

# Impact of Non-Newtonian Fluids' Rheological Behavior on Double-Diffusive Natural Convection in an Inclined Square Porous Layer

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#### **ARTICLE INFO**

#### ABSTRACT

Article history: Received 10 April 2022 Received in revised form 4 August 2022 Accepted 15 August 2022 Available online 10 September 2022

Keywords:

Double-diffusive natural convection; Carreau-Yasuda model; buoyancy ratio; heat and mass transfer; non-Newtonian fluids This paper presents a numerical study of double-diffusive convection in a square cavity with a porous layer filled with a non-Newtonian fluid and subjected to uniform Neumann heat and air flows applied to the active walls of the cavity, while the other walls are considered adiabatic and impermeable. We used the Carreau-Yasuda rheological model, which is adequate for many non-Newtonian fluids, and is used to characterize the behavior of the shear-tinning fluids. The finite difference method is used to obtain the numerical solution of the general governing equations, for a thin shear-thinning fluid with Darcy model and Boussinesq approximation were employed to model the convective flow in the porous medium. The governing parameters of the problem are the rheological parameters of Carreau-Yasuda, namely (n, E, s and a), the thermal Rayleigh number,  $R_T$ , the Lewis number Le, the buoyancy ratio N, and inclination angel,  $\Phi$ . the effects of the mentioned governing parameters, flow intensity, apparent viscosity, and heat and mass transfer rates, were illustrated and discussed in terms of steamlines, isotherm, isoconcentration, apparent viscosity contours, stream function, apparent viscosity profiles, the average Nusselt number and the average Sherwood number. The results indicate a strong influence of the shear behavior of the non-Newtonian fluid on the heat and mass transfer by natural convection inside the enclosure. the flow structure evolves from conduction to convection as the buoyancy ratio increases. The Nusselt, Nu, and Sherwood, Sh, numbers increase along the transition path. The average number of Sh increases considerably with the improvement of the number of Lewis number but the average number of Nu changes slightly. The thermal and mass transfer is favored for an angle of inclination of 45°.

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https://doi.org/10.37934/arfmts.99.1.1747

## 1. Introduction

The study of thermosolutal convection in porous media is currently the subject of numerous works at the international level. It consists in studying the convective movements induced in a porous medium by a temperature gradient and a concentration gradient (caused by variation with temperature and/or solute concentration in the presence of a gravitational field). The movements generated by the variations of the density of the saturating fluid as a function of temperature and concentration can be very different from the classical case of natural convection of thermal origin [1]. The study of convection within enclosures filled with non-Newtonian fluids would help to improve the design and performance of a variety of engineering and environmental application processes such as thermal and chemical engineering, slurry transporting, food processing, migration of moisture in insulating fibers, crystal growth, petroleum drilling, hydrology, polymer engineering, geophysics, mixtures separation, gas storage, and in many other industrial processes, etc.

A rather complete review of these works has been made by number of publications [2-5]. Due to the conflicting volumetric forces of thermal and solutal forces, convection by double-diffusion is fundamentally defined by the phenomena of heat and mass transfer, which are the source of entropy creation, Wang *et al.*, [6]. In a porous medium, Chen and Chen [7] numerically studied the natural convection in a porous horizontal circular cylinder and a sphere filled with a non-Newtonian fluid, using a power-law model. They showed that the heat and mass characteristics for the natural convection of a non-Newtonian fluid with low power-law index values in the porous medium are worth studying. Yang and Wang [8] investigated the natural convection heat transfer of non-Newtonian fluids of power-law type with flow constraints. Mahrous *et al.*, [9] reviewed the different assumption used to calculate blood viscosity in CFD models of intracranial aneurysm.

