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Heat Transfer in Hartmann Flow of Hybrid Nano-Jeffrey Fluid with Heat Absorption and Thermal Radiation Impact

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ABSTRACT

In this study, we examine how heat radiation and absorption affect the flow of Jeffrey fluid across an infinite vertical plate in an unsteady magnetohydrodynamic (MHD) free convection flow. We use alumina (Al_2O_3) and copper (Cu) nanoparticles in water assuming it as a base fluid. The problem is solved, and exact solutions are obtained using the Laplace transform method. For embedded parameters like radiation parameter, heat absorption parameter, Hartmann number, Grashof number, material parameter of Jeffrey fluid, volume fraction of hybrid nanofluid, time, and Prandtl number, results of velocity and temperature distributions are visually displayed. It is clear from the results that while raising the heat absorption parameter and Prandtl number causes a decrease in the velocity and temperature profiles whereas increasing radiation parameter and Grashof Number increases the hybrid nanofluid velocity. The resulting analytical solution is then verified by comparing it to the results of the earlier investigation and is determined to be in excellent accord. This outcome may be used in a number of nanofluid cooling systems. This research might serve as a reference for other numerical and experimental studies as well as a manual for several industries because the answers are established in an analytical form.

1. Introduction

Due to the limited capabilities of conventional base fluids like ethylene glycol, engine oil, and water, are not sufficient to address today's needs, thus, an advanced form of high-potential heat transport fluid namely nanofluid is introduced and launched in the industrial area. Nanofluid is formed by adding some nanoparticles whose size of less than 100 nm in conventional base fluids [1]. Nanofluid shows better performance in heat transfer than regular fluids. Many investigations on nanofluid flow with various physical situations have been done by several authors; Hanif [2], Hanif

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and Shafie [3,4], Saeed *et al.*, [5], Sharma *et al.*, [6,7], and Mishra *et al.*, [8]. A major requirement for today's industry is the existence of systems or applications that allow heat transfer to occur more quickly. A lot of articles report that new hybrid nanoparticles may enhance the heat transfer rate compared to regular nanofluid [9]. The special behaviors of the hybrid nanofluid are its thermal conductivity and viscosity increase with increasing particle concentration in the base fluids. In recent years, hybrid nanofluids gained great importance in several industrial and technological processes such as electronic cooling, transportation, solar energy, automobiles, smart computers, catalysis, microfluidics, and biomedicine [10-13]. Driven by these important applications, many studies have been performed to analyze the boundary layer flow of a hybrid nanofluid. Salleh *et al.*, [14] examined the stability of the dual solutions obtained for the hybrid nanofluid flow past a moving thin needle. Hussain *et al.*, [15] performed the flow of a hybrid nanofluid in the presence of the convective condition using an exponentially stretchable rotating surface. The influence of Friedrich shear stress, hybrid nanoparticles, and Cattaneo heat flux on the characteristic of the flow and heat transfer of Maxwell hybrid nanofluid is studied by Hanif and Shafie [16]. Later, Dinarvand *et al.*, [17] carried out an analysis of mixed convection flow over a shrinking and porous surface of thermomicro-polar silver and graphene nanoparticles using the mass-based hybrid nanofluid model. A considerable amount of previous research on hybrid nanofluid under various situations has been successfully reported [18-24].

The main concern in the study of non-Newtonian fluids in the last few years is due to their practical usage in industry and technology. Several examples of non-Newtonian fluids are blood, dilute polymer solution, honey, gel, and many others. The main aspect of non-Newtonian fluid's importance is that it possesses nonlinear rheological properties [25-27]. Since many applications (geophysics, bioscience, cosmetics, drying of paper, food processing, chemical plastic production, and petroleum industries) involved rheological problems, many flow models have been proposed to interpret non-Newtonian fluids' behaviour [28,29]. The best solution to interpret that behaviour is by using the Jeffrey fluid model due to its simplicity. Among the non-Newtonian fluid models, the Jeffrey fluid model is often used because its constitutive equations can be reduced to the Newtonian model as a special case. Jeffrey fluid can describe the stress relaxation properties and relaxation time of non-Newtonian fluids, which normal fluids cannot describe. In recent years, many authors have investigated several studies of the Jeffrey fluid under different conditions. For instance, Sharma *et al.*, [30] analyzed the electromagnetohydrodynamic Jeffrey fluid flow past a vertical nonlinear stretching surface of variable thickness. In their study, they analyzed the effects of heat and mass transfer by using several source terms namely, thermophoresis, Brownian motion, Ohmic heating, viscous dissipation, exponential heat source, thermal heat source, and activation energy. Awais *et al.*, [31] investigated the impact of Hall current on magnetohydrodynamic flow with Jeffrey fluid adjacent to a nonlinear stretching plate with variable thickness. Hussain *et al.*, [32] carried out an investigation to analyse the Cattaneo–Christov heat flux in Jeffrey fluid flow in the presence of a heat source past a stretchable cylinder. They conclude that higher values of Deborah number in terms of relaxation time and ratio parameter diminishes the magnitude of the drag coefficient, while the opposite effect is noticed for larger Deborah number in terms of retardation time and curvature parameter. Recently, Kumar *et al.*, [33] analyzed the effects of Joule heating, viscous dissipation, exponential heat source, and Arrhenius activation energy on an electromagnetohydrodynamic Cu-polyvinyl alcohol/water Jeffrey nanofluid flow. It is found that the heat transfer rate augments with an increase in the thermophoresis diffusion and electric field parameters, while it diminishes with an increase in an exponential heat source parameter. More articles on Jeffrey fluid flow are available in the recent literature [34-36].

The consideration of the magnetic field in the flow plays a significant role in various fields such as medical, chemical, biological, and mechanical. For example, magnetohydrodynamics (MHD) power generators, MHD flow meters, loudspeaker fabrication, sink-float separation, magnetic resonance image, device sterilization, sealing of materials, and granular insulation. In the area of medicine, magnets are used to create three-dimensional images of diagnostic and anatomical importance from nuclear magnetic resonance signals. Due to these important applications, a lot of research has been done by many authors. Krishna *et al.*, [37] studied the peristaltic magnetohydrodynamic flow of a Jeffrey fluid past a porous medium in a vertical echelon by considering the impact of uniform transverse magnetic field as well as Hall current. A year later, Krishna *et al.*, [38] furthered their study by examining the influence of Joule, Soret, and Hall currents on MHD rotating mixed convection flow adjacent to an infinite porous surface. Inspired by the previously published paper, a lot of investigations have been carried out to focus on the magnetohydrodynamic [39-42]. Very recently, Reddy *et al.*, [43] examined the influence of the porosity on unsteady MHD mixed convection stagnation point flow with radiation and viscous dissipation, meanwhile, Sharma *et al.*, [44] analyzed the influence of porosity, radiation, and viscous dissipation on unsteady MHD mixed convection flow at the stagnation point.

Other than that, the researchers are devoted to discovering new energy technologies and energy resources. The analysis of radiative heat flux is highly important in space technology and processes that demand high temperatures [45]. There are numerous applications of radiation effects such as electricity generation, astrophysical flows, and solar power technologies. The consideration of radiation in the energy equation leads to a highly nonlinear partial differential equation. A lot of research has been conducted to analyze the radiation effect on the flow. Roşca *et al.*, [46] discussed the theoretical and numerical outcomes for an axisymmetric hybrid nanofluid flow under the influence of radiation past a stretching/shrinking plate. It is noticed from their study that the addition of radiation effect enhances the fluid temperature. The variation of the energy dissipation, diameter of nanoparticles, and mass flux caused by the temperature gradient in convective radiation of the fluid, Darcy-Forchheimer model, and heat source has been investigated by Ali *et al.*, [47] considering cylindrical surface. Besides that, Bejawada *et al.*, [48] examined computationally the effect of thermal radiation, heat source and chemical reaction on magnetohydrodynamic Casson fluid flow with velocity slip past a nonlinear inclined stretchable sheet in a Forchheimer porous medium. They noted that the presence of radiation in the flow decreases the plate temperature. Recently, several researchers have conducted various versions of these effects on flow fields [49-53].

From the published literature it is found that no study on Jeffrey nanofluid with hybrid nanoparticles is performed under the imposed constraints. Hence to fill this gap, this study is carried out. More exactly, in this work we have explored the analytical solutions of MHD Jeffrey hybrid nanofluid flow under the effects of thermal radiation, heat absorption, and magnetic field. Two different kinds of nanoparticles, namely, alumina and copper are taken into consideration. To the best of knowledge, this problem has not been reported in recent literature yet. Further studies on this topic should be conducted by more researchers. In this work, a set of appropriate dimensionless variables are applied to reduce the partial differential equations into a non-dimensional form. The analytical solutions for these governing equations are computed by the Laplace transform method. Some interesting results of velocity and temperature fields for various pertinent parameters are analyzed through plots with the help of MATHCAD software. The limiting cases are also provided to validate the present work.

