

Optimising The Mixing Ratio of Hybrid Nanofluids Based on Their Thermal Conductivity and Dynamic Viscosity Properties Using Design of Experiment Method

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| ARTICLE INFO | ABSTRACT |
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| Article history: Received 5 May 2022 Received in revised form 30 September 2022 Accepted 10 October 2022 Available online 3 November 2022 Keywords: Hybrid nanofluid; heat transfer; mixing ratio; design of experiment | The hybrid nanofluid's synergetic effect is proportional to the mixing ratio. However, the One Factor at A Time (OFAT) method only displays the optimised mixing ratio when the mixing ratio used in the respective experiments is specified. Thus, the purpose of this study is to optimise the nanoparticle mixing ratio using Design of Experiment (DOE) in Design Expert 11 to cover the entire range of mixing ratios with the fewest experiments possible. The prepared hybrid nanofluid comprises Titanium Dioxide (TiO ₂) and Graphene Nanoplatelets (GNP) at a concentration of 0.3vol%, a mixing ratio ranging from 1:9 to 9:1, and temperature ranging from 30°C to 60°C. However, the DOE method generates only 1:9, 1:1, and 9:1 mixing ratios. ANOVA analysis was used to generate a model for thermal conductivity. Additionally, the optimisation results indicate that a mixing ratio of 1:4 (TiO ₂ -GNP) and a temperature of 40°C are the optimised parameters. The difference between the measured and predicted thermal conductivity values was less than 5% |
| | iess than 5%. |

1. Introduction

Despite increasing nanofluids' thermal properties, many real-world applications require tradeoffs between various nanofluid characteristics/properties. For example, metal oxide nanoparticles exhibit good chemical inertness and stability, while metallic nanoparticles like Aluminum, Copper, Silver possess higher thermal conductivities but are chemically reactive and unstable [1]. Thus, a new type of nanofluid called hybrid nanofluid is created by hybridising two different nanoparticles with unique properties. A hybrid nanofluid is a mixture of two distinct nanoparticles dispersed in a base fluid. The purpose of a hybrid nanofluid is to improve thermal properties compared to a base fluid or a mono-nanofluid through synergistic effects [2,3]. For heat transfer applications, hybrid nanofluid is expected to improve the heat transfer performance, pressure drop, and stability by trade-off the

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advantages and disadvantages of the nanoparticles used [4,5]. Based on a review on hybrid nanofluid done by Sarkar *et al.*, [2] proper hybridisation of hybrid nanofluid shows likely for heat transfer enhancement. Further work is recommended in preparation and stability, characterisation, and applications to address long-term stability, increased pressure drop or pumping power, high viscosity, and unavailability of a suitable thermal conductivity model [6].

Typically, the thermophysical properties of nanofluids depend on the dispersed nanoparticle type, size, shape, concentration, base fluid, operating temperature, and surfactant addition [7-13]. On the other hand, the hybrid nanofluid's synergetic effect is proportional to the mixing ratio. [1,2, 14]. A good synergetic effect of hybrid nanofluid is significant to enhance the thermal properties of the prepared hybrid nanofluid. As a result, the synergetic effect of hybrid nanofluid can be determined by optimising the mixing ratio of the nanoparticles [15-17].

Most researchers use the One factor at a time (OFAT) method to determine the best mixing ratio of hybrid nanofluid. OFAT method is a method of designing experiments involving the testing of factors, or causes, one at a time instead of multiple factors simultaneously. The traditional OFAT approach for optimisation has three serious downsides, which are (a) leading to an unnecessarily large number of experimental runs, (b) unable to study interactions among the factors, (c) time consuming to conduct a large number of experiments [18-20]. As a result, the best response value from the selected mixing ratio shows the best mixing ratio for the respective hybrid nanofluid. Therefore, this study aims to comprehensively optimise the mixing ratio of hybrid nanofluid based on thermal conductivity and viscosity based on statistical analysis.

2. Methodology

2.1 Preparation of Hybrid Nanofluid

A two-step method was used to produce the hybrid nanofluid using Eq. (1). First, a balance is used, AS 310.R2 PLUS Analytical Balance (Figure 1), to prepare the hybrid nanofluid. Various concentrations of 0.3vol% with different ratios of TiO_2 and GNP, which were 1:9 up to 9:1 dispersed in distilled water. Three mixing ratios of hybrid nanofluid had been prepared for each concentration which are 1:9, 1:1, and 9:1. The amount of surfactant used was 1:10 based on the amount of TiO_2 .



