. It can be concluded that the characteristics of soot nanoparticles decreased from C30D combustion compared to the diesel for different conditions of FIP.
- ii. The oxygen content in C30D contributes in a significant reduction in size distribution of soot particles by 43.62% compared to the diesel under 500 bar and 1000 bar of FIP.
- iii. For both FIP, it was observed that the n_{po} and d_{po} decreased by 44.35% and 47.68% during the combustion of C30D compared to the diesel, respectively.
- iv. The high FIP of 1000 bar decreased the soot characteristics of n_{po} (by 11.6 nm and 25.4 nm) and d_{po} (by 13 and 29) for C30D and diesel, respectively.
- v. It was found that BTE and BSFC increased from C30D combustion compared diesel, while high injection pressure improves the fuel economy and thermal efficiency for both fuels.
- vi. The NO_x emissions slightly increased 17.62% from C30D combustion compared diesel for 500 bar and 1000 bar of FIP.
- vii. The effects of C30D and high injection pressure were decreased the soot nanoparticles characteristics and improves the engine performance.
- viii. It was found that these results will be beneficial for improve the efficiency of aftertreatment catalyst in diesel engines.

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