2. Mathematical Formulation

Consider the unsteady free convection flow of incompressible Jeffrey hybrid nanofluid past an infinite vertical plate with constant temperature. The vertical plate serves as the x –axis and y –axis is chosen to be normal to it. This problem is modelled under the following assumptions [31,54-56]:

- i. The fluid is assumed electrically conducting under influence of uniform transverse magnetic field of strength B_0 applied parallel to y –axis as shown in Figure 1.
- ii. The low magnetic Reynolds number is taken, so that the effect of induced magnetic field can be neglected.
- iii. It is also assumed that the external electric field is negligible due to the fact that zero applied and polarization voltage.
- iv. Initially, at time $t \leq 0$, the plate and the fluid are at rest to a constant free stream temperature, T_∞ .
- v. At time $t > 0$ the temperature of the plate is raised or lowered to a constant temperature, T_w .
- vi. The hybrid nanofluid flow phenomena are described using the Jeffrey fluid model. Additionally, the effects of heat absorption and thermal radiation are accounted in the energy equation.
- vii. The nanoparticles are restricted to spherical shape and uniform size.
- viii. Both nanoparticles and base fluid are considered in a stable condition with the same velocity flow.

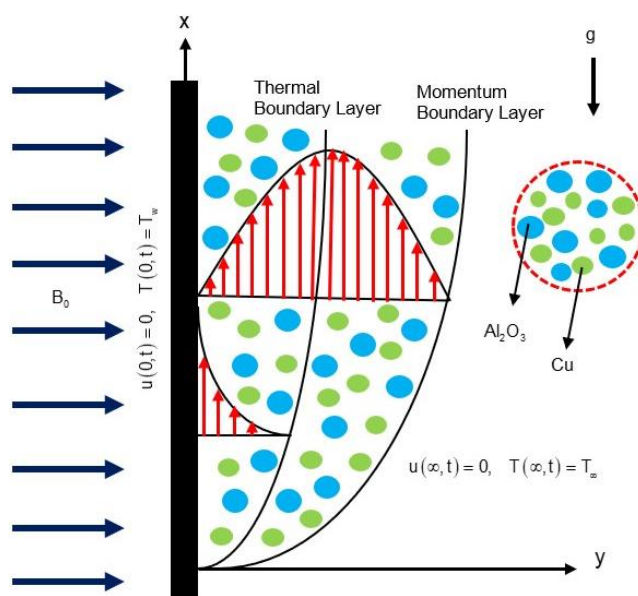


Fig. 1. Schematic diagram of Jeffrey hybrid nanofluid past an infinite vertical plate

Based on the above proposed assumptions and using the Boussinesq approximation, the governing equations of momentum and energy equations for unsteady free convection flow of hybrid nano-Jeffrey fluid adherence to Tiwari and Das Model past an infinite vertical plate with the impact of thermal radiation and heat absorption can be expressed as [57-62]:

$$\rho_{hnf} \frac{\partial u}{\partial t} = \frac{\mu_{hnf}}{1+\lambda_1} \left(1 + \lambda_2 \frac{\partial}{\partial t} \right) \frac{\partial^2 u}{\partial y^2} - \sigma B_0^2 u + g(\rho\beta_T)_{hnf} (T - T_\infty), \quad (1)$$

$$(\rho C_p)_{hnf} \frac{\partial T}{\partial t} = k_{hnf} \frac{\partial^2 T}{\partial y^2} - \frac{\partial q_r}{\partial y} - Q_0(T - T_\infty). \quad (2)$$

Provided that no-slip condition exists between the fluid and the plate. The appropriate initial and boundary conditions have been chosen as follows [59]:

$$u(y, 0) = 0; \quad T(y, 0) = T_\infty; \quad y \geq 0. \quad (3)$$

$$u(0, t) = 0; \quad T(0, t) = T_w; \quad t > 0, \quad (4)$$

$$u(\infty, t) = 0; \quad T(\infty, t) = T_\infty. \quad (5)$$

Here, ρ is the density, u is the velocity component in the x –direction, μ is the dynamic viscosity, λ_1 is the ratio of relaxation time and retardation time, λ_2 is the retardation time, σ is the electrical conductivity, g is the acceleration due to gravity, β_T is the volumetric coefficient of thermal expansion, T is the temperature, C_p is the specific heat at constant temperature, k is the thermal conductivity, q_r is the radiative heat flux, Q_0 is the heat absorption coefficient, and the subscript hnf , ∞ and w refer to hybrid nanofluid, free stream condition and condition at the surface, respectively.

Mathematically, the correlation of thermophysical properties for hybrid nanofluid are given by [62,63]:

$$\rho_{hnf} = \varphi_1 \rho_1 + \varphi_2 \rho_2 + (1 - \varphi_{hnf}) \rho_f, \text{ where } \varphi_{hnf} = \varphi_1 + \varphi_2. \quad (6)$$

$$\mu_{hnf} = \frac{\mu_f}{(1 - \varphi_1 - \varphi_2)^{2.5}}, \quad (7)$$

$$(\rho \beta_T)_{hnf} = \varphi_1 (\rho \beta_T)_1 + \varphi_2 (\rho \beta_T)_2 + (1 - \varphi_{hnf}) (\rho \beta_T)_f, \quad (8)$$

$$(\rho C_p)_{hnf} = \varphi_1 (\rho C_p)_1 + \varphi_2 (\rho C_p)_2 + (1 - \varphi_{hnf}) (\rho C_p)_f, \quad (9)$$

$$\frac{k_{hnf}}{k_f} = \frac{(k_{hp} + 2k_f) - 2\varphi_{hnf}(k_f - k_{hp})}{(k_{hp} + 2k_f) + \varphi_{hnf}(k_f - k_{hp})}, \text{ where } k_{hp} = \frac{\varphi_1 k_1 + \varphi_2 k_2}{\varphi_1 + \varphi_2}. \quad (10)$$

Here, the subscripts f , 1 and 2 stand for the base fluid, Alumina, (Al_2O_3) and Copper, (Cu) nanoparticles, respectively. The thermophysical features of base fluids and nanoparticles are demonstrated in Table 1.

Table 1
 The thermophysical features of base fluids and nanoparticles [62,64,65]

Physical properties	Base fluid			Nanoparticles	
	Ethylene Glycol	Kerosene	Water	Al_2O_3	Cu
ρ (kg/m^3)	1115	780	997.1	3970	8933
C_p (J/kgK)	2386	2090	4179	765	385
k (W/mK)	0.2499	0.149	0.613	40	400
β (K^{-1})	3.41×10^{-3}	9.9×10^{-4}	21×10^{-5}	0.85×10^{-5}	01.67×10^{-5}
Pr	203	21	6.2	-	-

The radiation heat flux, q_r under Rosseland approximation can be defined as [66-68]

$$q_r = -\frac{4\sigma^*}{3k_1} \frac{\partial T^4}{\partial y}, \quad (11)$$

where σ^* and k_1 denote the Stefan-Boltzmann constant and the coefficient of Rosseland absorption respectively. Since, the temperature differences within the flow are assumed to be very small, then using Taylor series expansion, T^4 about T_∞ can be expressed as

$$T^4 \cong T_\infty^4 + \frac{4T_\infty^3}{1!} (T - T_\infty) + \frac{12T_\infty^2}{2!} (T - T_\infty)^2 + \dots \quad (12)$$

Hence, by emitting higher order, Eq. (12) takes the form of

$$T^4 \cong T_\infty^4 + 4T_\infty^3(T - T_\infty) = T_\infty^4 + 4T_\infty^3T - 4T_\infty^4 = 4T_\infty^3T - 3T_\infty^4. \quad (13)$$

Upon substituting Eq. (11) and Eq. (13) in Eq. (2), yields

$$\frac{\partial T}{\partial t} = \frac{k_f}{(\rho C_p)_{hnf}} \left(\frac{k_{hnf}}{k_f} + \frac{16}{3} \frac{\sigma^* T_\infty^3}{k_f k_1} \right) \frac{\partial^2 T}{\partial y^2} - \frac{1}{(\rho C_p)_{hnf}} Q_0 (T - T_\infty). \quad (14)$$

Introducing the following dimensionless variables [59,60]:

$$u^* = \frac{u}{U_0}, \quad t^* = \frac{t U_0^2}{\nu_f}, \quad y^* = \frac{y U_0}{\nu_f}, \quad \theta = \frac{T - T_\infty}{T_w - T_\infty}, \quad (15)$$

into Eq. (1) to Eq. (5) and make use of relations in Eq. (6) to Eq. (10), leads to the expressions of non-dimensional partial differential equations (for simplicity, omit the star notations)

$$\xi_0 \frac{\partial u}{\partial t} = \left(\frac{\xi_1}{1 + \lambda_1} \right) \left(1 + \lambda \frac{\partial}{\partial t} \right) \frac{\partial^2 u}{\partial y^2} - (Ha)u + \xi_2 (Gr)\theta, \quad (16)$$

$$\eta_1 \frac{\partial \theta}{\partial t} = \frac{\eta_2}{Pr} \frac{\partial^2 \theta}{\partial y^2} - Q\theta. \quad (17)$$