Fig. 1. Analytics Balance

Firstly, the required amount of surfactant was mixed with distilled water until it dissolved completely in water using a magnetic stirrer. The colour of the solution becomes apparent as the

surfactant is completely dissolved. After that, the required amount of TiO₂ and GNP was mixed and let the solution stir for 15 minutes. The presence of surfactant dissolved in the distilled water help the nanoparticles and distilled water become homogeneous. However, using the magnetic stirrer was not enough to make the solution homogeneous. Therefore, the mixture was mixed using Ultrasonic Probe (FS-1200 N, frequency: 20 kHz, power output: 1200 W, 18mm probe) for 90 minutes to achieve a better homogeneous solution. The setup for the ultrasonic probe is shown in Figure 2.

$$\phi = \frac{\omega \rho_{bf}}{\left(1 - \frac{\omega}{100}\right)\rho_{np} + \frac{\omega}{100}\rho_{bf}}$$

(1)



Fig. 2. Ultrasonic probe

2.2 Design Expert 11 Setup

In this study, the experimental design of the operating conditions is performed by the Design Expert 11 software. In this software, a set of DOE is developed to study the relationship of more than one variable that affects a response or several responses. This method is more efficient than OFAT because more information can be collected with fewer experiments. There are three steps involved in DOE: planning, execution, and analysis.

At first, Full Factorial Design is used to develop the DOE. During the planning process, two responses were used: thermal conductivity and viscosity, and two variables were used: the amount of TiO_2 (mixing ratio) and temperature, as shown in Table 1. The mixing ratio is determined by the amount of TiO_2 , which is calculated based on Eq. (1). Two levels were used for each variable. Each independent variable is varied over two levels. Each variable's low and high levels were -1 and +1, respectively.

Furthermore, used five replications with a center point to increase the experiment's sensitivity and the precision of the developed model. Therefore, the software listed 25 experiments, as shown in Table 2. After collecting the response, analysis is done by following these steps

- i. Chose a transformation if desired. Otherwise, leave the option at "None".
- Used the appropriate model. The Fit Summary button displays the sequential F-tests, lack-of-fit tests, and other adequacy measures to assist in selecting the appropriate model.
- iii. Perform the analysis of variance (ANOVA).
- iv. Inspect various diagnostic plots to validate the model statistically.
- v. If the model looks good, generate model graphs.

| Table 2 | 1 | | | | | | | | |
|---|----------------------|--------------------------------------|------------------|--|--|--|--|--|--|
| Independent variable of DOE | | | | | | | | | |
| Level of value (A) Mixing Ratio (TiO ₂ :GNP) (B) Temperature | | | | | | | | | |
| -1 | 1:9 | | 30 | | | | | | |
| +1 | 9:1 | | 60 | | | | | | |
| | | | | | | | | | |
| Table | 2 | | | | | | | | |
| DOE | for Full Fact | orial Design 0.3% conce | entration | | | | | | |
| Run | Mixing Ratio |) | Temperature (°C) | | | | | | |
| | TiO ₂ (g) | Mixing Ratio (TiO ₂ :GnP) | | | | | | | |
| 1 | 0.475276 | 9:1 | 30 | | | | | | |
| 2 | 0.0528084 | 1:9 | 60 | | | | | | |
| 3 | 0.475276 | 9:1 | 60 | | | | | | |
| 4 | 0.264042 | 1:1 | 45 | | | | | | |
| 5 | 0.0528084 | 1:9 | 30 | | | | | | |
| 6 | 0.264042 | 1:1 | 45 | | | | | | |
| 7 | 0.475276 | 9:1 | 60 | | | | | | |
| 8 | 0.475276 | 9:1 | 30 | | | | | | |
| 9 | 0.475276 | 9:1 | 60 | | | | | | |
| 10 | 0.0528084 | 1:9 | 60 | | | | | | |
| 11 | 0.0528084 | 1:9 | 30 | | | | | | |
| 12 | 0.0528084 | 1:9 | 60 | | | | | | |
| 13 | 0.0528084 | 1:9 | 30 | | | | | | |
| 14 | 0.264042 | 1:1 | 45 | | | | | | |
| 15 | 0.475276 | 9:1 | 60 | | | | | | |
| 16 | 0.264042 | 1:1 | 45 | | | | | | |
| 17 | 0.264042 | 1:1 | 45 | | | | | | |
| 18 | 0.475276 | 9:1 | 30 | | | | | | |
| 19 | 0.475276 | 9:1 | 30 | | | | | | |
| 20 | 0.0528084 | 1:9 | 30 | | | | | | |
| 21 | 0.0528084 | 1:9 | 60 | | | | | | |
| 22 | 0.0528084 | 1:9 | 60 | | | | | | |