Non-Newtonian fluids in porous media behave substantially differently from Newtonian fluids in porous media in terms of convective heat and mass transfer. Because non-Newtonian fluids are nonlinear, their effects on porous media are distinct from those of Newtonian fluids. Pascal has thought about the flow of non-Newtonian fluids with a power-law through a porous medium, Pascal [10,11]. A modified version of Darcy's law that uses an extended Bingham rheological model to describe the flow through a simple capillary tube for non-Newtonian fluids. The first investigation of doublediffusive convection in a porous layer based on Darcy's law, which is applicable to dense, lowpermeability porous media, was done by Taunton et al., [12]. The commencement of motion was predicted using the linear permeability theory on a layered horizontal porous layer with a stable, inactive concentration that was heated and salted from the ground. A vertical plate in a saturated porous medium subjected to constant and uniform active wall temperature and concentration was examined by Jumah and Mujumdar [13] for heat and mass transfer by natural convection on non-Newtonian power-law fluids with flow constraint. Non-Newtonian liquids are characterized by shearthickening and shear-thinning materials, which have different influences on heat transport operations. Thus, shedding light on the heat transport attributes of non-Newtonian liquids at different working stresses helps to increase their heat transport efficiency. Here, we used the tile model for the analysis of flow behavior in which viscosity depends on shear rate. Al-Azawy et al., [14] numerically studied the three-dimensional, steady, laminar and non-Newtonian Carreau model blood flow through a stenosis artery. The shape of stenosis that has been selected is a trapezoidal with two cases (70% and 90% blockage). Shear-rate, streamlines, vorticity and importance factor were examined to assess the influence of non-Newtonian model. They showed that the levels of non-Newtonian model were predicted to be higher in the 90% blockage then that observed within the 70%. An examination of streamlines through the artery advised that the recirculation areas in the artery and after the stenosis stretched further in the Carreau model. Unuh et al., [15] carried out a numerical study of magnetic flux and shear-stress of OEM damper featuring MR fluid. The finite element model was built to analyse and examine the new design of OEM damper. Their main finding was that the induced magnetic field can manifest the shear stress development by polarizing the suspended partial in the MR fluid. In addition, the gradient of shear stress response decreased at highest shear stress and eventually become plateaus as the MR fluids saturated completely.

Wang et al., [16] investigated the natural convection of a non-Newtonian power-law fluid in a square porous cavity. The authors have solved the problem analytically and numerically using the fourth-order Runge-Kutta scheme and the shooting method. From the reported numerical results, it was found that the onset of natural convection would occur if a minimum value for the yield stress is provided. Jecl and Skerget [17] applied the boundary finite element method to study the natural convection in non-Newtonian fluid in a square porous cavity. Power-law and Carreau model are used to model non-Newtonian rheological behavior. The results of the hydrodynamic and heat transfer evaluations were reported for the configuration in which the enclosure is heated by a side wall while the horizontal walls are insulated. The flow in the porous medium a was modeled using the modified Brinkman extended Darcy model, taking into account non-Darcy viscous effects. Lamsaadi et al., [18] studied the effect of power index on natural convection in the rectangular cavity with constant heat flow on the side walls and adiabatic vertical walls for the high Prandtl number limit. Compared to Newtonian fluids (n=1), a decrease in the power-law index n (shear-thinning fluids, 0 < n < 1Þ) induces an early onset of the single-cell flow regime and increases the convective heat transfer rate, whereas an increase in n (shear-thickening fluids, n > 1) produces an opposite effect. Contrary. The main results of the approximate solution of the parallel flow have been validated numerically. Natural convection in a rectangular porous medium is studied analytically and numerically by Bahloul [19]. He showed that the thermal stratification coefficient, depends essentially on the aspect ratio of the enclosure and that it becomes almost independent of the Rayleigh number in the boundary layer regime. For high heating, he gave a simplified model for the stratification parameter  $\gamma =$  $1.22A^{-0.47} Ra^{0.46}$ . The linear stability study of the parallel flow has been used to determine the critical Rayleigh number for a cavity of large extension. The author found that the flow is stable regardless of the stratification coefficient. The natural convection flow, heat and mass transfer of non-Newtonian power law fluids with flow constraint in a porous medium from a vertical plate with varying heat and wall mass fluxes were considered by Cheng [20], he observed that the existence of a threshold pressure gradient in power law fluids tends to decrease the fluid velocity and the local Nusselt and Sherwood numbers. Similarly, an increase in the power law exponent increases the local Nusselt and Sherwood numbers.

The natural convection of non-Newtonian power-law fluids in a porous cavity was numerically studied and described by Hadim [21] using the modified Brinkman-Forchheimer model. He concluded that as the power-law index decreases, the circulation inside the enclosure increases, leading to a higher Nusselt number. These effects are enhanced as the Darcy number increases. This results in a higher vertical velocity near the walls and a higher Nusselt number in the cavity. Therefore, an increase in the Rayleigh number produced similar effects to a decrease in the power-law index. Cheng's [20] research on the Nusselt and Sherwood numbers shows that they rise as the power-law increases. A mathematical analysis of thermosolutal convection in a porous media was published by Lin and Payne [22]. This study employed the Darcy model. The flow solution is continuously dependent on the Soret effect, according to the authors. Current findings on asymptotic and numerical double-diffusion convection in the presence of a magnetic field was conducted by Rebhi *et al.*, [23,24]. Neumann and Dirichlet boundary conditions for temperature and solute concentrations were used to generalize the study. various convection mechanisms, and solute concentrations, were noted.

