

# Saturated Porous Ferroconvection in a Ferrofluid Layer with Viscosity as a Function of Magnetic Field: Focus on Convective Boundary Condition

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ARTICLE INFO	ABSTRACT
<b>Article history:</b> Received 8 November 2023 Received in revised form 11 February 2024 Accepted 23 February 2024 Available online 15 March 2024	The present work aims to examine the influence of magnetic field dependent (MFD) viscosity on the onset of ferroconvection in a horizontal porous layer saturated with a quiescent ferrofluid and subjected to a uniform vertical magnetic field. It is assumed that the porous boundaries at the bottom and top are rigid-paramagnetic. The thermal conditions consist of a constant heat flux at the lower surface and a convective boundary condition at the upper surface, encompassing fixed temperature and uniform heat flux cases. The application of the Galerkin technique to the resulting eigenvalue problem reveals that the stability region expands as the porous parameter, Biot number, MFD viscosity parameter and magnetic suscentibility increase in magnitude. Conversely, the
<i>Keywords:</i> Ferroconvection; porous medium layer; Galerkin method; MFD viscosity; paramagnetic boundaries	stability region contracts as the magnetic number and non-linearity of magnetization increase. Furthermore, it is noted that under uniform heat flux boundary conditions, the criterion for the initiation of ferroconvection remains unaffected by the non-linearity of fluid magnetization.

#### 1. Introduction

Ferrofluids are versatile materials that have garnered significant attention in recent decades due to their unique properties and wide-ranging applications. An ferrofluids is a colloidal suspension of magnetic nanoparticles, typically iron oxide or cobalt ferrite, stably dispersed in a carrier fluid, often a hydrocarbon-based solvent or water. First developed by NASA in the 1960s for space-related applications, ferrofluids have since found a wide array of applications in engineering, medicine, electronics, and various other fields. Some of the notable applications include magnetic sealing, damping, drug delivery systems, loudspeaker technology and cooling in electronics [1-5].

Numerous research studies have been undertaken to examine the phenomenon of convection in ferrofluids through porous media [6-10]. The ferrofluid's magnetic properties, the porous material's structure, and outside influences like gravity and a magnetic field all have an impact on the flow patterns and heat transmission characteristics. Qin and Chadam [11] extended the nonlinear stability

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analysis to consider thermal convection in a ferrofluid-saturated porous medium with inertial effects by adopting the Darcy-Forchheimer model. Borglin et al., [12] shown through experimentation that using permanent magnets generated a predictable pressure gradient that induced fluid flow, allowing ferrofluid to be retained in the porous media in predetermined configurations solely determined by the magnetic field. Shivakumara et al., [13] analyzed the impact of vertical permeability heterogeneity on the onset of ferroconvection in a horizontal layer of magnetized Darcy porous media that is saturated with ferrofluid for various permeability function forms. Nanjundappa et al., [14] elucidated the influence of cubic temperature profiles on the initiation of ferroconvection in a Brinkman porous medium under a uniform vertical magnetic field. Control volume based finite element method was employed by Li et al., [15] to simulate ferrofluid migration due to magnetic forces in a porous cylinder using a single-phase model to predict nanofluid characteristics. Siddiqui and Turkyilmazoglu [16] employed the modified Rosensweig-model to numerically investigate heat transfer in a water-based ferrofluid enclosed porous cavity with a novel permeable chamber using the successive-overrelaxation method (SOR). A linear stability analysis was conducted by Senin et al., [17] to examine how internal heating and variable gravity in an anisotropic porous medium affect the initiation of Benard-Marangoni convection in a ferrofluid layer system. Nanjundappa et al., [18] investigated theoretically the penetrative ferro-thermal-convection (FTC) via internal heating in a ferrofluid-saturated porous layer for different types of velocity, temperature and magnetic potential bounding surfaces. Saeed et al., [19] employed the RK4 shooting method to investigate the influence of temperature-dependent viscosity (TDV) and thermal conductivity on ferrofluid (FF) flow through a porous medium adjacent to a vertically stretching surface. The initial flow of immiscible fluids in a porous medium subjected to a rapid pressure gradient and a transverse magnetic field was studied by Goyal and Srinivas [20] to explore the influence of Hartmann number and porous medium parameters on the system's physical characteristics.

In ferrofluid saturating a porous media, Sunil and Sharma [21] studied the effect of MFD viscosity on thermo--solutal convection, taking into account a fluid layer heated and soluted from below in the presence of a uniform magnetic field with two free boundaries. Nanjundappa *et al.*, [22] investigated the impact of MFD viscosity on the initiation of Bénard–Marangoni ferroconvection with rigid-free boundaries to obtain the critical stability parameters using the Rayleigh–Ritz method. Bhandari [23] analyzed the influence of MFD viscosity on ferrofluid flow around a rotating disk in the existence of a stationary magnetic field using the Neruinger-Rosensweig model and solving the nonlinear coupled equations with Flex PDE. Molana *et al.*, [24] examined the natural convection heat transfer of Fe<sub>3</sub>O<sub>4</sub>-water nanofluids with MFD viscosity in a unique porous cavity geometry under a constant inclined magnetic field. The impact of a perpendicular magnetic field on the flow of micropolar nanofluid over an impermeable stretching sheet in a porous medium and the combined convection heat transfer was investigated by Izadi *et al.*, [25] in relation to the control of MFD viscosity. Savitha *et al.*, [26] examined the impact of viscosity at MFD and energy-based volumetric internal heating in conjunction involving ferrofluid-saturated porous layers on convection Robin-type thermal and magnetic potential boundary conditions.