ANOVA analyses the data to study the relationship between variables and responses. A good model must be significant, and the lack of fit must be insignificant. The Adjusted R² value should not be less than 0.2 with the Predicted R² value to ensure the accuracy of the generated model terms. Furthermore, if there is a curvature presence in the results, the design needs to be upgraded to a Response Surface Design (RSM). If the augmentation is needed, choose Central Composite Design (CCD) with one run per axial (star) point, zero center point as the center point had been added from the previous design, and face-centered alpha where the point selected is within the level set before.

30

30

60

2.3 Thermal Conductivity Measurement

0.475276

0.475276

0.0528084

9:1

1:9

9:1

23

24

25

The thermal conductivity of nanofluid was measured using KD2 Pro, which was a transient hotwire method. This study used a KS1 sensor, and it had an uncertainty of ±10.0% as it was the most suitable sensor for liquid analysis. Before starting the thermal conductivity measurement, the sample was put in an ultrasonic bath (Elmasonic S100H) to ensure that the sample was homogeneous to have an accurate measurement. The temperature involved was 30 to 60°C. The water bath function was to control the temperature of the sample. The sample test tube was put in a water bath to ensure the temperature was in an equilibrium state. Collect a total of five readings for each sample. The thermal conductivity setup is as in Figure 3.



Fig. 3. Thermal conductivity measurement setup

2.4 Dynamic Viscosity Measurement

This experiment used Daihan Scientific Viscometer WVS-2M to measure the viscosity of hybrid nanofluid. The viscometer setup is as Figure 4. Based on the manual given by the manufacturer, the sample with low viscosity should use a large dimensioned rotor (No.0 – No.2) and fast rotating speed. Therefore, in this experiment, the rotor SP is No. 0, the rotating speed 60RPM, 30 seconds reading with 10mPa.s maximum capacity. The spindle LV1 used is suitable for low-viscosity liquid. The volume of the liquid sample must be sufficient to immerse the spindle to ensure the measurement's precision, as shown in Figure 4. The viscometer was compared with distilled water at 30°C for calibration. The percentage error is only 5% with the actual dynamic viscosity.



Fig. 4. Viscometer measurement setup

3. Results and Discussions

3.1 Overall Results and ANOVA

The experiments were done by following the sequence of runs provided by Design Expert 11 to prevent bias in the results obtained. The thermal conductivity and viscosity of the hybrid nanofluid prepared are shown in Table 3. Those results will be used in the Analysis of Variance (ANOVA) to develop models for each concentration.

