

The Removal of Biomass Tar Derived Producer Gas by Means of Thermal and Catalytic Cracking Methods

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ARTICLE INFO	ABSTRACT
Article history: Received 2 June 2021 Received in revised form 20 September 2021 Accepted 25 September 2021 Available online 31 October 2021 Keywords: Thermal and catalytic cracking; modified catalyst; biomass gasification; biomass tar	Tar derived from biomass gasification system needs to be eliminated before applying biomass producer gas for avoiding equipment and its gas problems. In this study, thermal and catalytic cracking methods of biomass tar along with microwave assistance in heat transfer were experimented at various temperatures during 650-1,200 °C and residence at 0.24-0.5 s. The results present that high tar removal efficiency by approximately 90 % under thermal cracking treatment and about 98 % with catalytic cracking method. It also shows that the catalytic cracking especially modified catalyst could be lowered carbon deposition on catalyst surface.

1. Introduction

The lack of fossil fuel energy and the environmental impacts due to the abundant usability of fossil fuel energy, those issues have caused the renewable energy source is considered for substitution of its energy [1]. Among of renewable energy, biomass energy source is the most interesting because of its advantages and low pollutant emission. Gasification, the one commonly used of thermochemical technology, transforms biomass source into useful energy such as biomass producer gas. That gas is mainly composed of H₂, CO, CO₂, CH₄ and also some dirty products such as tar and particles [2-4]. Tar is a main point in biomass gasification system because it can be a lot of problems to all equipment and producer gas too [5,6]. The tar along with producer gas is imperative to decompose for avoiding from tar problems before using in any applications [7]. The removal of tar can be divided into three approaches: 1) mechanical or physical method, 2) thermal treatment method and 3) catalytic cracking method [3,7,8]. Nevertheless, thermocatalytic treatment method, thermal and/or catalytic cracking, is desirable because its treatment can remove the tar and convert

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into advantageous gases such as H_2 , CO or HCN gases which can improve energy content of syngas [9].

It has been reported that the heavy tar can be cracked by using thermal cracking at temperature of 900 °C [10]. Meanwhile, the high temperature upper than 1,100 °C is sufficiently required to complete the tar removal [11]. It is also mentioned that thermal cracking method has been shown high tar removal efficiency with operating at temperature of 1,200 °C and residence time shorter than 10 s. Zhang et al., [12] have mentioned that one of biomass tar composition (toluene) was hardly to remove, and should be up the temperature to 1,200 °C for elimination. In term of catalytic cracking method, this method is extremely favorable because tar can be removed and reformed into gaseous compositions with increasing quantity of H₂ and CO on producer gas [8,13]. Several types of catalysts have been tested on tar removal such as nickel based, non-nickel metal, alkali metal, basic, acid, and activated carbon [3,13]. Among of these catalysts, nickel-supported catalysts are the most used catalyst for tar decomposition. They present not only high activity on tar removal but also increasing H₂ and CO contents of the producer gas and low-price costs [14]. It has suggested that Ni-based catalysts supported by alumina (Al₂O₃) as metal oxides, or dolomite, olivine as natural materials are considered to have a positive effect in transforming tar into useable gas [15]. Nickel alumina, Ni/Al₂O₃ catalyst, presents high catalytic activity and tar removal efficiency but it is not stable and eventual deactivation [14,16]. Several parameters such as acidity, pore, structure, and surface area of the support are determined of catalytic activity [17]. Anis and Zainal [3] have reported that nickel-based catalysts can be completely eliminated the tar at temperature of 900 °C, depending on promoter and support used types. In spite of the high activity of nickel-based catalysts, the main disadvantages with these catalysts have been occurred as rapid deactivation because of carbon deposition on catalyst surface (coke formation) and catalyst reduction. Furthermore, the other issue of thermal and catalytic cracking treatment of tar method is the high energy demand to complete tar removal at temperature range of 700-1,200 °C. It has been reported that treatment usually uses an external high electrical source where heat transfer arises from the surface into the core of material. Some effects such as heat transfer resistance, heat losses to surrounding and the corrosion of wall reactor are the lack of this treatment because of the continued high electrical heating [18].

This paper, the activity of thermocatalytic treatment of biomass tar was investigated. In addition, in order that the effectiveness of tar removal during it treatment, the modified catalyst and the microwave assisted were tested by using biomass tar derived from producer gas with various temperature conditions.