Each of the aforementioned investigations has focused on isothermal boundary conditions at the ferrofluid layer's surfaces. In spite of this, these conditions might prove to be overly restrictive when actual situations are taken into account. Hence, the purpose of this research is to investigate the impact of MFD viscosity on Brinkman-Bénard ferroconvection while relaxing the temperature boundary conditions. This is accomplished by assuming a rigid-paramagnetic lower surface with a constant heat flux and a general type of boundary condition on the upper rigid-paramagnetic boundary. The solution to the subsequent eigenvalue problem is numerically determined using the Galerkin method with second-order Chebyshev polynomials as trial functions.

## 2. Mathematical Formulation

The system investigated comprises of a horizontal layer of porous medium which is saturated with ferrofluid which is initially quiescent and has an applied vertical magnetic field  $(H_0)$ . The physical configuration is depicted in Figure 1. The porous layer thickness d between the two surfaces and edge effects are neglected due to its large horizontal extension. The bottom surface of the porous layer serves as the origin of the Cartesian coordinate system (x, y, z) used, and gravity operates in the negative z-direction,  $\vec{g} = -g \hat{k}$ , represented by the unit vector  $\hat{k}$ . Notably, experimental evidence by Rosensweig *et al.*, [27] has shown that the viscosity of ferrofluids exhibits significant variations with respect to the applied magnetic field. As an initial approximation, the assumption is that the viscosity changes linearly with the magnetic field in the approach,  $\eta = \eta_0(1 + \vec{\delta} \cdot \vec{B})$ , where  $\eta$  is the magnetic viscosity,  $\vec{\delta}$  is the coefficient of variation of the MFD viscosity, which is assumed to be independent of the location (i.e.,  $\delta_x = \delta_y = \delta_z = \delta$ ), while  $\eta_0$  represents the ferrofluid's viscosity in the absence of the magnetic field and  $\vec{B}$  is the magnetic induction. Additionally, the fluid is considered to be incompressible, and its density variation, following the Boussinesq approximation, can be expressed as

$$\rho = \rho_0 [1 - \alpha_t (T - T_0)] \tag{1}$$

where  $\rho$  is the fluid density, T is the Temperature,  $T_0$  is the lower boundary's temperature,  $\alpha_t$  is the thermal expansion coefficient and  $\rho_0$  is the reference density at temperature  $T_0$ .

A condition of the type for a constant heat flux exists at the lower surface (z=0) is

$$-k_1 \frac{\partial T}{\partial z} = q_0 \tag{2}$$

where  $k_1$  is the thermal conductivity,  $q_0$  is the conductive thermal flux.

Utilizing a general thermal boundary condition at the upper surface (z = d) of the form

$$-k_1 \frac{\partial T}{\partial z} = h_t (T - T_\infty)$$
(3)

where  $h_t$  is heat transfer coefficient and  $T_\infty$  is temperature in the bulk of the environment.



The governing equations of continuity, momentum, energy and Maxwell equations respectively are given by Eq. (4)-(7) respectively.

$$\nabla \cdot \vec{q} = 0 \tag{4}$$

$$\rho_0 \left[ \frac{1}{\varepsilon} \frac{\partial \vec{q}}{\partial t} + \frac{1}{\varepsilon^2} (\vec{q} \cdot \nabla) \vec{q} \right] = -\nabla \mathbf{p} + \rho \, \vec{g} - \frac{\eta}{k} \vec{q} + 2\nabla \cdot (\eta \, \underline{\underline{D}}) + \rho_0 (\vec{M} \cdot \nabla) \vec{H}$$
(5)

$$\varepsilon \left[ \rho_0 C_{V,H} - \mu_0 \vec{H} \cdot \left( \frac{\partial \vec{M}}{\partial T} \right)_{V,H} \right] \frac{DT}{Dt} + (1 - \varepsilon)(\rho_0 C)_s \frac{\partial T}{\partial t} + \mu_0 T \left( \frac{\partial \vec{M}}{\partial T} \right)_{V,H} \cdot \frac{D\vec{H}}{Dt} = k_1 \nabla^2 T$$
(6)

$$\nabla \cdot \vec{B} = 0, \ \nabla \times \vec{H} = 0 \text{ or } \vec{H} = \nabla \varphi$$
 (7)

where  $\vec{q} = (u, v, w)$  is velocity vector, p is the pressure,  $\varepsilon$  is the porosity of the porous medium, t is the time, k is the permeability of the porous medium,  $\underline{D} = [\nabla \vec{q} + (\nabla \vec{q})^T]/2$  is the rate of strain tensor,  $\vec{M}$  is Magnetization,  $\vec{H}$  magnetic field's strength,  $C_{V,H}$  is the specific heat at constant volume and magnetic field,  $\varphi$  is the magnetic potential, while the subscript s denotes the porous media.