The topic of coupled, stable, laminar heat and mass transmission through a permeable wedge immersed in a porous medium with variable surface temperature and concentration, as well as heat generation or absorption and wall transpiration effects, was examined by Chamkha [25]. In the presence of Soret and Dufour parameters, Kefayati [26,27] examined the naturally occurring doublediffusive convection of non-Newtonian power-law fluids and entropy generation in an inclined porous cavity. The impact of Carreau-Yasuda rheological parameters on natural convection in a horizontal porous cavity saturated with a non-Newtonian fluid was examined analytically and numerically by Khechiba et al., [28]. The parallel flow assumption was used to generate the analytical solution. Zhu et al., [29] investigated a numerical study of 3D double-diffusive natural convection in a fluid-saturated porous cubic enclosure by a generalized non-Darcy model. Wahid et al., [30] carried out an analytical study the magnetohydrodynamic slip Darcy flow of viscoelastic fluid over stretching sheet and heat transfer with thermal radiation and viscous dissipation. Their main conclusions that the elastico-viscous fluid ( $k_1^* < 0$ ) enhances the skin friction coefficient and reduce the heat transfer coefficient compared to second grade fluid. Parvin *et al.,* [31] investigated the magnetohydrodynamics Casson fluid flow, heat mass transfer due to the presence of assisting flow and Buoyancy ratio parameters. They showed that the increment and decrement of the velocity, temperature, concentration, skin friction coefficient, local Nusselt number and local Sherwood number are influenced by magnetic field, assisting flow and buoyancy ratio parameters.

Recently, using the Dupuit-Darcy model, Rebhi et al., [32,33] conducted analytical and numerical studies of convective fluxes created in vertical and horizontal porous cavities filled with a binary mixture. studying the linear stability of the parallel flow approximation, the authors explicitly and implicitly predicted the onset of convective motion and the trigger point of the Hopf bifurcation characterizing the transition between stable convective and oscillatory states. They showed a considerable impact of the shape drag on the critical conditions and the heat and mass exchange rates. Multiple stable and oscillatory solutions coexisted near the criticality and vertically moving waves were observed. The linear and double-diffusive convection in a horizontal porous medium filled with a linked nano-fluid was analytically and numerically explored by Khan et al., [34]. The Fourier series method employed the equation regulating the phenomenon. The Dufour effect and the Soret effect are two examples of concentration gradient-induced heat flow and temperature gradient-induced material flow, respectively. They discovered that the torque constancy parameter enhances the system's stability in both oscillatory and stationary convection modes. A theoretical and numerical study of Soret-induced convection in a horizontal porous layer saturated with a mixture of n components was conducted by Mutschler and Mojtabi [35]. Ali et al., [36]. studied the impact of magnetic field on the flow behavior of a non-Newtonian Casson fluid in a constricted channel using Darcy's law for steady and pulsatile flows. The wall shear stress (WSS) had an incentive trend as a function of the magnetic parameter, Strouhal number, and Casson parameter. In addition, the flow separation region can be controlled by the magnetic parameter. Analytical and numerical solutions of 2D sakiadis flow of non-Newtonian Casson fluid with convective boundary conditions based on the Buongiorn's mathematical model was studied by Ghiasi and Saleh [37]. They found that the skin friction coefficient for non-Newtonian fluid is found to be higher than that of the Newtonian one. In addition, the thermal boundary layer thickness is greatly affected by the resistive Lorentz force and viscous dissipation. Wang et al., [38] studied numerically the implications of temperaturedependent viscosity and thermal conductivity for heat and mass transport of Williamson nanofluids across a nonlinear stretching sheet of irregular thickness are examined when biconvection of microorganisms is incorporated. They found that the value of Brownian motion and Lewis number reduce the concentration of nanoparticles. In addition, the velocity of non-Newtonian is less than the viscous nanofluid but temperature behaves oppositely. Khdher et al., [39] studied the secondary flow configuration in square straight channel with heat transfer enhancement of water and three different types nanofluids (Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub> and CuO) water a base fluid under constant heat flux in upper and lower walls. CFD software were employed to perform the investigation numerically in the range of Reynolds number 104-106. They concluded that by increasing Reynolds number the secondary flow increases as well as shear stress is increase. In addition, the volume concentration increases, the wall shear stress and heat transfer rates increase. Nanofluid with CuO, nanoparticle achieved higher Nusselt number followed by  $TiO_2$  and  $Al_2O_3$ , respectively. The steady of stagnation point flow and radiative heat transfer of a non-Newtonian fluid which is Casson fluid passing over an exponentially permeable slippery Riga plate was studied by Yusof et al., [40]. They recorded that the momentum boundary layer thickness increases with increasing the values of Casson parameter. The temperature decreases when the velocity slip parameter and thermal slip parameter are increased. Khan et al., [41] studied the effectiveness of utilizing the suspension of nanoparticles in water at supercritical pressures in the mitigation of heat transfer deterioration. The thermohydraulic performances of the supercritical water-based nanofluids are analysed using the dimension less parameters based on normalized Nusselt numbers and Fanning friction factors. They concluded that the increasing nanoparticles delayed and weekend the HTD at pseudocritical region. In addition, increasing nanoparticles increase the overall thermal performance of the base fluid. Significance of biconvection and mass transpiration for MHD micropolar Maxwell nanofluid flow over an extending sheet, was studied by Habib et al., [42]. The similarity variable was used to transform the flow equations into corresponding non-dimensional ODEs. It was reported that motile density profile is decline when Lewis and Peclet numbers are boosted. In addition, the temperature distribution increased for large values of Brownian motion, Rayleigh number and thermophoresis parameters. Awan et al., [43] published a comparative study of hybrid nano liquid (Al<sub>2</sub>O<sub>3</sub>, Cu/Water) and nano liquid (Al<sub>2</sub>O<sub>3</sub>/water) over the linearly extending surface. They found out that the Al<sub>2</sub>O<sub>3</sub>-Cu nano particles proved to be a better heat transforms as compared to Al<sub>2</sub>O<sub>3</sub> nano particle.