2. Methods

2.1 Catalyst Preparation

The Al₂O₃ catalyst as commercial grade, was prepared through wetness impregnation method as followed with Liu *et al.*, [19]. Starting with the catalyst was dried in an oven at temperature of 120 °C overnight for removal catalyst moister along with immersion of dry catalyst into magnesium nitrate solution at room temperature for 24 h. The catalyst was calcined in a furnace at temperature of 500 °C about 3 h and then cooling the catalyst at ambient temperature. Finally, the Mg/Al₂O₃ catalyst was immersed again into nickel nitrate solution and following same previous process.

2.2 Materials

The commercial wood pellets were used as biomass fuels for producer gas production in a downdraft gasifier. The properties of wood pellet are listed in Table 1.

Table 1				
Properties of wood pellets				
Proximate analysis (wt % dry basis)				
Fixed carbon	14.8			
Volatile matter	76.2			
Ash	0.5			
Moisture	9			
Elemental analysis (wt % dry ash-free basis)				
Carbon	44.55			
Hydrogen	7.54			
Nitrogen	0.06			
Sulfur	0.17			
Oxygen	47.67			
HHV (MJ/kg)	17.8			

2.3 Experimental Apparatus and Parameters

The schematic diagram of the overall experimental apparatus system is shown in Figure 1. The system was consisted of three subsystems: a) biomass gasifier, b) tar cracking unit, and c) tar sample collection.





The biomass gasifier system was composted of a throatless downdraft fixed bed, cyclone, drum cooler, blower, and gas flare. The gasifier has a thermal power output of 8.3 kW_T which depends on biomass feeding rate of 5 kg/h.

Tar cracking system was consisted a modified microwave and alumina reactor. A microwave oven was drilled the hole for installing alumina tube reactor with a height of 16 cm, 2.54 cm of internal diameter and 0.5 cm of thickness inside microwave chamber. It provides 700 and 1,125 W of maximum microwave power output and power consumption, respectively. Silicon carbide (SiC), susceptor material, was used for absorption and conversion the energy of microwave into heat. In addition, a temperature controller was attached into the system to control and maintain the temperature within reactor.

The tar sample collection system included a tar sampling train, vacuum pump, and flow meter. A tar sampling train has been modified to capture tar and particles in producer gas with six impinger

bottles [20]. Each bottle was filled with 50 ml of isopropanol other than the last bottle was empty. The first two bottles were placed at ambient temperature and next four bottles were submerged into an ice box. That ice box was filled with the mixture of ice and salt together for keeping temperature about -22 °C which suffices to condense the tar [21]. The dry producer gas was suctioned and flowed through the tar removal and this system by using a vacuum pump. A flow meter was installed in this system for measuring and controlling the flow rate of biomass producer gas.

Table 2 presents the experimental parameters for thermocatalytic cracking of biomass tar. The temperatures were tested in the range of 700 - 1,200 °C. The residence time was set at 0.24-0.5 s depending on gas flow rate of 3.8-5 LPM.

Table 2						
The	experimental	pai	rameters	for		
thermocatalytic cracking of biomass tar						
Conditio	n		Parameter	Unit		
Catalyst mass			3	g		
Biomass producer gas flow rate		te	3.8 – 5	LPM		
Catalyst bed height			3	cm		
Residence time			0.24-0.5	S		
Temperature			700-1,200	°C		
Microwave power			0.7	kW		

2.4 Thermocatalytic

This study was focused on biomass tar removal through thermal and catalytic cracking methods. The biomass producer gas was run through the pipeline system from downdraft gasifier until the tar sample collection system. In term of thermal cracking method, the range of testing temperature was operated during 900-1,200 °C with residence time of 0.5 s. For catalytic cracking method, the catalysts and absorber material, SiC, SiC+ catalysts and SiC, were arranged into three layers with total of bed high 120 cm inside the reactor. Each experimental was set 3 g of Ni/Mg/Al₂O₃ and mixed together with SiC about 25 g. The temperature was tested in the range of 700-900 °C with residence time of 0.24 s.

2.5 Sampling and Analysis

The biomass producer gas, before and after exit the microwave reactor, was flowed through sample collection system. The biomass tar samples were captured in the isopropanol solution in tar collection system and then were filtered through a Whatman filter paper to separate particles. The filtered solution of isopropanol with the condensed tar was sent into BUCHI rotary evaporator to evaporate and determine the gravimetric of tar. The gas after cracking was sent into the gas sampling bag and then investigated with GC-TCD to analyze the quantification gas composition. Thethermogravimetric analyser or TGA was used to determine the carbon deposited on catalyst.

3. Result and Discussion

3.1 The Biomass Gasification

As the process of thermochemical derived biomass gasification, the producer gas which was produced by a throatless downdraft gasifier of wood pellet in this study contains not only useful gas

such as hydrogen, nitrogen, oxygen, methane and carbon dioxide but also tar, water and particulates [22]. Table 3 shows the products of producer gas as well as some related data.