Subject to initial and boundary conditions:

$$u(y, 0) = 0; \quad \theta(y, 0) = 0; \quad y \geq 0, \quad (18)$$

$$u(0, t) = 0; \quad \theta(0, t) = 1; \quad t > 0, \quad (19)$$

$$u(\infty, t) = 0; \quad \theta(\infty, t) = 0; \quad t > 0. \quad (20)$$

In which, λ is the dimensionless Jeffrey parameter, Ha is the Hartmann number, Gr is the Grashof number, Pr is the Prandtl number and Q is the heat absorption parameter. These parameters can be defined as follows:

$$\lambda = \frac{\lambda_2 U_0^2}{\nu_f}, \quad Ha = \frac{\sigma B_0^2 \nu_f}{\rho_f U_0^2}, \quad Gr = \frac{g(\beta_T \nu)_f (T_w - T_\infty)}{U_0^3}, \quad Pr = \frac{\nu_f}{\alpha_f}, \quad Q = \frac{Q_0}{U_0} \left(\frac{\nu}{\rho C_p} \right)_f,$$

where

$$\alpha_f = \frac{k_f}{(\rho C_p)_f}. \quad (21)$$

The arbitrary constants are given by

$$\xi_0 = \left(\frac{\varphi_1 \rho_1 + \varphi_2 \rho_2}{\rho_f} \right) + (1 - \varphi_1 - \varphi_2), \quad (22)$$

$$\xi_1 = \frac{1}{(1 - \varphi_1 - \varphi_2)^{2.5}}, \quad (23)$$

$$\xi_2 = \frac{\varphi_1 (\rho \beta_T)_1 + \varphi_2 (\rho \beta_T)_2}{(\rho \beta_T)_f} + (1 - \varphi_1 - \varphi_2), \quad (24)$$

$$\eta_1 = \frac{\varphi_1 (\rho C_p)_1 + \varphi_2 (\rho C_p)_2}{(\rho C_p)_f} + (1 - \varphi_1 - \varphi_2), \quad (25)$$

$$\eta_2 = \frac{k_{nnf}}{k_f} + Rd. \quad (26)$$

Here, Rd is the radiation parameter which can be written as

$$Rd = \frac{16 \sigma^* T_\infty^3}{3 k_f k_1}. \quad (27)$$

3. Solution of the Problem

There are two methods to solve the above partial differential equations, namely analytical method, and numerical approach. However, in this study, an analytical method is chosen to solve the present problem with the help of Laplace transform technique. Thus, applying the Laplace transform to Eq. (16) to Eq. (20) leads to the following transformed system in (y, q) –plane:

$$\xi_0 [q\bar{u}(y, q) - \bar{u}(y, 0)] = \left(\frac{\xi_1}{1 + \lambda_1} \right) \frac{d^2 \bar{u}(y, q)}{dy^2} + \left(\frac{\lambda \xi_1}{1 + \lambda_1} \right) \frac{d^2}{dy^2} [q\bar{u}(y, q) - \bar{u}(y, 0)] - (Ha)\bar{u}(y, q) + \xi_2 (Gr)\bar{\theta}(y, q), \quad (28)$$

$$\eta_1 [q\bar{\theta}(y, q) - \bar{\theta}(y, 0)] = \frac{\eta_2}{Pr} \frac{d^2 \bar{\theta}(y, q)}{dy^2} - Q\bar{\theta}(y, q), \quad (29)$$

together with the transform initial and boundary conditions below:

$$\bar{u}(y, 0) = 0; \quad \bar{\theta}(y, 0) = 0, \quad (30)$$

$$\bar{u}(0, q) = 0; \quad \bar{u}(\infty, q) = 0, \quad (31)$$

$$\bar{\theta}(0, q) = \frac{1}{q}; \quad \bar{\theta}(\infty, q) = 0. \quad (32)$$

Here, $\bar{u}(y, q)$ and $\bar{\theta}(y, q)$ denotes the Laplace transforms of $u(y, t)$ and $\theta(y, t)$. Now, using Eq. (30) into Eq. (28) and Eq. (29), yields to

$$\xi_0 q \bar{u}(y, q) = \left(\frac{\xi_1}{1+\lambda_1} \right) \frac{d^2 \bar{u}(y, q)}{dy^2} + \left(\frac{\lambda \xi_1}{1+\lambda_1} q \right) \frac{d^2 \bar{u}(y, q)}{dy^2} - (Ha) \bar{u}(y, q) + \xi_2 (Gr) \bar{\theta}(y, q), \quad (33)$$

$$\frac{d^2 \bar{\theta}(y, q)}{dy^2} - \left[\frac{Pr}{\eta_2} (Q + \eta_2 q) \right] \bar{\theta}(y, q) = 0. \quad (34)$$

Since there exists the term of energy equation in Eq. (33), therefore, it is much simpler to solve the energy equation first rather than the momentum equation. Invoking Eq. (32) into Eq. (34), then

$$\bar{\theta}(y, q) = \frac{1}{q} e^{-y \sqrt{\frac{\eta_1 Pr}{\eta_2} \sqrt{q + \frac{Q}{\eta_1}}}}. \quad (35)$$

the inverse Laplace transform of Eq. (35), gives the required temperature distribution as

$$\theta(y, t) = \frac{1}{2} e^{y \sqrt{\frac{QPr}{\eta_2}}} \cdot \operatorname{erfc} \left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2 t}} + \sqrt{\frac{Qt}{\eta_1}} \right) + \frac{1}{2} e^{-y \sqrt{\frac{QPr}{\eta_2}}} \cdot \operatorname{erfc} \left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2 t}} - \sqrt{\frac{Qt}{\eta_1}} \right). \quad (36)$$

In Eq. (36), $\operatorname{erfc}(\cdot)$ is the complementary error function which can defined as

$$\operatorname{erf}(x) = 1 - \operatorname{erfc}(x); \quad \operatorname{erfc}(x) = 2 \int_x^\infty \frac{1}{\sqrt{x}} e^{-u^2} du. \quad (37)$$

Plugging Eq. (35) into Eq. (33) and make use of Eq. (31) gives

$$\bar{u}(y, q) = \left(\frac{a_1 \eta_2}{a_2} \right) [\bar{u}_1(y, q) - \bar{u}_2(y, q)], \quad (38)$$

where,

$$\bar{u}_1(y, q) = \left(\frac{1}{q} \right) \left(\frac{1}{(q+b_0)^2 - b_1} \right) e^{-y \sqrt{a_0 \left(\frac{Ha + \xi_0 q}{1 + \lambda q} \right)}}, \quad (39)$$

$$\bar{u}_2(y, q) = \left(\frac{1}{q} \right) \left(\frac{1}{(q+b_0)^2 - b_1} \right) e^{-y \sqrt{\frac{\eta_1 Pr}{\eta_2} \sqrt{q + \frac{Q}{\eta_1}}}}. \quad (40)$$

Here arbitrary constants are given by:

$$a_0 = \frac{1+\lambda_1}{\xi_1}, \quad a_1 = \frac{\xi_2 Gr}{\xi_1} (1 + \lambda_1), \quad a_2 = \lambda \eta_1 Pr, \quad b_0 = \frac{a_3}{2a_2}, \quad b_1 = \frac{(a_3)^2 - 4a_2 a_4}{4(a_2)^2}. \quad (41)$$

In which,

$$a_3 = (\eta_1 + \lambda Q) Pr - a_0 \eta_2 \xi_0, \quad a_4 = QPr - a_0 \eta_2 Ha. \quad (42)$$

In order to determine the inverse Laplace transform of Eq. (39), we set up it in the form of

$$\bar{u}_1(y, q) = \bar{F}_1(q) \cdot \bar{F}_2(y, q). \quad (43)$$

In which,

$$\bar{F}_1(q) = \frac{1}{(q+b_0)^2-b_1}, \quad (44)$$

$$\bar{F}_2(y, q) = \frac{1}{q} e^{-y\sqrt{a_0\left(\frac{Ha+\xi_0q}{1+\lambda q}\right)}}. \quad (45)$$

Taking the inverse Laplace transform of Eq. (44) implies

$$F_1(t) = \frac{1}{\sqrt{b_1}} e^{-b_0t} \sinh(\sqrt{b_1}t). \quad (46)$$

Now, split Eq. (45) into

$$\bar{F}_{21}(q) = \frac{1}{q}, \quad (47)$$

$$\bar{F}_{22}(y, q) = e^{-y\sqrt{\frac{a_0Ha+a_0\xi_0q}{1+\lambda q}}}. \quad (48)$$

The inversion Laplace transform of Eq. (47) is given by

$$F_{21}(t) = 1. \quad (49)$$

Let Eq. (48) as

$$\bar{F}_{22}(y, q) = e^{-y\sqrt{w(q)}}, \text{ where } w(q) = \frac{a_0Ha+(a_0\xi_0)q}{1+\lambda q}. \quad (50)$$

Following Nazar *et al.*, [69], the inverse Laplace transform of Eq. (50) can be determined using the inversion formula of compound function such that

$$F_{22}(y, t) = \int_0^\infty f(y, u)g(u, t)du, \quad (51)$$

where

$$f(y, u) = \frac{y}{2u\sqrt{\pi u}} e^{-\left(\frac{y^2}{4u}\right)}, \quad (52)$$

$$g(u, t) = e^{-ud_0} \delta(t) + \sqrt{\frac{ud_1}{t}} e^{-ud_0-\frac{t}{\lambda}} I_1(2\sqrt{ud_1t}). \quad (53)$$

Here, $\delta(\cdot)$ is Dirac delta function, $I_1(\cdot)$ is the modified Bessel function of the first kind of order one and the arbitrary constants are given as follows

$$d_0 = \frac{a_0\xi_0}{\lambda}, \quad d_1 = \frac{a_0\xi_0}{\lambda^2} - \frac{a_0Ha}{\lambda}. \quad (54)$$