In shallow and finite aspect ratio enclosures, Rebhi *et al.*, [44] investigated numerically and analytically the influence of the rheological behavior of non-Newtonian fluids on Rayleigh-Bénard thermosolutal convection instabilities. In an inclined square hollow filled with a non-Newtonian liquid subjected to uniform and constant concentrations and temperatures, while the outer walls are impermeable and adiabatic. The Carreau-Yasuda model was used to represent the rheological behavior of non-Newtonian fluids. These authors studied the effect of the rheological parameters of the model used on the bistability of thermosolutal convection. Lounis *et al.*, [45] statistically explored thermosolutal convection with Soret and Dufour effects. For various values of the governing parameters, the results were presented and examined in terms of streamlines, isotherms, isoconcentration, stream function, and average Nusselt and Sherwood numbers. For increasing Soret and Dufour parameters, heat exchange increases.

This paper studies heat and mass transfer by natural convection inside a saturated square cavity in a porous medium filled with a non-Newtonian fluid. The Carreau-Yasuda model is adopted to represent the behavior of non-Newtonian fluids. The active cavity walls are subject to either Neumann-type thermal and solutale boundary conditions (constant heat and concentration fluxes). The numerical method used to solve the set of governing equations uses the time-accurate finite difference method. The effect of different control parameters, namely, thermal Rayleigh number  $R_T$ , buoyancy ratio, N, Lewis number, Le, cavity tilt angle,  $\Phi$ , and different C-Y parameters (n, E, a and s). The results are discussed in terms of flow function, apparent viscosity, and iso-thermal and isoconcentration lines. Variation of apparent viscosity, flow function, temperature and concentration and profiles, and heat and mass transfer rate.

## 2. Physical and Mathematical Model

The physical model described in Figure 1 considers a double-diffusive convection in a square porous cavity filled with a non-Newtonian fluid. The axes of coordinates *x*, *y* are respectively oriented according to the horizontal and vertical directions. The active walls of this cavity are subjected to a uniform density of heat and mass fluxes while the others are assumed to be adiabatic and impermeable. The rheological behavior of a non-Newtonian fluid can be described by the Carreau-Yasuda model [44-48].



Fig. 1. Schematic of the physical model

The fluid is assumed to be a laminar, incompressible, non-Newtonian, low shear flow. the thermophysical properties are constant, except for the effect of density variation in the buoyancy term. Using the Boussinesq approximation, the variation of the density with temperature and concentration is described by the linearized equation of state as [49]

$$\rho = \rho_0 \left[ 1 - \beta_T \left( T' - T'_0 \right) - \beta_s \left( C' - C'_0 \right) \right]$$
(1)

where  $\rho$  is the fluid density  $\rho_0$  is s the medium density at the Reference at temperature *T* and concentration *C* which represents the temperature and concentration values at the origin of the coordinate system, and  $\beta_T$  and  $\beta_s$  are the thermal expansion coefficient and the concentration

coefficient, respectively which are defined by  $\beta_T = -\frac{1}{\rho_0} \left[ \frac{\partial \rho}{\partial T'} \right]_C$  and  $\beta_C = -\frac{1}{\rho_0} \left[ \frac{\partial \rho}{\partial C'} \right]_T$ .