Table 3						
The products of producer gas from a throatless downdraft gasifier						
Parameter	Value					
	Thermal cracking method	Catalytic cracking method				
Gasifier condition						
Equivalence ratio (ER)	0.26	0.26				
Low heating value (LHV)	4.44 MJ/Nm ³	4.32 MJ/Nm ³				
Products yields at sample point	wt.%	wt.%				
Gas	94.55	92.96				
Tar	0.23	0.34				
Water	5.14	6.65				
Particulates	0.07	0.05				
The composition of producer gas	vol.%	vol.%				
Hydrogen	10.7	10.23				
Oxygen	3.27	3.14				
Carbon monoxide	19.86	19.5				
Methane	2.18	2.12				
Carbon dioxide	10.45	10.25				
Nitrogen	53.56	54.76				

3.2 Thermal Cracking of Biomass Tar

Thermal cracking of biomass tar from wood pellet gasification was tested on temperature during 900-1200 °C. The composition of producer gas and low heating value (LHV) presents in Figure 2. At 900 °C, H_2 and O_2 appear slightly decrease from initial of raw producer gas. The result of CO shows increase as the temperature of testing goes up that because of the forming from partial oxidation of solid particles as reported by Anis and Zainal [9].



Fig. 2. Gas formation and LHV by thermal cracking of biomass tar

The results in Figure 2 also present difference effects of gas composition when the gas formations come to be intenseness of flammable gases at high temperature. The partial oxidation, water gas reaction, and Boudouard reaction are created the flammable gases by supporting of O_2 , water, and particle. By the time of increasing the temperature of reaction, CO and H₂ products show increase formation but CH₄ and CO₂ appear decreasingly. The yield of products both tar and particle perform inverse variation with testing temperature as shown in Figure 3. At the maximum reaction temperature, the tar and particle are decomposed more than 90% and 97% with final concentration of them about 0.182 g/Nm³ and 0.015 g/Nm³, respectively. These results confirm to mention of Zhang *et al.*, [12] as the removal accomplishment of tar and particle derived from producer gas by thermal treatment occurs at high temperature above 1,200 °C.



3.3 Catalytic Cracking of Biomass Tar

Catalytic cracking of biomass tar from wood pellet gasification was run under temperatures during 700-900 °C. The gas composition of producer gas and LHV are presented in Figure 4. The yield of products along with product conversion efficiency by Ni/Mg/Al₂O₃ cracking of biomass tar display in Figure 5.

At 700 °C, H₂ and CO seem slightly decrease whilst CH₄ and CO₂ show opposite curve from initial value of raw producer gas. In this temperature reaction, the concentration of tar is reduced from initial of tar (raw producer gas) at 2.63 g/Nm³ to 0.58 g/Nm³. The tar and particle are converted about 82% and 88%, respectively. The graph in Figure 4 also displays the gas content of CO₂ and CH₄ which are imperceptible difference at reaction temperature of 800 °C. While, CO shows to increase the gas content from initial of raw producer gas until 900 °C. That result is because the Boudourd reaction as following in Eq. (1) with occurrence at high temperature [23]. At higher temperature of 800 °C, CH₄ exits increase formation that because the reforming products such as H₂, O₂, and CO₂ prevent reaction of methane steam reforming on catalyst as Eq. (2) [23].





$$C + CO_2 \leftrightarrow 2CO$$

 $CH_4 + H_2O \rightarrow CO + 3H_2$

(1) (2)

As shown in Figure 5, at temperature of 900 °C, the highest tar is cracked by Ni/Mg/Al₂O₃ about 98% that tar concentration remains 0.044 g/Nm^3 whereas the lowest of particle is about 0.009 g/Nm^3 . The yield of coke deposition on catalyst surface as presented in Figure 6, it appears to be related to tar removal efficiency. It is the reduction of coke deposition with resulting in high tar removal as reported by some studies [24,25].



4. Conclusions

The performance of thermal and catalytic cracking methods of biomass tar has been studied at several temperature tests during 700-1,200 °C and residence time of 0.24-0.5 s. Wood pellets were used as biomass fuels for producer gas production of this study with HHV of 17.8 MJ/Kg. In this paper, thermal cracking method shows high removal efficiency of tar at 1200 °C about 90 % with tar concentration of 0.182 g/Nm³. The achievement of tar removal by using Ni/Mg/Al₂O₃ is about 98% corresponds to the concentration remained 0.044 g/Nm³ from initial tar concentration of 2.63 g/Nm³. In addition, the effect of upgraded catalyst can be caused to removal high efficiency of biomass tar whereas that catalyst has occurred low carbon deposition on its surface.

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