Hence, make use of Eq. (52) and Eq. (53) into Eq. (51) yielding the following simplified form:

$$F_{22}(y, t) = \delta(t)e^{-y\sqrt{d_0}} + \int_0^\infty \frac{y}{2u} \sqrt{\frac{d_1}{\pi t}} e^{-\frac{y^2}{4u}-ud_0-\frac{t}{\lambda}} I_1(2\sqrt{ud_1 t}) du. \quad (55)$$

In order to determine the function $F_2(y, t)$ in Eq. (45), we need to use the convolution theorem as being given by:

$$F_2(y, t) = (F_{21} * F_{22})(t) = \int_0^t F_{21}(t - s) \cdot F_{22}(y, s) ds. \quad (56)$$

Incorporating Eq. (49) and Eq. (55) into Eq. (56), and after further simplification, the function $F_2(y, t)$ takes the following form:

$$F_2(y, t) = e^{-y\sqrt{d_0}} + \int_0^t \int_0^\infty \frac{y}{2u} \sqrt{\frac{d_1}{\pi s}} e^{-\frac{y^2}{4u}-ud_0-\frac{s}{\lambda}} I_1(2\sqrt{ud_1 s}) du ds. \quad (57)$$

Since, Eq. (43) involves multiplication of two functions of $\bar{F}_1(q)$ and $\bar{F}_2(y, q)$, again the convolution theorem is utilized. Hence it can be written as

$$\begin{aligned} u_1(y, t) &= (F_1 * F_2)(t) = \int_0^t F_1(t - p) \cdot F_2(y, p) dp \\ &= \int_0^t \frac{1}{\sqrt{b_1}} e^{-b_0(t-p)-y\sqrt{d_0}} \sinh(\sqrt{b_1}(t-p)) dp \\ &\quad + \int_0^t \int_0^p \int_0^\infty \frac{y}{2u} \sqrt{\frac{d_1}{\pi b_1 s}} e^{-b_0(t-p)-\frac{y^2}{4u}-ud_0-\frac{s}{\lambda}} \sinh(\sqrt{b_1}(t-p)) \times I_1(2\sqrt{ud_1 s}) du ds dp. \end{aligned} \quad (58)$$

Furthermore, to evaluate the function $\bar{u}_2(y, q)$, we split Eq. (40) into

$$\bar{u}_2(y, q) = \bar{F}_1(q) \cdot \bar{F}_3(y, q), \quad (59)$$

where $\bar{F}_1(q)$ as in Eq. (44) and

$$\bar{F}_3(y, q) = \frac{1}{q} e^{-y\sqrt{\frac{\eta_1 Pr}{\eta_2}} \sqrt{q + \frac{Q}{\eta_1}}}. \quad (60)$$

Following Hetnarski [70], The inversion Laplace transform of Eq. (60) can be obtained as follows:

$$F_3(y, t) = \frac{1}{2} e^{y\sqrt{\frac{QPr}{\eta_2}}} \operatorname{erfc}\left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2 t}} + \sqrt{\frac{Qt}{\eta_1}}\right) + \frac{1}{2} e^{-y\sqrt{\frac{QPr}{\eta_2}}} \operatorname{erfc}\left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2 t}} - \sqrt{\frac{Qt}{\eta_1}}\right). \quad (61)$$

Since, Eq. (40) involves multiplication of two functions of $\bar{F}_1(q)$ and $\bar{F}_3(y, q)$, again the convolution theorem

$$u_2(y, t) = (F_1 * F_3)(t) = \int_0^t F_1(t - s) \cdot F_3(y, s) ds \quad (62)$$

is used. Then,

$$u_2(y, t) = \int_0^t \frac{1}{2\sqrt{b_1}} e^{-b_0(t-s)+y\sqrt{\frac{QPr}{\eta_2}}} \sinh[\sqrt{b_1}(t-s)] \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{\eta_1 Pr}{\eta_2 s}} + \sqrt{\frac{Qs}{\eta_1}}\right) ds + \int_0^t \frac{1}{2\sqrt{b_1}} e^{-b_0(t-s)-y\sqrt{\frac{QPr}{\eta_2}}} \sinh[\sqrt{b_1}(t-s)] \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{\eta_1 Pr}{\eta_2 s}} - \sqrt{\frac{Qs}{\eta_1}}\right) ds. \quad (63)$$

Thus, the solution of velocity profile in Eq. (38) can be written as

$$u(y, t) = \left(\frac{a_1 \eta_2}{a_2}\right) [u_1(y, t) - u_2(y, t)]. \quad (64)$$

In which the functions of $u_1(y, t)$ and $u_2(y, t)$ are given by Eq. (58) and Eq. (63) respectively.

4. Nusselt Number and Skin Friction

The rate of heat transfer or Nusselt number, Nu and the coefficient of skin friction, τ are defined as

$$Nu = -\frac{\partial \theta}{\partial y} \Big|_{y=0}, \quad (65)$$

$$\tau = \frac{1}{1+\lambda_1} \left(1 + \lambda \frac{\partial}{\partial t}\right) \frac{\partial u}{\partial y} \Big|_{y=0}. \quad (66)$$

Plugging Eq. (36) into Eq. (65) and Eq. (64) into Eq. (66), therefore

$$Nu = -\frac{1}{2} \sqrt{\frac{QPr}{\eta_2}} \operatorname{erfc}\left(\sqrt{\frac{Qt}{\eta_1}}\right) + \sqrt{\frac{Pr \eta_1}{\pi \eta_2}} e^{-\sqrt{\frac{Qt}{\eta_1}}} + \frac{1}{2} \sqrt{\frac{QPr}{\eta_2}} \operatorname{erfc}\left(-\sqrt{\frac{Qt}{\eta_1}}\right), \quad (67)$$

$$\tau = \frac{1}{1+\lambda_1} \left(\frac{a_1 \eta_2}{a_2}\right) [\Psi_1(t) + \Psi_2(t) - \Psi_3(t) + \Psi_4(t)] + \frac{\lambda}{1+\lambda_1} \left(\frac{a_1 \eta_2}{a_2}\right) [\Phi_1(t) + \Phi_2(t) - \Phi_3(t) + \Phi_4(t)] \quad (68)$$

In which the components of $\Psi_i (i = 1, 2, 3, 4)$ and $\Phi_j (j = 1, 2, 3, 4)$ are given by

$$\Psi_1(t) = -\frac{\sqrt{d_0}}{b_1} \left[\frac{\sqrt{b_1} e^{-b_0 t} \cosh(\sqrt{b_1} t) - \sqrt{b_1 + b_0} e^{-b_0 t} \sinh(\sqrt{b_1} t)}{b_1 - b_0^2} \right], \quad (69)$$

$$\Psi_2(t) = \int_0^t \int_0^p \int_0^\infty \frac{1}{2u} \sqrt{\frac{d_1}{\pi b_1 s}} e^{b_0(p-t)-ud_0-\frac{s}{\lambda}} \times \sinh[\sqrt{b_1}(t-p)] I_1(2\sqrt{ud_1 s}) dudsdp, \quad (70)$$

$$\Psi_3(t) = \int_0^t \frac{1}{2\sqrt{b_1}} e^{b_0(s-t)} \sinh[\sqrt{b_1}(t-s)] \times \left[\sqrt{\frac{QPr}{\eta_2}} \operatorname{erfc}\left(\sqrt{\frac{Qs}{\eta_2}}\right) - \frac{1}{\sqrt{\pi}} e^{\frac{Qs}{\eta_2}} \sqrt{\frac{\eta_1 Pr}{s \eta_2}} \right] ds, \quad (71)$$

$$\Psi_4(t) = \int_0^t \frac{1}{2} \sqrt{\frac{Pr}{\eta_2 b_1}} e^{b_0(s-t)} \sinh[\sqrt{b_1}(t-s)] \times \left[\sqrt{Q} \operatorname{erfc}\left(-\sqrt{\frac{Qs}{\eta_2}}\right) + \sqrt{\frac{\eta_1}{s \pi}} e^{-\frac{Qs}{\eta_2}} \right] ds, \quad (72)$$

and

$$\Phi_1(t) = \sqrt{\frac{d_0}{b_1}} \left[\frac{b_0^2 e^{-b_0 t} \sinh(\sqrt{b_1} t) - b_1 e^{-b_0 t} \sinh(\sqrt{b_1} t)}{b_1 - b_0^2} \right], \quad (73)$$

$$\Phi_2(t) = \int_0^t \int_0^p \int_0^\infty \left[b_0 e^{-b_0 t} \sinh[\sqrt{b_1}(p-t)] + \sqrt{b_1} e^{-b_0 t} \cosh[\sqrt{b_1}(p-t)] \right] \times \frac{1}{2u} \sqrt{\frac{d_1}{b_1 \pi s}} e^{b_0 p - u d_0 - \frac{s}{\lambda}} \times I_1(2\sqrt{u d_1 s}) du ds dp, \quad (74)$$

$$\Phi_3(t) = \int_0^t \frac{b_0 e^{b_0(s-t)}}{2} \sqrt{\frac{Pr}{b_1 \eta_2}} \left[\sqrt{Q} \operatorname{erfc} \left(\sqrt{\frac{Qs}{\eta_2}} \right) - \sqrt{\frac{\eta_1}{\pi}} e^{\frac{Qs}{\eta_2}} \right] \times \left[\sinh[\sqrt{b_1}(s-t)] + \sqrt{b_1} \cosh[\sqrt{b_1}(s-t)] \right] ds, \quad (75)$$

$$\Phi_4(t) = \int_0^t \frac{1}{2} \sqrt{\frac{Pr}{b_1 \eta_2}} \left[\sqrt{Q} \operatorname{erfc} \left(-\sqrt{\frac{Qs}{\eta_2}} \right) + \sqrt{\frac{Pr \eta_1}{s \pi}} e^{-\frac{Qs}{\eta_2}} \right] \times \left[b_0 e^{b_0(s-t)} \sinh[\sqrt{b_1}(s-t)] + \sqrt{b_1} e^{b_0(s-t)} \cosh[\sqrt{b_1}(s-t)] \right] ds. \quad (76)$$

5. Special Cases

In this section, closed-form solutions for two special cases are provided by taking suitable parameters equal to zero.