Further,  $\vec{B}$  ,  $\vec{M}$  and  $\vec{H}$  are related by

$$\vec{B} = \mu_0 \left( \vec{M} + \vec{H} \right) \tag{8}$$

with

$$\vec{M} = \frac{\vec{H}}{H} M(H,T).$$
(9)

Eq. (10) denotes the linearized magnetic equation of state with respect to  $\,H_0\,$  and  $\,T_0\,$ 

$$M = M_0 + \chi (H - H_0) - K (T - T_0)$$
(10)

where  $\mu_0$  is the vacuum's free space magnetic permeability,  $\chi$  is the magnetic susceptibility and K is the pyromagnetic co-efficient.

The initial state is considered to be at rest and can be described by the following expression:

$$\vec{q}_b = 0, \ \rho = \rho_b(z), \ \eta = \eta_b(z), \ p = p_b(z), \ T = T_b(z), \ \vec{H} = \vec{H}_b(z), \ \vec{M} = \vec{M}_b(z)$$
 (11)

where subscript b denotes the basic state.

Using Eq. (11), Eq. (5) and Eq. (6), respectively, yield

$$\frac{dp_b}{dz} = -\rho_0 \left[ 1 - \alpha_t \left( T_b - T_0 \right) \right] g \,\hat{k} + \mu_0 M_b \frac{dH_b}{dz} \tag{12}$$

$$\frac{d^2 T_b}{dz^2} = 0 \tag{13}$$

Upon solving Eq. (13) with consideration of the boundary conditions of Eq. (2) and Eq. (3), the result obtained is as follows:

$$T_b(z) = -\beta z + \frac{q_0}{h_t} + T_\infty + \beta d$$
(14)

where  $\beta = q_0 / k_1$  is the temperature gradient.

Upon substituting the basic state Eq. (11) into Eq. (7) and utilizing Eq. (8) and Eq. (10), the magnetic field intensity and magnetization for the basic state is determined as demonstrated in Finlayson [28].

$$\vec{H}_{b}(z) = \left[H_{0} - \frac{K\beta z}{1+\chi}\right]\hat{k}$$
(15)

$$\vec{M}_{b}(z) = \left[M_{0} + \frac{K\beta z}{1+\chi}\right]\hat{k}$$
(16)

where  $M_0 + H_0 = H_0^{ext}$ .

Using Eq. (12) to Eq. (14) in Eq. (10) and integrating, we obtain

$$p_b(z) = p_0 - \rho_0 g \, z - \frac{1}{2} \rho_0 \alpha_t g \beta \, z^2 - \frac{\mu_0 M_0 \kappa \beta}{1 + \chi} \, z - \frac{\mu_0 \kappa^2 \beta^2}{2(1 + \chi)^2} \, z^2 \tag{17}$$

To investigate the system's stability, a small disturbance is applied to the system, and the variables are perturbed in the form:

$$\vec{q} = \vec{q}', \ p = p_b(z) + p', \ \eta = \eta_b(z) + \eta', \ T = T_b(z) + T', \ \vec{H} = \vec{H}_b(z) + \vec{H}', \ \vec{M} = \vec{M}_b(z) + \vec{M}'$$
(18)

The perturbed variables  $\vec{q}', p', \eta', T', \vec{H}'$  and  $\vec{M}'$  are assumed to be negligible. Eq. (17) is substituted into Eq. (8) and Eq. (9), and Eq. (7) is used and ignoring the primes in the notation,

$$H_{x} + M_{x} = \left(1 + \frac{M_{0}}{H_{0}}\right)H_{x}, \quad H_{y} + M_{y} = \left(1 + \frac{M_{0}}{H_{0}}\right)H_{y}, \quad H_{z} + M_{z} = \left(1 + \chi\right)H_{z} - KT$$
(19)

The above equations are derived under the assumption that  $K\beta d \ll (1+\chi) H_0$ . Substituting the perturbation Eq. (18) into momentum Eq. (5) and linearizing, we obtain (after neglecting the primes)

$$\rho_0 \frac{\partial u}{\partial t} = -\frac{\partial p}{\partial x} - \frac{\eta_b}{k} u + \eta_b \nabla^2 u + \mu_0 (M_0 + H_0) \nabla^2 u + \frac{\partial H_x}{\partial z}$$
(20)

$$\rho_0 \frac{\partial v}{\partial t} = -\frac{\partial p}{\partial y} - \frac{\eta_b}{k} v + \eta_b \nabla^2 v + \mu_0 (M_0 + H_0) \nabla^2 v + \frac{\partial H_y}{\partial z}$$
(21)

$$\rho_0 \frac{\partial w}{\partial t} = -\frac{\partial p}{\partial z} - \frac{\eta_b}{k} w + \eta_b \nabla^2 w + \mu_0 (M_0 + H_0) \nabla^2 w + \frac{\partial H_z}{\partial z} + \rho_0 \alpha_t g T - \mu_0 K \beta H_z + \frac{\mu_0 K^2 \beta T}{1 + \chi}$$
(22)

where  $\eta_b = \eta_0 [1 + \delta \mu_0 (M_0 + H_0)]$  and  $\nabla^2 = \partial^2 / \partial x^2 + \partial^2 / \partial y^2 + \partial^2 / \partial z^2$  is the Laplacian operator.