| Table 3 |
|--|
| DOE for Full Factorial Design 0.3% concentration |

| Run | n Mixing Ratio | | Temperature (°C) | Thermal Conductivity (W/m.K) | Viscosity (mPa.s) |
|-----|----------------------|--------------------------------------|------------------|------------------------------|-------------------|
| | TiO ₂ (g) | Mixing Ratio (TiO ₂ :GNP) | | | |
| 1 | 0.475276 | 9:1 | 30 | 0.818 | 0.9 |
| 2 | 0.0528084 | 1:9 | 60 | 1.147 | 0.83 |
| 3 | 0.475276 | 9:1 | 60 | 1.016 | 0.8 |
| 4 | 0.264042 | 1:1 | 45 | 0.9552 | 0.86 |
| 5 | 0.0528084 | 1:9 | 30 | 0.958 | 0.94 |
| 6 | 0.264042 | 1:1 | 45 | 0.9361 | 0.86 |
| 7 | 0.475276 | 9:1 | 60 | 1.048 | 0.79 |
| 8 | 0.475276 | 9:1 | 30 | 0.748 | 0.89 |
| 9 | 0.475276 | 9:1 | 60 | 1.0526 | 0.8 |
| 10 | 0.0528084 | 1:9 | 60 | 1.032 | 0.82 |
| 11 | 0.0528084 | 1:9 | 30 | 0.983 | 0.93 |
| 12 | 0.0528084 | 1:9 | 60 | 1.043 | 0.85 |
| 13 | 0.0528084 | 1:9 | 30 | 1.212 | 0.95 |
| 14 | 0.264042 | 1:1 | 45 | 0.871 | 0.86 |
| 15 | 0.475276 | 9:1 | 60 | 1.0985 | 0.82 |
| 16 | 0.264042 | 1:1 | 45 | 1.086 | 0.87 |
| 17 | 0.264042 | 1:1 | 45 | 1.2472 | 0.88 |
| 18 | 0.475276 | 9:1 | 30 | 0.964 | 0.89 |
| 19 | 0.475276 | 9:1 | 30 | 0.783 | 0.89 |
| 20 | 0.0528084 | 1:9 | 30 | 0.979 | 0.91 |
| 21 | 0.0528084 | 1:9 | 60 | 0.984 | 0.83 |
| 22 | 0.0528084 | 1:9 | 60 | 1.152 | 0.83 |
| 23 | 0.475276 | 9:1 | 30 | 0.895 | 0.87 |
| 24 | 0.0528084 | 1:9 | 30 | 0.951 | 0.94 |
| 25 | 0.475276 | 9:1 | 60 | 0.999 | 0.81 |

All terms available for the thermal conductivity ANOVA analysis are shown in the half-normal plot in Figure 5. The available terms are $A - TiO_2$, B - Temperature, and AB. The terms are selected from the largest effect to the lowest (right to the left). Therefore, the ANOVA generated is shown in Table 4. P-values less than 0.0500 indicate model terms are significant. In this case, A and B are significant model terms. Values greater than 0.1000 indicate that the model terms are not significant. Therefore, AB is not significant and can be removed to improve the model.

Furthermore, curvature appears insignificant and needs to remove to simplify the analysis. After removing the insignificant term, the final ANOVA for analysis is shown in Table 5. The Model F-value of 6.52 implies that the model is significant. The Lack of Fit F-value of 1.50 implies that the Lack of Fit is not significant relative to the pure error. Non-significant lack of fit is good. The Predicted R² of 0.2191 is in reasonable agreement with the Adjusted R² of 0.3152, where the difference is less than 0.2. Adeq Precision measures the signal-to-noise ratio. A ratio greater than 4 is desirable. This model can be used to navigate the design space. In Eq. (2), the thermal conductivity of hybrid nanofluid is suggested in volume fraction and temperature. The equation can be used to make predictions about the response for given levels of each factor.





Table 4

Thermal conductivity ANOVA for 0.3% Concentration

| Source | Sum of Squares | df | Mean Square | F-value | p-value | Source |
|----------------------|----------------|----|-------------|---------|---------|-------------|
| Model | 0.1607 | 3 | 0.0536 | 5.45 | 0.0066 | significant |
| A-TiO ₂ | 0.0519 | 1 | 0.0519 | 5.28 | 0.0325 | |
| B-Temperature | 0.0821 | 1 | 0.0821 | 8.35 | 0.0091 | |
| AB | 0.0267 | 1 | 0.0267 | 2.72 | 0.1147 | |
| Curvature | 0.0027 | 1 | 0.0027 | 0.2740 | 0.6064 | |
| Pure Error | 0.1965 | 20 | 0.0098 | | | |
| Cor Total | 0.3599 | 24 | | | | |