5.1 Case 1: $\lambda_1 = 0$

Surprisingly, by taking $\lambda_1 = 0$, the obtained velocity profile in Eq. (64) can be reduced to the problem of second grade hybrid nanofluid with heat absorption and radiation effects. This implies:

$$u(y, t) = \frac{\xi_2 \eta_2 Gr}{\xi_1 \eta_1 \lambda Pr} \left[\frac{1}{\sqrt{b_{11}}} u_{11}(y, t) + \frac{1}{2} \sqrt{\frac{d_{11}}{\pi b_{11}}} u_{12}(y, t) - \frac{1}{2\sqrt{b_{11}}} u_{13}(y, t) - \frac{1}{2\sqrt{b_{11}}} u_{14}(y, t) \right], \quad (77)$$

where

$$u_{11}(y, t) = \int_0^t e^{b_{01}(p-t) - y\sqrt{d_{01}}} \sinh(\sqrt{b_{11}}(t-p)) dp, \quad (78)$$

$$u_{12}(y, t) = \int_0^t \int_0^p \int_0^\infty \frac{y}{u\sqrt{s}} e^{b_{01}(p-t) - \frac{y^2}{4u} - u d_{01} - \frac{s}{\lambda}} \sinh(\sqrt{b_{11}}(t-p)) \times I_1(2\sqrt{u d_{11} s}) du ds dp, \quad (79)$$

$$u_{13}(y, t) = \int_0^t e^{b_{01}(s-t) + y\sqrt{\frac{QPr}{\eta_2}}} \sinh[\sqrt{b_{11}}(t-s)] \operatorname{erfc} \left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2}} + \sqrt{\frac{Qs}{\eta_1}} \right) ds, \quad (80)$$

$$u_{14}(y, t) = \int_0^t e^{b_{01}(s-t) - y\sqrt{\frac{QPr}{\eta_2}}} \sinh(\sqrt{b_{11}}(t-s)) \operatorname{erfc} \left(\frac{y}{2} \sqrt{\frac{\eta_1 Pr}{\eta_2 s}} - \sqrt{\frac{Qs}{\eta_1}} \right) ds. \quad (81)$$

In which the arbitrary parameters are given by

$$\begin{aligned}
 a_{31} &= \eta_1 Pr + \lambda Q Pr - \frac{\eta_2 \xi_0}{\xi_1}, & a_{41} &= Q Pr - \frac{\eta_2 Ha}{\xi_1}, \\
 b_{01} &= \frac{a_{31}}{2a_2}, & b_{11} &= \frac{(a_{31})^2 - 4a_2 a_{41}}{4(a_2)^2}, \\
 d_{01} &= \frac{\xi_0}{\lambda \xi_1}, & d_{11} &= \frac{1}{\lambda \xi_1} \left(\frac{\xi_0}{\lambda} - Ha \right).
 \end{aligned} \tag{82}$$

5.2 Case 2: $\varphi_1 = \varphi_2 = 0$

In addition, substituting $\varphi_1 = \varphi_2 = 0$, into Eq. (64) leads to the following expression:

$$u(y, t) = \frac{(1+\lambda_1)(1+Rd)Gr}{\lambda Pr} \left[\frac{1}{\sqrt{b_{12}}} u_{21}(y, t) + \frac{1}{2} \sqrt{\frac{d_{12}}{\pi b_{12}}} u_{22}(y, t) - \frac{1}{2\sqrt{b_{12}}} u_{23}(y, t) - \frac{1}{2\sqrt{b_{12}}} u_{24}(y, t) \right]. \tag{83}$$

Here,

$$u_{21}(y, t) = \int_0^t e^{b_{02}(p-t)-y\sqrt{\frac{1+\lambda_1}{\lambda}}} \sinh(\sqrt{b_{12}}(t-p)) dp, \tag{84}$$

$$u_{12}(y, t) = \int_0^t \int_0^p \int_0^\infty \frac{y}{u\sqrt{s}} e^{b_{02}(p-t)-\frac{y^2}{4u}-u\left(\frac{1+\lambda_1}{\lambda}\right)-\frac{s}{\lambda}} \sinh(\sqrt{b_{12}}(t-p)) \times I_1(2\sqrt{ud_{12}s}) dudsdp, \tag{85}$$

$$u_{23}(y, t) = \int_0^t e^{b_{02}(s-t)+y\sqrt{\frac{QPr}{1+Rd}}} \sinh[\sqrt{b_{12}}(t-s)] \times \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{Pr}{1+Rd}} + \sqrt{Qs}\right) ds, \tag{86}$$

$$u_{24}(y, t) = \int_0^t e^{b_{02}(s-t)-y\sqrt{\frac{QPr}{1+Rd}}} \sinh(\sqrt{b_{12}}(t-s)) \times \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{Pr}{(1+Rd)s}} - \sqrt{Qs}\right) ds, \tag{87}$$

and

$$\begin{aligned}
 b_{02} &= \frac{Pr(1+\lambda Q) + (1+\lambda_1)(1+Rd)}{2\lambda Pr}, \\
 b_{12} &= \left[\frac{Pr(1+\lambda Q) + (1+\lambda_1)(1+Rd)}{2\lambda Pr} \right]^2 - \frac{1}{\lambda} [Q + (1+Rd)Ha], \\
 d_{12} &= \frac{(1+\lambda_1)}{\lambda} \left(\frac{1}{\lambda} - Ha \right).
 \end{aligned} \tag{88}$$

It corresponds to the general unsteady MHD free convection flow of Jeffrey fluid with the effects of radiation and heat absorption. However, by taking $Rd = 0$ and $Q = 0$ into Eq. (36) and $Rd = 0$, $Q = 0$ and $Ha = 0$ into Eq. (83), leads to

$$\theta(y, t) = \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{Pr}{t}}\right) \tag{89}$$

$$\begin{aligned}
 u(y,t) = & \frac{2Gr(1+\lambda_1)}{Pr+1+\lambda_1} \int_0^t e^{\frac{Pr+1+\lambda_1}{2\lambda Pr}(p-t)-y\sqrt{\frac{1+\lambda_1}{\lambda}}} \sinh\left[\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(t-p)\right] dp + \\
 & \frac{Gr(1+\lambda_1)}{\lambda(Pr+1+\lambda_1)} \sqrt{\frac{1+\lambda_1}{\pi}} \int_0^t \int_0^p \int_0^\infty \frac{y}{u\sqrt{s}} e^{\frac{Pr+1+\lambda_1}{2\lambda Pr}(p-t)-\frac{y^2}{4u}-u\left(\frac{1+\lambda_1}{\lambda}\right)\frac{s}{\lambda}} \times \sinh\left[\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(t-p)\right] I_1\left(\frac{2}{\lambda}\sqrt{u(1+\lambda_1)s}\right) dudsdp - \\
 & \frac{Gr(1+\lambda_1)}{Pr+1+\lambda_1} \int_0^t e^{\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(s-t)} \sinh\left[\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(t-s)\right] \times \\
 & \operatorname{erfc}\left(\frac{y}{2}\sqrt{Pr}\right) ds - \frac{Gr(1+\lambda_1)}{Pr+1+\lambda_1} \int_0^t e^{\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(s-t)} \sinh\left[\left(\frac{Pr+1+\lambda_1}{2\lambda Pr}\right)(t-s)\right] \times \operatorname{erfc}\left(\frac{y}{2}\sqrt{\frac{Pr}{s}}\right) ds, \quad (90)
 \end{aligned}$$

respectively, which is identical to the previous work obtained by Khan [59].

6. Results and Discussions

This section discussed several connected parameters such as radiation parameter Rd , heat absorption parameter Q , Hartmann number Ha , Grashof Number Gr , dimensionless material parameter λ , volume fraction of hybrid nanofluid φ_{hnf} , dimensionless time t and Prandtl number Pr on velocity and temperature distributions. The physical model is given in Figure 1. The results of temperature and velocity profiles in Eq. (36) and (64) are computed using MATHCAD software. Figure 2 illustrates the radiation impact on the hybrid nanofluid flow. As can be seen in the graph, velocity of the hybrid nanofluid increases when radiation parameter increases. This phenomenon is observed since the bond of nanofluid's particles are easily disrupted due to the increases of rate energy transmission when radiation parameter rises. Hence, it reduces the nanofluid's viscosity and enhance hybrid nanofluid flow. The variation of heat absorption influence velocity profile is presented in Figure 3. It is found that increases of heat absorption cause velocity profiles to decrease. The occurrence of heat absorption (heat sink) reduces the thermal energy of fluid which leads to increase the viscous force of fluid. Thus, the velocity of hybrid nanofluid is decelerated.