Eq. (20) and Eq. (21) can be partially differentiated with respect to x and y, respectively, and added, we obtain

$$\nabla_{h}^{2} p = \rho_{0} \frac{\partial}{\partial z} \left( \frac{\partial w}{\partial t} \right) + \frac{\eta_{b}}{k} \frac{\partial w}{\partial z} - \eta_{b} \frac{\partial}{\partial z} \left( \nabla^{2} w \right) + \mu_{0} (M_{0} + H_{0}) \frac{\partial}{\partial z} \left( \frac{\partial H_{x}}{\partial x} + \frac{\partial H_{y}}{\partial y} \right)$$
(23)

where  $\nabla_h^2 = \partial^2 / \partial x^2 + \partial^2 / \partial y^2$  is the horizontal Laplacian operator

Eq. (22) is simplified by substituting Eq. (23) to eliminate the pressure term, we obtain

$$\left(\rho_0 \frac{\partial}{\partial t} + \frac{\eta_b}{k} - \eta_b \nabla^2\right) \nabla^2 w = -\mu_0 K \beta \frac{\partial}{\partial z} \left(\nabla_h^2 \varphi\right) + \frac{\mu_0 K^2 \beta}{1 + \chi} \nabla_h^2 T + \rho_0 \alpha_t g \nabla_h^2 T$$
(24)

As before, substituting Eq. (18) into Eq. (6), linearizing and the resulting equation upon using  $\vec{H} = \nabla \varphi$ , we obtain (after neglecting primes)

$$(\rho_0 C)_1 \frac{\partial T}{\partial t} - \mu_0 T_0 K \frac{\partial}{\partial t} \left( \frac{\partial \varphi}{\partial z} \right) = k_1 \nabla^2 T + \left[ (\rho_0 C)_2 - \frac{\mu_0 T_0 K^2}{1 + \chi} \right] w \beta$$
(25)

where  $(\rho_0 C)_1 = \varepsilon \rho_0 C_{V,H} + \varepsilon \mu_0 H_0 K + (1-\varepsilon)(\rho_0 C)_s$  and  $(\rho_0 C)_2 = \varepsilon \rho_0 C_{V,H} + \varepsilon \mu_0 H_0 K$ .

After substituting Eq. (18) and using Eq. (19), Eq. (7) can be rewritten (omitting the primes) as

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$$\left(1 + \frac{M_0}{H_0}\right) \nabla_h^2 \varphi + \left(1 + \chi\right) \frac{\partial^2 \varphi}{\partial z^2} - K \frac{\partial T}{\partial z} = 0$$
(26)

It is expected that the dependent variables' normal mode expansion will have the form

$$\{w, T, \varphi\} = \{W(z), \Theta(z), \Phi(z)\} \exp[i(\ell x + my) + \omega t]$$
(27)

where W,  $\Theta$  and  $\Phi$  are the amplitudes of the perturbed vertical component velocity, temperature and magnetic potential respectively, while  $\omega$  is the growth rate and  $\ell$ , m are the wave numbers in the x and y directions.

After substituting normal mode expansion Eq. (27) into Eq. (24) to Eq. (26) and then all the variables are non-dimensionalized using the following relations

$$z^{*} = \frac{z}{d}, \quad W^{*} = \frac{d}{vA}W, \quad t^{*} = \frac{v}{d^{2}}t, \quad \omega^{*} = \frac{d^{2}}{v}\omega, \quad \Theta^{*} = \frac{\kappa}{\beta v d}\Theta,$$

$$\Phi^{*} = \frac{(1+\chi)\kappa}{\kappa\beta v d^{2}} \Phi \text{ and } \delta^{*} = \mu_{0}(M_{0} + H_{0})\delta \qquad (28)$$

where  $v = \eta_0 / \rho_0$  is the kinematic viscosity,  $A = (\rho_0 C)_1 / (\rho_0 C)_2$  is the heat capacity ratio and  $\kappa = k_1 / (\rho_0 C)_2$  is the thermal diffusivity.

To obtain the ordinary differential equations of the form (omitting the asterisks),

$$\left[(1+\delta)\left\{(D^2-a^2)-\sigma^2\right\}-\omega\right](D^2-a^2)W = -a^2\left[ND\Phi-(R+N)\Theta\right]$$
(29)

$$\left(D^2 - a^2 - \Pr\omega\right)\Theta - \Pr M_2\omega D\Phi = -(1 - M_2 A)W$$
(30)

$$\left(D^2 - a^2 M_3\right)\Phi = D\Theta \tag{31}$$

where D = d/dz is differential operator,  $a = \sqrt{l^2 + m^2}$  is the horizontal wave number,  $\sigma^2 = d/\sqrt{k}$  is the porous parameter,  $R = \alpha_t g \beta d^4 / v \kappa A$  is the thermal Rayleigh number,  $M_1 = \mu_0 K^2 \beta / (1 + \chi) \alpha_t \rho_0 g$  is the magnetic number,  $N = RM_1 = \mu_0 K^2 \beta^2 d^4 / (1 + \chi) \eta_0 \kappa A$  is the magnetic Rayleigh number,  $Pr = v/\kappa$  is the Prandtl number,  $M_2 = \mu_0 T^2 K^2 / (1 + \chi) (\rho_0 C)_s$  is the magnetic parameter,  $M_3 = (1 + M_0 / H_0) / (1 + \chi)$  is the Magnetization parameter's nonlinearity.

Owing to its average value for ferrofluid with various carrier liquids, which is of the order of  $10^{-6}$ , the effect of  $M_2$  is ignored in comparison to unity [28].