Table 5

Selected thermal conductivity ANOVA for 0.3% Concentration with fit statistic

| ANOVA | | | | | | |
|--------------------------|----------------|----|-------------|---------|---------|-----------------|
| Source | Sum of Squares | df | Mean Square | F-value | p-value | |
| Model | 0.1340 | 2 | 0.0670 | 6.52 | 0.0060 | significant |
| A-TiO ₂ | 0.0519 | 1 | 0.0519 | 5.05 | 0.0349 | |
| B-Temperature | 0.0821 | 1 | 0.0821 | 7.99 | 0.0098 | |
| Residual | 0.2259 | 22 | 0.0103 | | | |
| Lack of Fit | 0.0294 | 2 | 0.0147 | 1.50 | 0.2479 | not significant |
| Pure Error | 0.1965 | 20 | 0.0098 | | | |
| Cor Total | 0.3599 | 24 | | | | |
| Fit Statistics | | _ | | | | |
| R ² | 0.3722 | - | | | | |
| Adjusted R ² | 0.3152 | | | | | |
| Predicted R ² | 0.2191 | | | | | |
| Adeq Precision | 25.0860 | _ | | | | |

Thermal conductivity = 0.9983 - 0.0509A + 0.0641B

Next, for the dynamic viscosity ANOVA analysis, all terms available are shown at the half-normal plot as shown in Figure 6. The available terms are $A - TiO_2$, B - Temperature, and AB. The terms are

(2)

selected from the largest effect to the lowest (right to the left). Therefore, the ANOVA generated is shown in Table 6. P-values less than 0.0500 indicate model terms are significant. In this case, A and B are significant model terms. Values greater than 0.1000 indicate that the model terms are not significant. Therefore, AB is not significant and can be removed to improve the model. Furthermore, curvature appears insignificant and needs to remove to simplify the analysis. After removing the insignificant term, the final ANOVA for analysis is shown in Table 7. The Model F-value of 99.96 implies that the model is significant. The Lack of Fit F-value of 0.42 implies that the Lack of Fit is not significant relative to the pure error. Non-significant lack of fit is good. The Predicted R² of 0.8683 is in reasonable agreement with the Adjusted R² of 0.8919, where the difference is less than 0.2. Adeq Precision measures the signal-to-noise ratio. A ratio greater than 4 is desirable. This model can be used to navigate the design space. In Eq. (3), the dynamic viscosity of hybrid nanofluid is suggested in terms of volume fraction and temperature. The equation can be used to make predictions about the response for given levels of each factor.



Fig. 6. Half-Normal plot for dynamic viscosity analysis 0.3% concentration

| Tal | ble | 6 |
|-----|-----|---|
|-----|-----|---|

Dynamic viscosity ANOVA for 0.3% Concentration

| Source | Sum of Squares | df | Mean Square | F-value | p-value | Source |
|----------------------|----------------|----|-------------|---------|----------|-------------|
| Model | 0.0505 | 3 | 0.0168 | 123.76 | < 0.0001 | significant |
| A-TiO ₂ | 0.0068 | 1 | 0.0068 | 50.33 | < 0.0001 | |
| B-Temperature | 0.0432 | 1 | 0.0432 | 317.98 | < 0.0001 | |
| AB | 0.0004 | 1 | 0.0004 | 2.98 | 0.0998 | |
| Curvature | 9.000E-06 | 1 | 9.000E-06 | 0.0662 | 0.7996 | |
| Pure Error | 0.0027 | 20 | 0.0001 | | | |
| Cor Total | 0.0532 | 24 | | | | |
| | | | | | | |

| Table 7 | | | | | | | | | |
|--------------------------|--|----|-------------|---------|----------|-----------------|--|--|--|
| Selected dynar | Selected dynamic viscosity ANOVA for 0.3% Concentration with fit statistic | | | | | | | | |
| ANOVA | | | | | | | | | |
| Source | Sum of Squares | df | Mean Square | F-value | p-value | | | | |
| Model | 0.0501 | 2 | 0.0250 | 175.81 | < 0.0001 | significant | | | |
| A-TiO ₂ | 0.0068 | 1 | 0.0068 | 48.05 | < 0.0001 | | | | |
| B-Temperature | 0.0432 | 1 | 0.0432 | 303.57 | < 0.0001 | | | | |
| Residual | 0.0031 | 22 | 0.0001 | | | | | | |
| Lack of Fit | 0.0004 | 2 | 0.0002 | 1.52 | 0.2425 | not significant | | | |
| Pure Error | 0.0027 | 20 | 0.0001 | | | | | | |
| Cor Total | 0.0532 | 24 | | | | | | | |
| Fit Statistics | | | | | | | | | |
| R ² | 0.9411 | _ | | | | | | | |
| Adjusted R ² | 0.9358 | | | | | | | | |
| Predicted R ² | 0.9220 | | | | | | | | |
| Adeq Precision | 31.4423 | | | | | | | | |