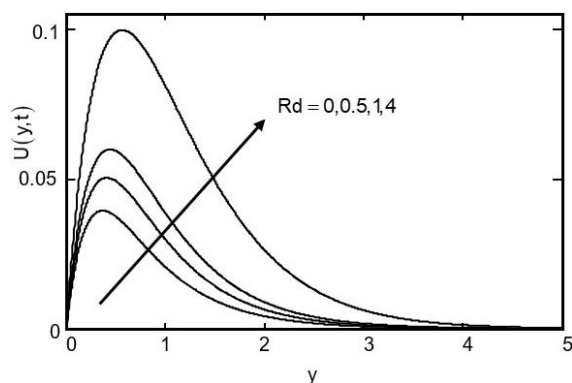


Fig. 2. Velocity profile for different value of Rd , when $\lambda_1 = 1$, $\lambda = 1$, $Ha = 2$, $Q = 2$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$ and $\varphi_{hnf} = 0.04$

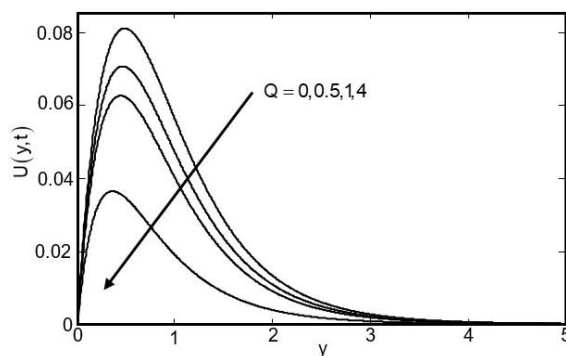


Fig. 3. Velocity profile for different value of Q , when $\lambda_1 = 1$, $\lambda = 1$, $Ha = 2$, $Rd = 0.5$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$ and $\varphi_{hnf} = 0.04$

Figure 4 displays the effect of the MHD on the velocity profiles. It is shown that velocity profiles with the existence of the MHD effect, $Ha = 1, 2, 3$ are higher than velocity profile with no MHD effect, $Ha = 0$. Besides that, velocity profiles diminish with the increasing of MHD parameter. It is due to the drag force produced from the induced current retard the hybrid nanofluid flow when electrical conducting fluid flow across the external magnetic field. The Grashof number effect on the velocity profiles is depicted in Figure 5. Based on the graph observation, velocity distribution inclined with the increment of the Grashof number. It is because buoyancy force rises as temperature gradient

increases and causes reduction of viscous force acting on a fluid. Thus, it enhances the hybrid nanofluid flow.

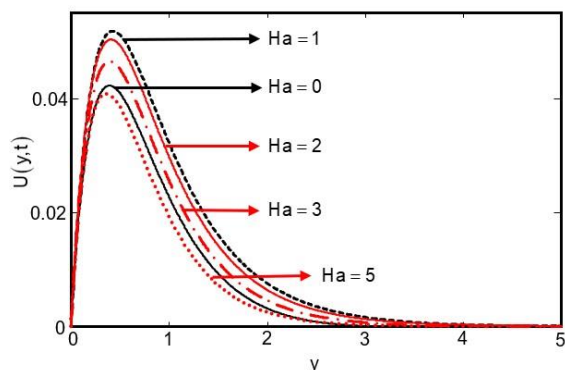


Fig. 4. Velocity profile for different value of Ha , when $\lambda_1 = 1$, $\lambda = 1$, $Q = 2$, $Rd = 0.5$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$ and $\phi_{hnf} = 0.04$

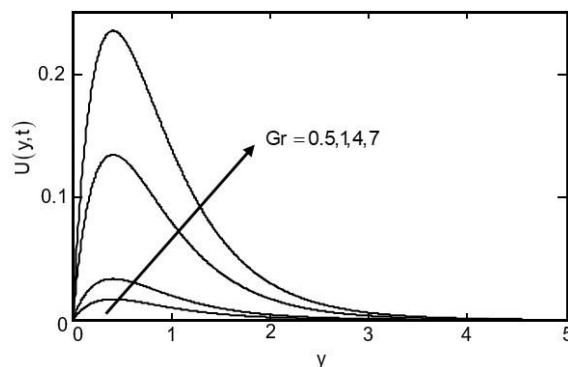


Fig. 5. Velocity profile for different value of Gr , when $\lambda_1 = 1$, $\lambda = 1$, $Q = 2$, $Rd = 0.5$, $Pr = 6.2$, $Ha = 2$, $t = 1$ and $\phi_{hnf} = 0.04$

Figure 6 to 8 are represented the Jeffrey parameters impact on the velocity profiles. For both cases of increasing the relaxation to retardation time ratio, λ and $\lambda = \lambda_1$. As shown in Figure 6 and 7, the velocity profiles decrease at $y < 1.5$. However, velocity profiles increase at $y > 1.5$. Inversely as can be seen in Figure 8, the velocity field is an increasing function of retardation time, λ_1 at $y < 1.5$ while the velocity field is a decreasing function of λ_1 at $y > 1.5$. It is because λ and λ_1 are viscoelastic parameters that exhibit both elastic and viscous behavior which influence the fluid flow velocity.

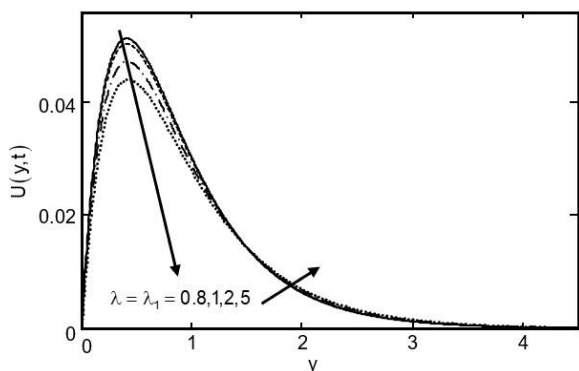


Fig. 6. Velocity profile for different value of λ and λ_1 , when $Q = 2$, $Rd = 0.5$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$ and $\phi_{hnf} = 0.04$

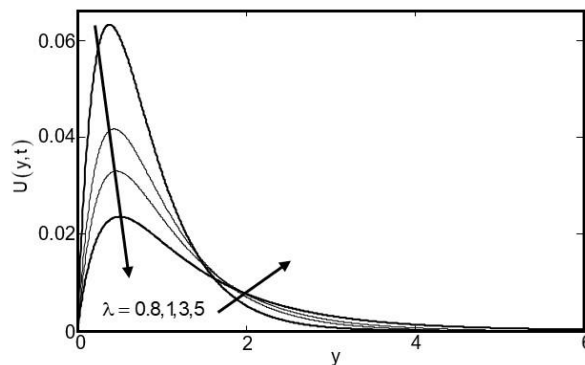


Fig. 7. Velocity profile for different value of λ , when $\lambda_1 = 1.5$, $Gr = 1.5$, $Q = 2$, $Rd = 0.5$, $Pr = 6.2$, $Ha = 2$, $t = 1$ and $\phi_{hnf} = 0.04$

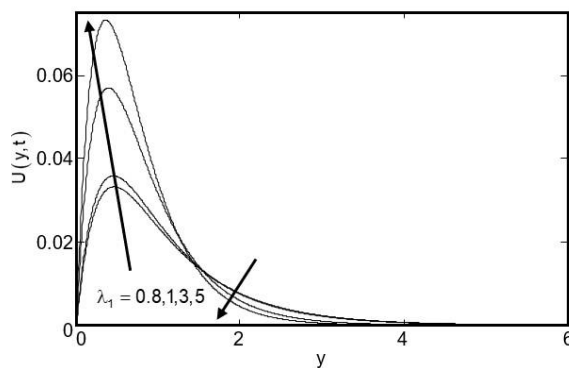


Fig. 8. Velocity profile for different value of λ_1 , when $\lambda = 1.5, Gr = 1.5, Q = 2, Rd = 0.5, Pr = 6.2, Ha = 2, t = 1$ and $\phi_{hnf} = 0.04$

Figure 9 demonstrates the effects of several base fluid types (water, kerosene, and ethylene glycols (EG)) on the velocity profiles. It is found that water has maximum velocity, followed by kerosene, and ethylene glycols. It indicates that water has the lowest viscosity when compared with other types of base fluid. The influence of the hybrid nanofluid in the regular Jeffrey fluid can be seen in Figure 10. It is found that by increasing the nanoparticle volume fraction of hybrid nanofluid, ϕ_{hnf} the velocity profiles fall. It is justified by rising ϕ_{hnf} , the hybrid nanofluid got denser and concentrated. Hence, thermal conductivity of hybrid nanofluid is dominated by the effective density of hybrid nanofluid, which causes the velocity profile to decline.