The ordinary differential Eq. (29) to Eq. (31) are solved using the following boundary conditions

$$W = DW = (1 + \chi)D\Phi - a\Phi = D\Theta = 0$$
 at  $z = 0$  (on the lower rigid-paramagnetic) (32)

 $W = DW = (1 + \chi)D\Phi + a\Phi = D\Theta + Bi\Theta = 0 \text{ at } z = 1 \text{ (at the upper rigid-paramagnetic)}$ (33)

The case Bi = 0 and  $Bi \rightarrow \infty$  to upper boundary conditions with constant heat flux and temperature, respectively.

#### 3. Method of Solution

Considering the validity of the principle of exchange of stability, we set  $\omega = 0$  in Eq. (29) to Eq. (31) and simplifying, we get

$$\left[ (1+\delta)(D^2 - a^2 - \sigma^2) \right] (D^2 - a^2) W = -a^2 R \left[ M_1 D \Phi - (1+M_1) \Theta \right]$$
(34)

$$(D^2 - a^2)\Theta = -W \tag{35}$$

$$(D^2 - a^2 M_3) \Phi - D\Theta = 0$$
 (36)

The eigenvalue problem, consisting of Eq. (29) to Eq. (31) along with the selected boundary conditions Eq. (32) and Eq. (33), is mathematically resolved using the Galerkin Method to obtain R as the eigenvalue. Consequently, W,  $\Theta$  and  $\Phi$  are expressed as follows.

$$W = \sum_{i=1}^{n} A_i W_i(z), \quad \Theta(z) = \sum_{i=1}^{n} C_i \ \Theta_i(z), \quad \Phi(z) = \sum_{i=1}^{n} D_i \ \Phi_i(z)$$
(37)

The unknown constants,  $A_i$ ,  $C_i$  and  $D_i$  are determined through the chosen base functions  $W_i(z)$ ,  $\Theta_i(z)$  and  $\Phi_i(z)$ , which are generally selected to satisfy the corresponding boundary conditions. After substituting Eq. (37) into Eq. (34) to Eq. (36), the resulting equations are respectively multiplied with  $W_j(z)$ ,  $\Theta_j(z)$  and  $\Phi_j(z)$ . The equations obtained are subsequently integrated by parts between the lower and upper limits of z i.e., (0, 1) and are evaluated using boundary conditions. The resulting equations constitute a system of linear homogeneous algebraic equations:

$$C_{ji}A_i + D_{ji}C_i + E_{ji}D_i = 0 ag{38}$$

$$F_{ji}A_i + G_{ji}C_i = 0 aga{39}$$

$$H_{ji}C_i + I_{ji}D_i = 0. (40)$$

The inner products of the basic functions are involved in the coefficients  $C_{ji} - I_{ji}$ , which are provided by

$$C_{ji} = (1+\delta)[< D^2 W_j D^2 W_i > + (2a^2 + \sigma^2) < DW_j DW_i > +a^2(a^2 + \sigma^2) < W_j W_i >]$$
  
$$D_{ji} = -a^2 R (1+M_1) < W_j \Theta_i >$$
  
$$E_{ji} = a^2 R M_1 < W_j D\Phi_i >$$

$$\begin{split} F_{ji} &= - \langle \Theta_{j} W_{i} \rangle \\ G_{ji} &= Bi \Theta_{j}(1) \Theta_{i}(1) + \langle D\Theta_{j} D\Theta_{i} \rangle + a^{2} \langle \Theta_{j} \Theta_{i} \rangle \\ H_{ji} &= - \langle D\Phi_{j} \Theta_{i} \rangle \\ I_{ji} &= \frac{a}{1 + \chi} \Big[ \Phi_{j}(1) \Phi_{i}(1) + \Phi_{j}(0) \Phi_{i}(0) \Big] + \langle D\Phi_{j} D\Phi_{i} \rangle + a^{2} M_{3} \langle \Phi_{j} \Phi_{i} \rangle \Big] \end{split}$$

where  $\langle \cdots \rangle = \int_{0}^{1} (\cdots) dz$  is the specification of the inner product.

There is a non-trivial solution to the set of homogeneous algebraic equations stated above if and only if

$$\begin{vmatrix} C_{ji} & D_{ji} & E_{ji} \\ F_{ji} & G_{ji} & 0 \\ 0 & H_{ji} & I_{ji} \end{vmatrix} = 0.$$
 (41)

The extraction of eigenvalues from Eq. (41) is done by selecting the trial functions as

$$W_i = (z^4 - 2z^3 + z^2)T_{i-1}^*, \quad \Theta_i = z^2(1 - 2z/3)T_{i-1}^*, \quad \Phi_i = (z - 1/2)T_{i-1}^*$$
(42)

In the process of solving the eigenvalue problem, trial functions are used to approximate the solutions for the dependent variables  $W_i$ ,  $\Theta_i$  and  $\Phi_i$ . These trial functions are represented by the modified Chebyshev polynomials, denoted as  $T_i^*$ 's. However, these trial functions may not satisfy the boundary conditions initially. To address this, the residual technique is employed. The residual term, which appears as the first term on the right-hand side of the characteristic equations  $G_{ji}$  and  $I_{ji}$ , accounts for the deviation of the trial functions from the actual boundary conditions. By incorporating this residual term, the characteristic equation can accurately describe the behavior of the system. The extracted eigenvalue determines the stability of the system and provide crucial information about the convection behavior of the ferrofluids flowing through porous media under the influence of a magnetic field.