The governing equations that describe the thermal behavior of the system are conservation of momentum, energy and solute balances by [28]

$$\nabla^{2}\psi' = -\frac{gK\beta_{T}}{v} \left[ \frac{\partial}{\partial x} \left( T' + \frac{\beta_{s}}{\beta_{T}} C' \right) \cos\Phi + \frac{\partial}{\partial y} \left( T' + \frac{\beta_{s}}{\beta_{T}} C' \right) \sin\Phi \right]$$
(2)

$$\left(\rho C\right)_{P} \frac{\partial T'}{\partial t'} + \left(\rho C\right)_{\rho} V' \cdot \nabla T' = k \nabla^{2} T'$$
(3)

$$\varphi \frac{\partial C'}{\partial t'} + V' \cdot \nabla C' = D \nabla^2 C' \tag{4}$$

where  $(\rho C)_p$  and  $(\rho C)_f$  are respectively the heat capacity of the saturated porous medium and the fluid, V' is the Darcy speed, g is the gravitational acceleration, v is the kinematical viscosity, k and D are the heat conductivity and the isothermal diffusion coefficient,  $\phi$  is the normalized porosity of the porous medium,  $\psi'$ , the stream function is defined such that  $v' = -\partial \psi' / \partial x'$ ,  $u' = \partial \psi' / \partial y'$ .

In the present work, the fluid considered is a purely viscous fluid, it is a rheofluidic fluid whose viscosity,  $\mu$ , obeys the Carreau-Yasuda model [44-48]

$$\frac{\mu - \mu_{\infty}}{\mu_0 - \mu_{\infty}} = \left[1 + \left(E'\dot{\gamma}'\right)^a\right]^{(n-1)/a}$$
(5)

where  $\mu_0$  represents is the fluid's viscosity at zero shear rates,  $\mu_{\infty}$  is the fluid's viscosity at infinite shear rates. The shear-thinning index is shown by n < 1. The fluid's time character is represented by  $E' \cdot \dot{\gamma}'$  is the shear rate amplitude, and the transition between the zero-shear-rate zone and the power-law area is described by the dimensionless parameter a.

In order to proceed to the numerical solution of the system, we introduce the following nondimensional variables [26,27]

$$(u, y) = \frac{(x', y')}{H'}, \quad t = \frac{t'\alpha}{\sigma H'^2}, \quad (u, y) = \frac{(u', v')H'}{\alpha}, \quad \psi = \frac{\psi'}{\alpha}, \quad \varepsilon = \phi/\sigma, \quad T = \frac{(T' - T_0')}{\Delta T^*}, \quad C = \frac{(C' - C_0')}{\Delta C^*}, \\ \Delta T^* = \frac{q'H'}{k}, \quad \Delta C^* = \frac{j'H'}{\rho_0 D}, \quad \mu_{CY} = \frac{\mu}{\mu_0}, \quad E = \frac{E'\alpha}{\varepsilon H'^2}$$
(6)

where *k* and  $\alpha$  are the thermal conductivity and thermal diffusivity respectively and  $\mu_0$  is the dynamic viscosity of a Newtonian fluid.

The mass, momentum, energy, and concentration equations, considering the applied assumptions are as

$$\frac{\partial}{\partial x} \left( \mu \frac{\partial \psi}{\partial x} \right) + \frac{\partial}{\partial y} \left( \mu \frac{\partial \psi}{\partial y} \right) = -R_T \left[ \frac{\partial}{\partial x} (T + NC) \cos \Phi + \frac{\partial}{\partial y} (T + NC) \sin \Phi \right]$$
(7)

$$\frac{\partial T}{\partial t} + \frac{\partial \psi}{\partial y} \frac{\partial T}{\partial x} - \frac{\partial T}{\partial y} = \nabla^2 T$$
(8)

$$\frac{\partial C}{\partial t} + \frac{\partial \psi}{\partial y} \frac{\partial C}{\partial x} - \frac{\partial \psi}{\partial x} \frac{\partial C}{\partial y} = Le^{-1} \nabla^2 C$$
(9)