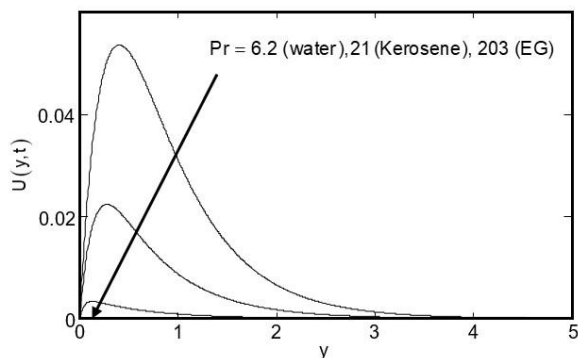


Fig. 9. Velocity profile for different value of Pr , when $\lambda_1 = \lambda = 1, Gr = 1.5, Q = 2, Rd = 0.5, Ha = 2, t = 1$ and $\phi_{hnf} = 0.005$

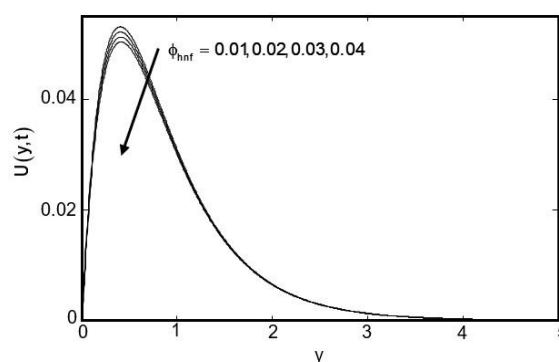


Fig. 10. Velocity profile for different value of ϕ_{hnf} , when $\lambda_1 = 1, \lambda = 1, Ha = 2, Q = 2, Pr = 6.2, Gr = 1.5, t = 1$ and $Rd = 0.5$

The comparison of velocity distribution between nanofluids and regular Jeffrey fluid can be seen in Figure 11. It is discovered that regular Jeffrey fluid has the highest amplitude, followed by nanofluids and then hybrid nanofluids. This indicates that the viscosity of the regular Jeffrey fluid is the lowest among other nanofluids. Hence, regular Jeffrey fluid is the fastest flow while the hybrid nanofluid is the slowest flow.

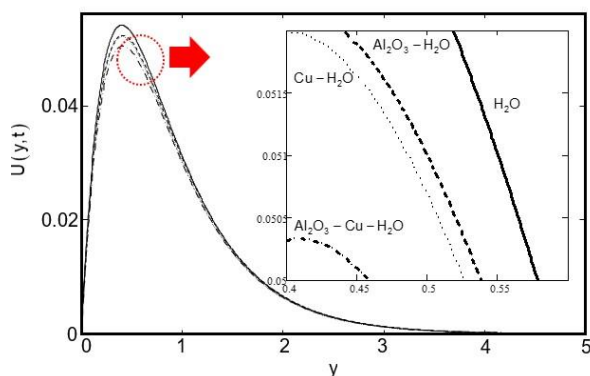


Fig. 11. Comparison of velocity profile for different nanofluids and regular Jeffrey fluid, when $\lambda_1 = 1$, $\lambda = 1$, $Ha = 2$, $Q = 2$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$, $Rd = 0.5$ and $Pr = 6.2$

Figure 12 and 13 are plotted to evaluate the differences velocity profiles between $Al_2O_3 - H_2O$ and $Cu - H_2O$. Both graphs shown that when nanoparticles volume fraction rise, velocity profiles drop. It is due to the increment of the nanofluid viscosity which causes the nanofluid flow to slower down. Besides that, graph observation revealed $Al_2O_3 - H_2O$ has a greater velocity than $Cu - H_2O$. It is because Cu has higher density ($8.92g/cm^3$) compared to Al_2O_3 ($3.95g/cm^3$). Density of the nanoparticles affects the fluid's viscosity. Hence, fluid velocity consists of Cu slower than fluid consists of Al_2O_3 .

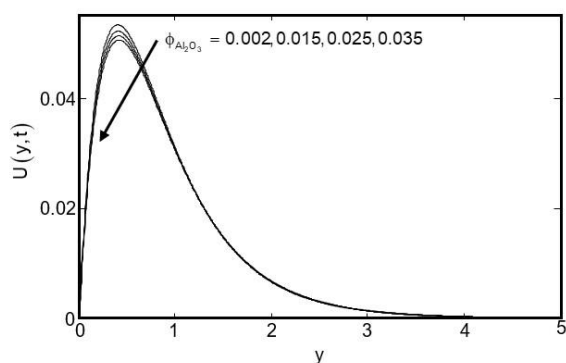


Fig. 12. Comparison of velocity profile for different values of $\phi_{Al_2O_3}$, when $\phi_{Cu} = 0.005$, $\lambda_1 = 1$, $\lambda = 1$, $Ha = 2$, $Q = 2$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$, $Rd = 0.5$ and $Pr = 6.2$

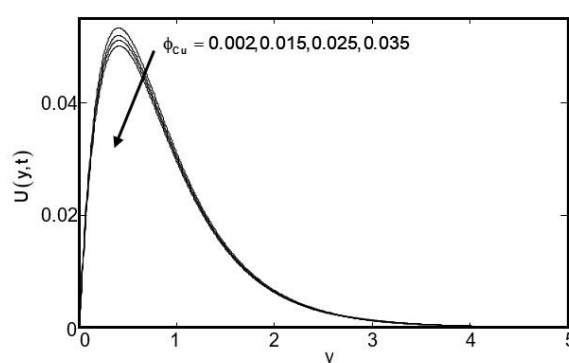


Fig. 13. Comparison of velocity profile for different values of ϕ_{Cu} , when $\phi_{Al_2O_3} = 0.005$, $\lambda_1 = 1$, $\lambda = 1$, $Ha = 2$, $Q = 2$, $Pr = 6.2$, $Gr = 1.5$, $t = 1$, $Rd = 0.5$ and $Pr = 6.2$

Moreover, the influence of radiation on temperature field is plotted in Figure 14. As shown, higher values of Rd will increase the temperature distributions. This is because radiation effect signifies the relative contribution of conduction heat transfer to thermal radiation transfer. Figure 15 shows the effect of t on temperature profiles. It is clearly shown that temperature is an increasing function of t . This is because the temperature will increase as time increases due to a large amount of heat energy being released into the fluid.

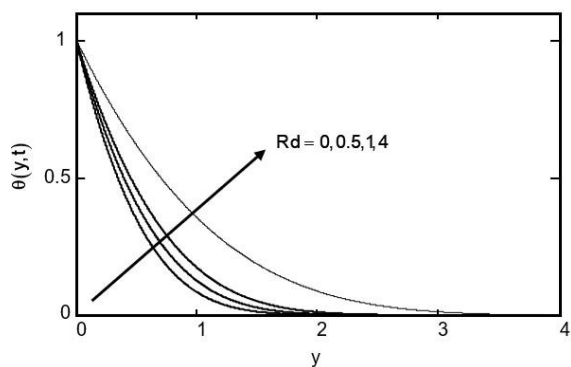


Fig. 14. Temperature profile for different value of Rd , when $Q = 0.5$, $Pr = 6.2$, $t = 1$ and $\phi_{hnf} = 0.04$

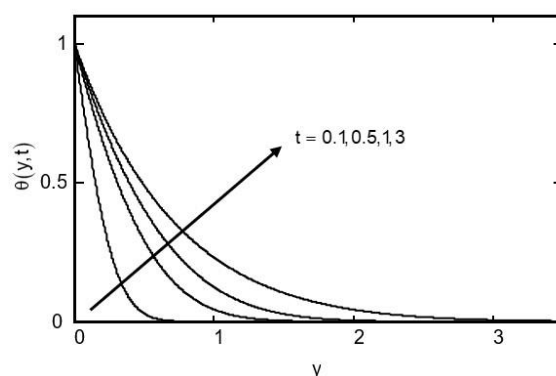


Fig. 15. Temperature profile for different value of t , when $Q = 0.5$, $Pr = 6.2$, $Rd = 0.5$ and $\phi_{hnf} = 0.04$

The variation of heat absorption influence temperature profile is presented in Figure 16. It is found that, the behavior of parameter Q in temperature is like velocity profiles. It shown that the temperature decreases when heat absorption increases due to high viscous force in fluid flow which reduces the thermal energy of fluid. The effect of ϕ_{hnf} can be seen in Figure 17 and it is shown that, increase in ϕ_{hnf} will increase the temperature fields. The reason for this is that as more nanoparticles are added, the thermal conductivity of the nanofluid is improved, leading to an increase in the thermal boundary layer. This results in the dominance of thermal conduction in the flow and allows heat to diffuse rapidly from the heated surface, resulting in a high rate of heat transfer.