Eq. (41) allows for the derivation of a relation with the characteristic parameters of the following type

$$f(R, \delta, \sigma^2, Bi, N, M_1, M_3, a) = 0$$
 (43)

Numerical analysis is utilized to determine the critical value of R,  $(i.e., R_c)$  corresponding to various values of wave number a by varying it for different  $\delta$ , N,  $\sigma^2$ , Bi,  $M_1$  and  $M_3$ .

#### 4. Results

The effect of MFD viscosity on the initiation of Brinkman-Benard ferroconvection in a horizontal ferrofluid-saturated porous layer under the influence of a uniform vertical magnetic field is examined. The analysis is conducted using linear stability theory. In order to establish the rigid-

paramagnetic nature of the upper and lower boundaries of the porous layer, a general thermal condition is applied to the upper boundary and a uniform heat flux condition is applied to the lower boundary. Numerically, the eigenvalue problem that results is resolved by employing the Galerkin method. Initially, we verify the numerical method employed through a comparison of the critical Rayleigh number ( $R_c$ ) and the corresponding critical wave number ( $a_c$ ) with the values reported by Sparrow *et al.*, [29] for a conventional viscous fluid. It has been noted that in order to achieve convergent results, six terms (n = 6) are necessary in the series expansion of Eq. (37). A comparison between our findings and those of Sparrow *et al.*, [29] for different Biot numbers (Bi) in the limiting case of  $M_1=0$ ,  $M_3=0$ ,  $\sigma=0$  and  $\delta=0$  (i.e., ordinary viscous fluid) is presented in Table 1. The correctness of the numerical process used to identify the essential stability parameters is confirmed by the good agreement between the two methods.

$R_c$ and	$R_c$ and $a_c$ comparison for various $Bi$						
Bi	Sparrow et al., [2	.9]	Present analysis				
_	Rigid- Rigid		Rigid-Rigid				
	$R_c$	$a_c$	$R_c$	$a_c$			
0	720.000	0.00	720.000	0.000			
0.01	747.765	0.71	747.765	0.7126			
0.03	768.153	0.93	768.155	0.9283			
0.1	807.676	1.23	807.676	1.2281			
0.3	869.231	1.57	869.208	1.5571			
1	974.173	1.94	974.172	1.9427			
3	1093.744	2.24	1093.74	1.2419			
10	1204.571	2.44	1204.57	2.4367			
30	1259.884	2.51	1259.91	2.5110			
100	1284.263	2.53	1284.28	2.5394			
$\infty$	1295.781	2.55	1295.78	2.5490			

Table 1 $R_c$  and  $a_c$  comparison for various Bi

The value of  $R_c$  by corresponding the wave numbers  $a_c$  obtained for different physical parameters  $\delta$ ,  $\sigma^2$ , N, Bi, M<sub>1</sub>, M<sub>3</sub> and  $\chi$  are presented graphically in Figure 2 to Figure 6. The effect of the Biot number (Bi) on the critical Rayleigh number ( $R_c$ ) is studied while considering the variation of MFD viscosity in the context of Brinkman-Benard ferroconvection in Figure 2. Assigned to the boundary of the porous medium, the Biot number quantifies the relationship between the internal thermal resistance of the solid matrix and the external thermal resistance at the boundary of the porous medium. The initiation of convection in such systems is significantly influenced by it. The variation of critical Rayleigh number  $R_c$  and wave number  $a_c$  is shown in Figure 2(a) and Figure 2(b) respectively as a function of MFD viscosity parameter  $\delta$  for different Bi and  $\chi$  when  $M_3 = 1$ ,  $M_1 = 5$  and  $\sigma^2 = 50$ . Figure 2(a) illustrates that  $R_c$  increases with an increment in MFD viscosity parameter ( $\delta$ ), resulting in a stabilizing effect and delaying the onset of ferroconvection. Additionally, the variation in Bi from 0 to 2 significantly impacts the critical Rayleigh number,  $R_c$ with the most stable condition observed for Bi = 0 and the least stable for Bi = 2, as the system changes from an insulated to a conductive upper boundary. Moreover, the system exhibits higher stability with paramagnetic boundaries having large susceptibility  $(1 + \chi = 10^4)$  compared to  $\chi = 0$ , although the control of magnetic susceptibility diminishes as  $\chi$  increases. This finding aligns with the results obtained by Gotoh and Yamada [30]. On the other hand, Figure 2(b) demonstrates that an increase in Bi and  $\chi$  leads to an increase in the critical wave number  $(a_c)$ , reducing the size of convection cells, while  $\delta$  does not affect the critical wavenumber. This behavior holds the initiative that higher values of Bi lead to enhanced thermal conductivity within the porous medium, allowing heat to be transported more efficiently. As the magnetic susceptibility increases, the ferrofluid becomes more responsive to the magnetic field, leading to stronger magnetization effects. This enhanced magnetization creates stronger interactions between magnetic particles in the fluid, affecting its flow behavior. The increased magnetic response results in a more stable system, requiring higher convective instability (higher critical Rayleigh number) to trigger convection.