In this study, the behavior of the non-Newtonian fluid is described by the non-Newtonian is described by the phenomenological constitutive model of Carreau-Yasuda [44-48].

$$\mu_{CY}(\gamma) = \mu(\gamma) = s + (1 - s) \left[ 1 + (E|\dot{\gamma}|)^a \right]^{(n-1)/a}$$
(10)

where  $\mu$  denotes the apparent viscosity that is shear-dependent is the dimensionless sheardependent apparent viscosity.  $s = \mu_{\infty} / \mu_0$ , is the report of viscosities with infinite to zero shear-rates. E a dimensionless time constant, whose inverse is the critical shear rate marking the beginning of shear-thinning. a is dimensionless parameter describing the transition region between the zero shear-rate region. n, which is less than unity for pseudoplastic fluids, is the exponent of the powerlaw that characterizes the shear-thinning regime. The following is how the dimensionless rate-ofstrain  $\dot{\gamma}$  is expressed

$$\dot{\gamma} = \left[ 4 \left( \frac{\partial^2 \psi}{\partial x \partial y} \right)^2 + \left( \frac{\partial^2 \psi}{\partial y^2} - \frac{\partial^2 \psi}{\partial x^2} \right)^2 \right]^{1/2}$$
(11)

The system's walls are subjected to the equivalent dimensionless boundary conditions, which are [28]

$$u = v = 0, \ \psi = 0, \ \frac{\partial \psi}{\partial x} = \frac{\partial \psi}{\partial y} = 0 \tag{12}$$

and the thermal and solutal boundary conditions

$$\frac{\partial T}{\partial x} = \frac{\partial C}{\partial x} = 0 \text{ at } x = \pm \frac{1}{2}, \text{ and } \frac{\partial T}{\partial y} = \frac{\partial C}{\partial y} = -1 \text{ at } y = \pm \frac{1}{2}$$
(13)

The fluid flow, heat and mass transfer are characterized by the following parameters dimensionless parameters, namely the Darcy-Rayleigh number,  $R_T$ , the buoyancy ratio, N, the Lewis number, Le, and the normalized porosity,  $\varepsilon$ .

$$R_{T} = \frac{\rho_{0}\beta\Delta T'KH'}{\mu_{0}\alpha}, \quad N = \frac{\beta_{s}\Delta C^{*}}{\beta_{T}\Delta T^{*}}, \quad Le = \frac{\alpha}{D}, \quad \varepsilon = \frac{\phi}{\sigma}$$
(14)

The local and average Heat and mass transfer rates on the hot wall can be expressed in terms of the Nusselt and Sherwood numbers and can be obtained from the following expressions

$$Nu^{-1} = \Delta T = T_{(0,-1/2)} - T_{(0,1/2)}$$
 (Neumann) or (15)

$$Nu = -\frac{\partial T}{\partial y}\Big|_{y=\pm 1/2}$$
 (Dirichet) and (16)

$$Nu_{m} = A^{-1} \int_{-A/2}^{A/2} Nu dx$$
(17)

$$Sh^{-1} = \Delta C = C_{(0,-1/2)} - C_{(0,1/2)}$$
 (Neumann) or (18)

$$Sh = -\frac{\partial C}{\partial y}\Big|_{y=\pm 1/2}$$
 (Dirichet) and (19)

$$Sh_m = A^{-1} \int_{-A/2} Shdx \tag{20}$$

#### **3. Numerical Solution**

Previously discretized using the conventional centered approach. For convective flow simulations in a two-dimensional porous layer saturated with a non-Newtonian fluid, a double precision FORTRAN-95 algorithm was created.

First, the time terms that appeared in the governing equations based on the implicit alternating direction technique were discretized for the two-dimensional governing Eq. (7) to Eq. (9) using a second-order backward finite difference scheme (ADI).

To accelerate the convergence of the program and avoid the divergence of the solution at each time step, we used the sub-relaxation technique. The following convergence condition has been verified

$$\frac{\sum_{i}\sum_{j} \left| \psi_{i,j}^{k+1} - \psi_{i,j}^{k} \right|}{\sum_{i}\sum_{j} \left| \psi_{i,j}^{k} \right|} \le 10^{-8}$$

$$(21)$$

where  $\psi_{i,j}$  is the value of the stream function at the iteration's node (*i*, *j*).