$Dynamic \ viscosity = 0.8648 - 0.0185A - 0.0465B$

3.2 Optimisation

The objective of the optimisation is to determine which mixing ratio of hybrid nanofluid from each concentration has the best performance based on thermal conductivity and dynamic viscosity. Therefore, the optimisation condition is set as shown in Table 8. The level of importance of a goal can be changed based on the optimisation objectives. The default is for all goals to be equally important at three pluses (+++), and the most important is five pluses (++++). To achieve the best parameter for the mixing ratio and temperature of hybrid nanofluid, the target for optimisation is high thermal conductivity with a high level of importance and low dynamic viscosity with the default setting of the level of importance.

| Table 8 | | |
|------------------------------|---------------------|---------------------|
| Condition for optimization | | |
| Parameter | Target | Level of Importance |
| A: TiO ₂ (g) | In range | 3 |
| B: Temperature (°C) | In range up to 40°C | 3 |
| Thermal conductivity (W/m K) | Maximize | 5 |
| Dynamic Viscosity (mPa.s) | Minimize | 3 |

The optimal value suggested by the software for each concentration is shown in Table 9. Solution number 5 was the best value for each concentration. These values were picked from the previous model generated and goals set. From this table, the best parameter is 0.3vol% with 0.1053g of TiO₂ equivalent to 1:4(TiO₂:GNP) mixing ratio because it has the highest thermal conductivity compared to others. Dynamic viscosity is considered less important than thermal conductivity for this selection despite higher viscosity than the other solutions.

(3)

Table 9

| The optimal values for 0.3vol% suggested by the software | | | | | | | | | |
|--|----------------------|------------------|------------------------------|---------------------------|--|--|--|--|--|
| Solution | TiO ₂ (g) | Temperature (°C) | Thermal conductivity (W/m K) | Dynamic viscosity (mPa.s) | | | | | |
| 1 | 0.1228 | 40 | 1.0111 | 0.8927 | | | | | |
| 2 | 0.1213 | 40 | 1.0114 | 0.8928 | | | | | |
| 3 | 0.1244 | 40 | 1.0107 | 0.8925 | | | | | |
| 4 | 0.1303 | 40 | 1.0093 | 0.8920 | | | | | |
| 5 | 0.1053 | 40 | 1.0153 | 0.8942 | | | | | |
| 6 | 0.1420 | 40 | 1.0064 | 0.8910 | | | | | |
| 7 | 0.1525 | 40 | 1.0039 | 0.8901 | | | | | |
| 8 | 0.2004 | 40 | 0.9923 | 0.8859 | | | | | |
| 9 | 0.2391 | 40 | 0.9830 | 0.8825 | | | | | |

To validate the optimum value generated from the software, other thermal conductivity and dynamic viscosity experiments were done with 0.3vol% concentration, 1:4(TiO₂-GNP) mixing ratio, and 40°C. The results of the experiments are then compared with results generated from Eq. (2) and Eq. (3). Based on Figure 7 and Figure 8, The difference between the measured and predicted values of thermal conductivity and dynamic viscosity was less than 5%. Therefore, the model develops using this technique is acceptable. Graphene-based nanoparticles have a higher thermal conductivity compared with other nanofluids. Therefore, the presence of more GNP has a better thermal conductivity of hybrid nanofluid compared with a lower mixing ratio of GNP. A study by Vărdaru *et al.*, [21] verified that the presence of more graphene-based nanoparticles in the hybrid nanofluid has better thermal conductivity compared with other hybrid nanofluids with a lower mixing ratio of graphene-based nanoparticles.



Fig. 7. Thermal conductivity predicted vs actual



Fig. 8. Dynamic viscosity predicted vs actual

4. Conclusions

The experiment objective was to optimise the mixing ratio of hybrid nanofluid with thermal conductivity and viscosity using Design Expert 11. The optimised mixing ratio and concentration of the prepared hybrid nanofluid are 0.3vol% with a 1:4(TiO₂-GNP) mixing ratio. DOE method shows fewer experiments need to be done while having enough information for the optimisation process. The chosen mixing ratio was based on the model developed by the ANOVA. The difference between the measured and predicted values of thermal conductivity and dynamic viscosity was less than 5%. Therefore, the model develops using this technique is acceptable.