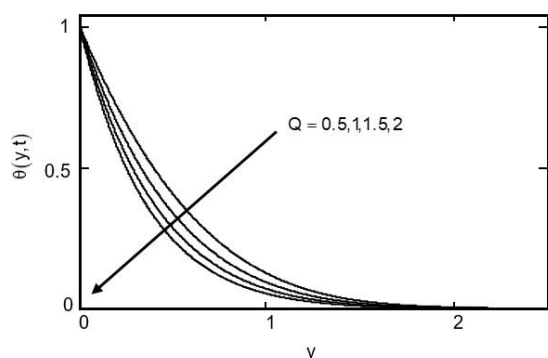


Fig. 16. Temperature profile for different value of Q , when $Rd = 0.5$, $Pr = 6.2$, $t = 1$ and $\phi_{hnf} = 0.04$

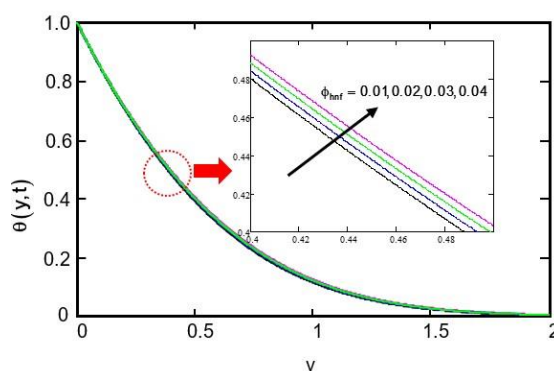


Fig. 17. Temperature profile for different value of ϕ_{hnf} , when $Rd = 0.5$, $Pr = 6.2$, $t = 1$ and $Q = 0.5$

The influence of Pr on temperature profiles is shown in Figure 18. Here, three physical values, $Pr = 6.2$ (water), $Pr = 21$ (Kerosene) and $Pr = 203$ (EG) have been chosen. As clearly shown, when Pr is increased, the temperature decreases. Prandtl number is the ratio of kinematic viscosity to thermal diffusivity. Therefore, when Pr is increased, the kinematic viscosity increases but thermal diffusivity decreases. Thus, temperature decreases due to the increase in kinematic viscosity.

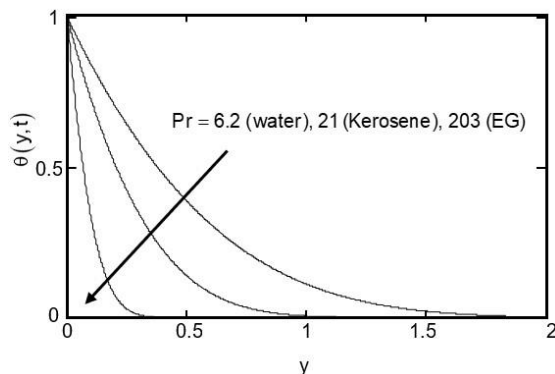


Fig. 18. Temperature profile for different value of Pr , when $Rd = 0.5$, $Q = 0.5$, $t = 1$ and $\varphi_{hnf} = 0.005$

Comparison of temperature profile for different nanofluids and regular Jeffrey fluid is also discussed in Figure 19. Physically, the addition of sufficient volume of nanoparticles leads to the enhancement of nanofluid's thermal conductivity. The more nanoparticles being inserted, the higher the thermal conductivity, which increases the temperature profiles. Besides, the results shown that, $Cu - H_2O$ is enhanced more heat energy compared to $Al_2O_3 - H_2O$ due to its properties which has higher thermal conductivity and heat diffusion. But both nanoparticles are still significantly enhancing the temperature profiles as can see in Figure 20 and 21.

The accuracy of the obtained solution is verified by comparing solution in Eq. (89) and (90) with the solution obtained by Khan [59] in Eq. (18) and (31). The comparison is conducted by letting nanoparticle volume fraction, thermal radiation, heat absorption and Hartmann number are equal to zero which are $\varphi_{hnf} = Rd = Q = Ha = 0$, respectively. This comparison shows the velocity and temperature profiles for both present and previous works are identical to each other as clearly presented in Figure 22 and 23, which thus proves that the accuracy of obtained solutions are verified and in excellent agreement. Meanwhile, another verification is also carried out to verify the validity of present solutions by comparing the values of both profiles from the present work by choosing $\varphi_{hnf} = 0$, and $\varphi_{hnf} = 0.04$. Physically, the addition of sufficient volume of nanoparticles leads to the enhancement of nanofluid's thermal conductivity. The more nanoparticles being inserted, the higher the thermal conductivity, which increases the velocity and temperature profiles.

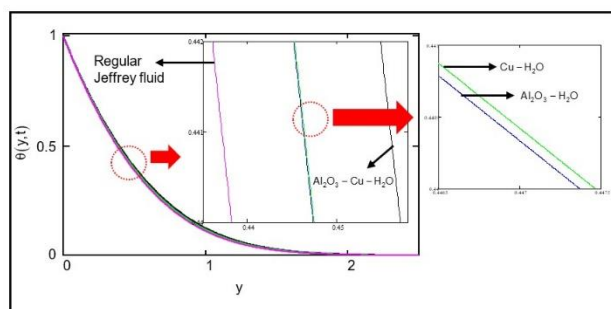


Fig. 19. Comparison of temperature profile for different nanofluids and regular Jeffrey fluid when, $Pr = 6.2$, $t = 1$, $Rd = 0.5$ and $Q = 0.5$

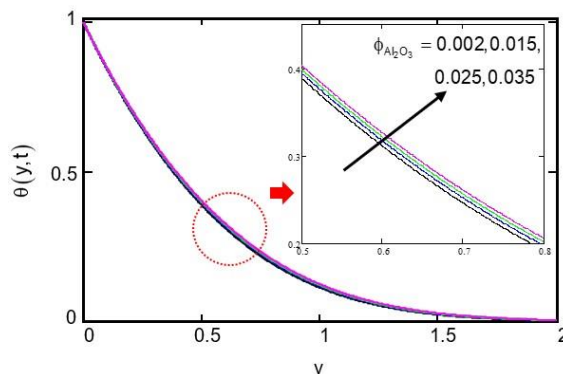


Fig. 20. Temperature profile for different value of $\varphi_{Al_2O_3}$, when $\varphi_{Cu} = 0.005$, $Pr = 6.2$, $t = 1$, $Rd = 0.5$ and $Q = 0.5$

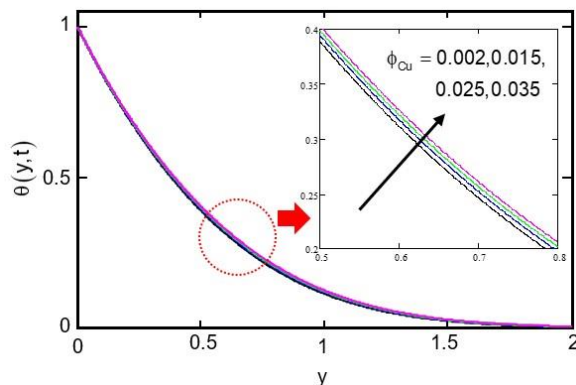


Fig. 21. Temperature profile for different value of φ_{Cu} , when $\varphi_{Al_2O_3} = 0.005$, $Pr = 6.2$, $t = 1$, $Rd = 0.5$ and $Q = 0.5$

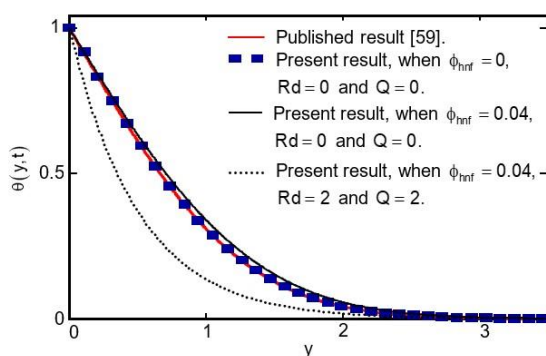


Fig. 22. Comparison of temperature profile in Eq. (36) and Eq. (89) with Eq. (18) by Khan [59], when $Pr = 6.2$ and $t = 3$

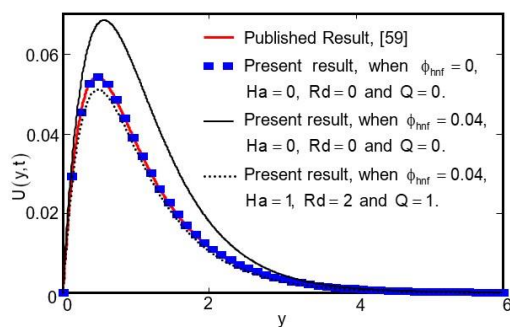


Fig. 23. Comparison of velocity profile in Eq. (64) and Eq. (90) with Eq. (31) published by Khan [59], when $\lambda_1 = \lambda = 0$, $Ha = 1$, $Gr = 1$, $Pr = 6.2$ and $t = 1$

7. Conclusions

This article presented an analytical solution to an unsteady Jeffrey hybrid nanofluid with heat absorption and radiation effects. This problem is tackled by the Laplace transform method. The impacts of the embedded parameters on the Jeffrey hybrid nanofluid velocity and temperature are illustrated in graphs and discussed in detail. Moreover, the main findings from the discussion above are as follows:

- i. The limiting case of the obtained result Eq. (89) and Eq. (90) are found in excellent mutual agreement with the previous study by Khan [59]. Thus, the accuracy of the obtained result is validated.
- ii. Enhancement of the Jeffrey hybrid nanofluid velocity when Rd and Gr are increased.
- iii. Jeffrey hybrid nanofluid velocity decreases as Q , Pr and φ_{hnf} increase.
- iv. Temperature profiles increase when Rd , t and φ_{hnf} increase.
- v. Interestingly, when $\lambda_1 = 0$, the present study can be reduced to unsteady free convection flow of MHD second grade hybrid nanofluid under influence of radiation and heat absorption effects as mentioned in Eq. (77).

The analysis of this analytical solution can be a reference for numerical and experimental works, as it could reduce the time and cost required to conduct an experiment as well as numerical study validation.

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