Figure 3(a) and Figure 3(b) display the variation of  $R_c$  and  $a_c$  respectively, as a function of MFD viscosity  $\delta$  to examine the influence of the porous medium's coarseness on the onset of ferroconvection for different values of  $\sigma^2$  and  $\chi$  with fixed values of  $M_1 = 5$ ,  $M_3 = 1$  and Bi = 2. When the porous parameter  $\sigma^2$  increases for a fixed thickness of the porous layer, it leads to a decrease in the permeability of the porous medium. This behavior can be attributed to the decreased fluid flow caused by a larger porous parameter  $\sigma^2$ , which hinders the convective heat transfer within the system. The reduced flow velocities restrict the transport of heat and result in less efficient mixing of the fluid, delaying the onset of ferroconvection. Thus, it requires higher heating and a higher value of the thermal Rayleigh number for the onset of ferroconvection in the ferrofluid-saturated porous medium. Figure 3(b) demonstrates that in the absence of the pyromagnetic coefficient ( $\chi = 0$ ), an increase in  $\sigma^2$  causes cell size  $a_c$  to become destabilizing. However, for a high pyromagnetic coefficient ( $1 + \chi = 10^4$ ) an increase in  $\sigma^2$  results in a stabilizing nature of cell size  $a_c$ .



By plotting the critical Rayleigh number  $R_c$  against the MFD viscosity parameter  $\delta$ , Figure 4(a) illustrates the influence of the magnetic number  $M_1$  on the initiation of ferroconvection for  $M_3 = 1$ ,  $\sigma^2 = 50$  and Bi = 2. The magnetic number  $(M_1)$  is a dimensionless parameter that characterizes the relative strength of the magnetic forces to buoyancy forces in a ferrofluid system. When the magnetic number is increased, it implies that the magnetic forces become more dominant compared to buoyancy forces. An increase in the magnetic number is observed to have a destabilizing effect. This pattern can be explained by attributing it to the enhanced magnetic response of the ferrofluid as the magnetic number increases. The stronger magnetic forces lead to more vigorous fluid motion and heat transfer, promoting convection at lower thermal gradients. The stronger magnetic field enhances the interaction between magnetic particles in the ferrofluid, leading to more significant disturbances and convection. On the other hand, a lower magnetic number would result in a more stable system with smaller and less pronounced convection cells. The observed trend in Figure 4(b) reveals that with an increase in the magnetic number  $(M_1)$ , the critical wave number  $(a_c)$  also increases, leading to a reduction in the size of convection cells. This implies that as the magnetic field strength increases, the convection cells become smaller and more compact, indicating a more organized and stable flow pattern within the ferrofluid-saturated porous layer.

Figure 5(a) illustrates the impact of the nonlinearity of fluid magnetization  $(M_3)$  on the onset of ferroconvection. The curves of  $R_c$  versus  $\delta$  are shown for different  $M_3$  and  $\chi$  when  $\sigma^2 = 50$ ,  $M_1 = 5$  and Bi = 2. The non-linearity of fluid magnetization refers to the deviation of the magnetic response of ferrofluid from a simple linear relationship with the applied magnetic field. In ferrofluids, the magnetization is often dependent on both the magnitude of the magnetic field and the temperature, resulting in non-linear behavior. The pyromagnetic coefficient quantifies the rate at which the magnetization changes with temperature. The graph demonstrates that an increase in  $M_3$  has a destabilization caused by  $M_3$  is relatively small. This can be explained by the fact that when the pyromagnetic coefficient is large, the magnetization becomes highly dependent on temperature, making it more non-linear. This non-linearity of magnetization has significant implications for the behavior of the ferrofluid in response to external magnetic fields and thermal gradients, which accelerates the initiation of convection due to a reduction in stability region. Similar patterns of

behavior are seen in the case of critical wave numbers, as shown in Figure 5(b), where an increase in  $M_3$  causes a decrease in  $a_c$  and a resulting increase in convection cell size.



**Fig. 4.** Variation of (a)  $R_c$  and (b)  $a_c$  as a function of  $\delta$  for different  $M_1$  and  $\chi$  for  $M_3 = 1$ ,  $\sigma^2 = 50$ , Bi = 2



The combined influence of buoyancy and magnetic forces is depicted in Figure 6 through the locus of  $R_c$  and  $N_c (N_c = R_c M_1)$  for various  $M_3$  and  $\chi$  when  $\sigma^2 = 50$ ,  $\delta = 0.02$  and Bi = 2. The relationship between  $R_c$  and  $N_c$  is inversely proportional. For  $M_3 \rightarrow \infty$  case, the data aligns with the correlation

$$\frac{R_c}{R_{c0}} + \frac{N_c}{N_{c0}} = 1$$

as observed in the non-porous case for constant viscosity ferrofluids [28, 30]. Here,  $R_{c0}$  is the critical thermal Rayleigh number without magnetic field (N = 0) and  $N_{c0}$  is the critical magnetic Rayleigh number in the absence of gravity (R = 0).



The values of the critical stabilities parameters  $R_c$  and  $N_c$  are tabulated for different values of  $\delta$ , Bi,  $\sigma$ ,  $M_3$  and  $\chi$  in Table 2 to 4. From the tables, it is evident that  $R_c$  and  $N_c$  are increasing as a function of MFD viscosity parameter  $\delta$ . In the scenario of negligible buoyancy (i.e., R = 0), it is observed that the critical magnetic Rayleigh number  $N_c$  decreases as  $M_3$  increases. These findings indicate that the ferrofluid-saturated porous layer becomes more susceptible to temperature gradients when influenced by magnetic forces and/or greater non-linearity of the fluid magnetization. As  $M_3$  approaches to infinity, the results converge towards those of the classical Bénard problem, consistent across various magnetic susceptibility values.