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References

- [1] Babu, JA Ranga, K. Kiran Kumar, and S. Srinivasa Rao. "State-of-art review on hybrid nanofluids." *Renewable and Sustainable Energy Reviews* 77 (2017): 551-565. <u>https://doi.org/10.1016/j.rser.2017.04.040</u>
- [2] Sarkar, Jahar, Pradyumna Ghosh, and Arjumand Adil. "A review on hybrid nanofluids: recent research, development and applications." *Renewable and Sustainable Energy Reviews* 43 (2015): 164-177. <u>https://doi.org/10.1016/j.rser.2014.11.023</u>
- [3] Rubaa'i, Afifah Filza Ahmad, Lim Yeou Jiann, Sharidan Shafie, and Anati Ali. "Hybrid Nanofluid on Mixed Convection Flow Past a Stretching Sheet with Irregular Heat Source/Sink." *CFD Letters* 14, no. 12 (2022): 75-83. <u>https://doi.org/10.37934/cfdl.14.12.7583</u>
- [4] Kho, Yap Bing, Rahimah Jusoh, Mohd Zuki Salleh, Mohd Hisyam Ariff, and Nooraini Zainuddin. "Magnetohydrodynamics Ag-Fe3O4-Ethylene Glycol Hybrid Nanofluid Flow and Heat Transfer with Thermal Radiation." CFD Letters 14, no. 11 (2022): 88-101. <u>https://doi.org/10.37934/cfdl.14.11.88101</u>
- [5] Soid, Siti Khuzaimah, Afiqah Athirah Durahman, Nur Hazirah Adilla Norzawary, Mohd Rijal Ilias, and Amirah Mohamad Sahar. "Magnetohydrodynamic of Copper-Aluminium of Oxide Hybrid Nanoparticles Containing Gyrotactic Microorganisms over a Vertical Cylinder with Suction." *Journal of Advanced Research in Applied Sciences* and Engineering Technology 28, no. 2 (2022): 222-234. <u>https://doi.org/10.37934/araset.28.2.222234</u>
- [6] Sidik, Nor Azwadi Che, H. A. Mohammed, Omer A. Alawi, and S. Samion. "A review on preparation methods and challenges of nanofluids." *International Communications in Heat and Mass Transfer* 54 (2014): 115-125. <u>https://doi.org/10.1016/j.icheatmasstransfer.2014.03.002</u>
- [7] Esfe, Mohammad Hemmat, Seyfolah Saedodin, Omid Mahian, and Somchai Wongwises. "Thermophysical properties, heat transfer and pressure drop of COOH-functionalized multi walled carbon nanotubes/water nanofluids." *International Communications in Heat and Mass Transfer* 58 (2014): 176-183. <u>https://doi.org/10.1016/j.icheatmasstransfer.2014.08.037</u>