For thermosolutal natural convection, the best numerical results were achieved in a square cavity with a non-Newtonian fluid inside of it. For the Neumann and Dirichlet thermal boundary conditions, respectively, the results of the current technique were compared with those given by numerous publications as shown in Table 1 to Table 3. It was discovered that the uniform mesh size of  $(N_x \times N_y = 100 \times 100)$  provided good agreement between the current results and the information published in prior investigations.

Table 1

Comparison of  $\psi_0$ , Nu,  $Nu_m$ , and  $\mu$  with some previous studies numerical results for Neumann thermal boundary conditions,  $R_T = 50$ , E = 0.2,  $s = 10^{-2}$ , a = 2 and versus n

Neumann thermal boundary conditions									
n	Khechiba <i>et al.,</i> [28]			Present study			Present study vs Khechiba et al., [28]		
	1	0.8	0.6	1	0.8	0.6	1	0.8	0.6
$\psi_0$	1.915	2.235	2.872	1.914	2.235	2.869	0.05((%)	0.00(%)	0.10(%)
Nu	1.912	2.221	2.778	1.912	2.221	2.777	0.00	0.00	0.03
$Nu_m$	1.719	1.964	2.431	1.719	1.964	2.431	0.00	0.00	0.00
μ				1.000	0.815	.456			

#### Table 2

Comparison of  $\psi_0$ , Nu,  $Nu_m$ , and  $\mu$  with some previous studies numerical results for Dirichlet thermal boundary conditions,  $R_T = 70$ , E = 0.6,  $s = 10^{-2}$ , a = 2 and versus n

Dirichlet thermal boundary conditions									
n	Khechiba <i>et al.,</i> [28]			Present study			Present study vs Khechiba et al., [28]		
	1	0.8	0.6	1	0.8	0.6	1	0.8	0.6
$\psi_0$	3.715	6.685	14.017	3.717	6.716	14.076	2.74(%)	0.46(%)	0.42(%)
Nu	2.139	3.253	4.707	2.139	3.261	4.717	0.00	0.24	0.21
$Nu_m$	2.046	3.178	5.148	2.046	3.185	5.148	0.00	0.22	0.00
μ				1.000	0.525	0.169			

#### Table 3

Validation of the numerical code in terms of the flow function at the center of the cavity,  $\psi_{max}$ , the Nusselt number,  $Nu_m$ , and the Sherwood number,  $Sh_m$  for  $R_T = 100$ , N = -0.8, Le = 10 and A = 4

	Benhadji [50]	Mamou and Vasseur [51]	Present study	Present study vs Benhadj [50]	Present study vs Mamou and Vasseur [51]
$\psi_{max}$	3.695	3.689	3.688	0.18(%)	0.02(%)
$Nu_m$	3.653	3.635	3.643	0.27	0.21
$Sh_m$	6.747	6.737	6.743	0.05	0.08

### 4. Results and Discussion

The results are performed for different quantities of the Carreau-Yasuda parameters, i.e., n, E, s, and a, thermal Rayleigh number,  $R_T$ , buoyancy ratio, N, Lewis number, Le, and inclined angel,  $\gamma$ . Numerical results are provided in the range of:  $0.4 \le n \le 1$ ,  $0 \le E \le 0.6$ ,  $0 \le s \le 1$ ,  $0.85 \le a \le 2$ ,  $0 \le R_T \le 100$ ,  $10^{-1} \le Le \le 10^2$ ,  $-5 \le N \le 5$  and  $0^\circ \le \Phi \le 90^\circ$ . Figure 2 shows the effect of power law index, n, on the streamlines, isotherms, iso-concentrations, and the contours of the apparent viscosity of the square cavity, are presented from left to right, respectively. It can be seen clearly with a decrease in the power-law index, n, the streamlines become elliptical in the concentration of is on the hot wall. This confirms that decreasing of the power-law index, n, enhances heat transfer and mass. The apparent viscosity also changes with the change in power index, n, the transition from a Newtonian fluid (n = 1) to a non-Newtonian fluid (n < 1) is more complex and distorted.

Figure 3 presents the different time constant parameter, E, on the streamlines, isotherms, isoconcentrations and apparent viscosity contours for the square cavity. Increasing the, E, parameter increases the expansion of loops. Furthermore, the iso-concentrations gradient on the thermal wall decreases by the parameter, E, decreases from 0 to 0.6. the mass transfer improves when e decreases. Also, if the amount of parameter, E, is reduced, the fluid becomes highly viscous (when E=0  $\rightarrow$  Newtonian fluid  $\mu$ =1).