δ	$R_c$	$N_c$ ( $R=0$	)				
	(N = 0)	$M_{3} = 1$		$M_3 = 10$		$M_3 \rightarrow \circ$	0
		$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 99999$
0	720	1418.06	2128.58	974.67	1020.21	720	720
0.02	734.4	1446.42	2171.15	994.16	1040.61	734.4	734.4
0.04	748.8	1474.78	2213.72	1013.66	1061.01	748.8	748.8
0.06	763.2	1503.14	2256.29	1033.15	1081.42	763.2	763.2
0.08	777.6	1531.51	2298.86	1052.64	1101.82	777.6	777.6
0.1	792	1559.87	2341.43	1072.14	1122.23	792	792

Table 2	
Variation of $R$ and $N$ for different $\delta$ .	$M_2$ and $\gamma$ when $Bi = \sigma = 0$

Variation of $R_c$ and $N_c$ for different $\delta$ , $M_3$ and $\chi$ when $Bi=0$ and $\sigma=10$								
δ	$R_{c}$	$N_c (R=0)$						
	(N = 0)	$M_{3} = 1$		$M_{3} = 10$		$M_3 \rightarrow \infty$		
		$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 9999$	
0	889.511	1782.43	2671.86	1222.77	1282.12	889.511	889.511	
0.02	907.30	1818.08	2725.3	1247.22	1307.76	907.30	907.30	
0.04	925.09	1853.73	2778.74	1271.68	1333.4	925.09	925.09	
0.06	942.88	1889.37	2832.18	1296.13	1359.05	942.88	942.88	
0.08	960.67	1925.02	2885.61	1320.59	1384.69	960.67	960.67	
0.1	978.46	1960.67	2939.05	1345.04	1410.33	978.46	978.46	

## Table 4

Table 3

Variation of  $R_c$  and  $N_c$  for different  $\delta$ ,  $M_3$  and  $\chi$  when Bi=1 and  $\sigma=10$ 

$\delta$	$R_c$	$N_c (R=0)$					
	(N = 0)	$M_{3} = 1$		$M_{3} = 10$		$M_3 \rightarrow \infty$	
		$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 99999$	$\chi = 0$	$\chi = 99999$
0	1222.4	1969.9	2791.06	1402.23	1443.55	1222.4	1222.4
0.02	1246.85	2009.9	2846.88	1430.27	1472.42	1246.85	1246.85
0.04	1271.3	2048.69	2902.7	1458.31	1501.3	1271.3	1271.3
0.06	1295.75	2088.09	2958.52	1486.36	1530.17	1295.75	1295.75
0.08	1320.19	2127.49	3014.34	1514.4	1559.04	1320.19	1320.19
0.1	1344.64	2166.89	3070.16	1542.45	1587.45	1344.64	1344.64

### 4. Conclusions

The investigation focus is on the impact of MFD viscosity on the onset of Brinkman-Bénard ferroconvection in an ferrofluid-saturated porous layer, considering the variable viscosity of ferrofluid under an applied magnetic field. The porous layer is bounded by rigid-paramagnetic surfaces. The eigenvalue problem is numerically solved using the Galerkin technique with Rayleigh number R as the eigenvalue. The obtained results show excellent agreement with previously published works. The present study yields the following conclusions

- i. The MFD viscosity parameter  $\delta$  delays the onset of ferroconvection in the ferrofluid. This means that as the MFD viscosity parameter increases, it hinders the initiation of convection, making the system more stable and requiring higher values of critical Rayleigh number  $R_c$  for the convective motion to occur. The fluid's ability to flow becomes more resistant under the influence of the magnetic field, leading to a slower development of convection compared to the scenario without MFD viscosity.
- ii. The effect of the magnetic number  $M_1$  and nonlinearity of fluid magnetization parameter on  $R_c$  in ferrofluids indicates that increasing the magnetic number enhances the responsiveness of the fluid to the magnetic field, leading to a more efficient fluid flow and heat transfer. As a result, convection is triggered at lower thermal driving forces. Understanding this relationship can help in designing and optimizing magnetic fluid-based systems, where precise control of fluid motion and heat transfer is desired through magnetic fields.

- iii. The critical thermal Rayleigh number ( $R_c$ ) increases as both the Biot number Bi and porous parameter  $\sigma^2$  increase, resulting in a delay in the onset of ferroconvection. This means that higher values of Biot number and porous parameter lead to a more stable system, requiring a higher critical Rayleigh number for the initiation of convection in ferrofluid-saturated porous layer.
- iv. The system exhibits greater stability against ferroconvection when the boundaries are paramagnetic with a large magnetic susceptibility ( $\chi \neq 0$ ), compared to cases with very low susceptibility. The observation shows that ( $R_c$  and  $a_c$ )  $_{\chi \neq 0} > (R_c$  and  $a_c$ )  $_{\chi = 0}$ .
- v. As  $M_3 \rightarrow \infty$ , the results are reduced to those of the classical Rayleigh-Bénard problem due to the non-linearity of magnetization.
- vi. Complementary effects are observed between the buoyancy and magnetic forces, with the system attaining greater stability in the presence of magnetic forces alone.

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