- [8] Timofeeva, Elena V., Jules L. Routbort, and Dileep Singh. "Particle shape effects on thermophysical properties of alumina nanofluids." *Journal of applied physics* 106, no. 1 (2009): 014304. <u>https://doi.org/10.1063/1.3155999</u>
- [9] Pourpasha, Hadi, Saeed Zeinali Heris, Omid Mahian, and Somchai Wongwises. "The effect of multi-wall carbon nanotubes/turbine meter oil nanofluid concentration on the thermophysical properties of lubricants." *Powder technology* 367 (2020): 133-142. <u>https://doi.org/10.1016/j.powtec.2020.03.037</u>
- [10] Das, Pritam Kumar, Nurul Islam, Apurba Kumar Santra, and Ranjan Ganguly. "Experimental investigation of thermophysical properties of Al2O3–water nanofluid: Role of surfactants." *Journal of Molecular Liquids* 237 (2017): 304-312. <u>https://doi.org/10.1016/j.molliq.2017.04.099</u>
- [11] Harun, Muhammad Arif, Nor Azwadi Che Sidik, Yutaka Asako, and Tan Lit Ken. "Recent Review On Preparation Method, Mixing Ratio, and Heat Transfer Application Using Hybrid Nanofluid." *Journal of Advanced Research in Fluid Mechanics and Thermal Sciences* 95, no. 1 (2022): 44-53. <u>https://doi.org/10.37934/arfmts.95.1.4453</u>
- [12] Harun, M. A., N. A. C. Sidik, and M. A. M. Rohaizan. "Experimental investigation of stability and thermal properties of nanocellulose-water nanofluid." In *IOP Conference Series: Materials Science and Engineering*, vol. 1092, no. 1, p. 012044. IOP Publishing, 2021. <u>https://doi.org/10.1088/1757-899X/1092/1/012044</u>
- [13] Harun, Muhammad Arif, Nor Azwadi Che Sidik, and Mohamed Adham Mohamad Rohaizan. "A Review on Stability and Heat Transfer Performance of Nanofluid Using Surfactants." *Journal of Advanced Research in Materials Science* 75, no. 1 (2020): 1-9. <u>https://doi.org/10.37934/arms.75.1.19</u>
- [14] Ma, Mingyan, Yuling Zhai, Peitao Yao, Yanhua Li, and Hua Wang. "Synergistic mechanism of thermal conductivity enhancement and economic analysis of hybrid nanofluids." *Powder Technology* 373 (2020): 702-715. <u>https://doi.org/10.1016/j.powtec.2020.07.020</u>
- [15] Xian, Hong Wei, Nor Azwadi Che Sidik, Siti Rahmah Aid, Tan Lit Ken, and Yutaka Asako. "Review on preparation techniques, properties and performance of hybrid nanofluid in recent engineering applications." *Journal of Advanced Research in Fluid Mechanics and Thermal Sciences* 45, no. 1 (2018): 1-13.
- [16] Alawi, O. A., H. A. Mohammed, and NA Che Sidik. "Mixed convective nanofluids flow in a channel having forward-facing step with baffle." *Journal of Advanced Research in Applied Mechanics* 24, no. 1 (2016): 1-21.
- [17] Kho, Yap Bing, Rahimah Jusoh, Mohd Zuki Salleh, Muhammad Khairul Anuar Mohamed, Zulkhibri Ismail, and Rohana Abdul Hamid. "Inclusion of Viscous Dissipation on the Boundary Layer Flow of Cu-TiO2 Hybrid Nanofluid over Stretching/Shrinking Sheet." *Journal of Advanced Research in Fluid Mechanics and Thermal Sciences* 88, no. 2 (2021): 64-79. <u>https://doi.org/10.37934/arfmts.88.2.6479</u>
- [18] Czitrom, Veronica. "One-factor-at-a-time versus designed experiments." *The American Statistician* 53, no. 2 (1999): 126-131. <u>https://doi.org/10.1080/00031305.1999.10474445</u>
- [19] Singh, Santosh K., Sanjay K. Singh, Vinayak R. Tripathi, Sunil K. Khare, and Satyendra K. Garg. "Comparative one-factor-at-a-time, response surface (statistical) and bench-scale bioreactor level optimization of thermoalkaline protease production from a psychrotrophic Pseudomonas putida SKG-1 isolate." *Microbial cell factories* 10, no. 1 (2011): 1-13. <u>https://doi.org/10.1186/1475-2859-10-114</u>
- [20] Mutalik, Snehal R., Bhalchandra K. Vaidya, Renuka M. Joshi, Kiran M. Desai, and Sanjay N. Nene. "Use of response surface optimization for the production of biosurfactant from Rhodococcus spp. MTCC 2574." *Bioresource Technology* 99, no. 16 (2008): 7875-7880. <u>https://doi.org/10.1016/j.biortech.2008.02.027</u>
- [21] Vărdaru, Alexandru, Gabriela Huminic, Angel Huminic, Claudiu Fleacă, Florian Dumitrache, and Ion Morjan. "Synthesis, characterization and thermal conductivity of water based graphene oxide–silicon hybrid nanofluids: An experimental approach." Alexandria Engineering Journal 61, no. 12 (2022): 12111-12122. <u>https://doi.org/10.1016/j.aej.2022.06.012</u>