Figure 4 displays streamlines, isotherms, iso-concentrations, and apparent viscosity in different values of values of the ratio of infinite to zero shear rate viscosities, *s*. The movement of the streamlines is confirmed by the decrease of parameter, *s*. Also, the contours show that the iso-concentrations density on the hot wall increases with decreasing parameter, *s*. On one hand, the apparent viscosity of the fluids is improved (Newtonian fluid).

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**Fig. 2.** Effect of the power-law index, n, on : (a) streamlines, (b) isotherms, (c) is-concentrations and (d) apparent viscosity contours for  $R_T = 50$ , E = 0.2, S = 0.01, a = 2, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

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**Fig. 3.** Effect of the Time constant number, E, on : (a) streamlines, (b) isotherms, (c) is-concentrations and (d) apparent viscosity contours for  $R_r = 50$ , S = 0.01, n = 0.6, a = 2, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

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**Fig. 4.** Impact of the different parameter, *s*, on : (a) streamlines, (b) isotherms, (c) is-concentrations and (d) apparent viscosity contours for  $R_T = 50$ , E = 0.2, n = 0.6, d = 2, Le = 10, N = -0.5 and  $\Phi = 0^\circ$ 

Figure 5 resumes different values of parameter, a. on the streamlines, isotherms, isoconcentrations, and the apparent viscosity. Comparing the flow models, a decrease in the parameter a increases the convection process. On one hand, when the parameter, a, decreases, the concentration density on the hot wall increases. similar to the temperature is improved by decrease the value of parameter, a. The pattern demonstrates that the process creates a rise in the gradient of temperature and concentration on the hot wall, which leads to an increase in heat and mass transfer as the parameter a are lowered. In addition, the apparent viscosity increases with decrease of the parameter of, a, (a < 1, shear-thinning fluids).

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**Fig. 5.** Effect of the different parameter, *a*, on: (a) streamlines, (b) isotherms, (c) is-concentrations and (d) apparent viscosity contours for  $R_r = 50$ , n = 0.6, E = 0.2, s = 0.01, Le = 10, N = -0.5 and  $\Phi=0^{\circ}$ 

Figure 6 shows how the stream-function, apparent viscosity, temperature, and concentration profiles are affected by the power-law index, n. The profiles are symmetrical with respect to the center of the cavity. Figure 6(a) shows that the flow function goes from zero at the walls to a maximum at the center of the system. Furthermore, the flow function increases with decreasing power-law index, n. the effect of the power index, n. while the fluid becomes thinner at shear. On the apparent viscosity  $\mu$  as shown in Figure 6(b), increasing the power index, n, leads to an increase in the value of the viscosity to become constant (at Newtonian fluid). the effect of the power index, n, on the temperature profiles is shown in Figure 6(c) as the power index, n, decreases, the temperature decreases toward the center of the system. which leads to a significant increase in the convective heat transfer rate (i.e., Nu number). The concentration decreases with decreasing n and then increases towards the center of the cavity, as shown in Figure 6(d).

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**Fig. 6.** Effect of the power-law index, *n*, on: (a) stream-function,  $\psi$  (b) apparent viscosity,  $\mu$ , (c) temperature, *T*, and (d) concentration, *C*, profiles for  $R_T = 50$ , E = 0.2, a = 2, s = 0.01, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

Figure 7 present of the different time constant parameter, E, on the stream-function, apparent viscosity, temperature and the concentration profiles. Figure 7(a) illustrates the flux intensity increase for large values of parameter, E. The apparent viscosity,  $\mu$ , is symmetric about the center of the cavity, as shown in Figure 7(b). A decrease in the values of, E, results in an increase in the apparent viscosity from E = 0.6 (non-Newtonian fluid) to E = 0 (Newtonian fluid), so that the strength of convective motion is significantly increased by the increase in the value of E. Figure 7(c) and Figure 7(d) show that a decrease in the values of, E, results in a slight increase in the temperature and concentration difference between the walls.

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**Fig. 7.** Influence of the different time constant parameter, *E*, on: (a) stream-function,  $\psi$  (b) apparent viscosity,  $\mu$ , (c) temperature, *T*, and (d) concentration, *C*, profiles for  $R_T = 50$ , n = 0.6, a = 2, s = 0.01, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

The effects of the ratio of infinite to zero shear rate viscosities, s, on the temperature, concentration profiles, apparent viscosity, and stream function are shown in Figure 8. Figure 8(a) shows that a decrease in the parameter, s, leads to an increase in the flow intensity near the walls. The effect of parameter, s, on apparent viscosity, as shown in Figure 8(b), the shear- thinning effect becomes significant on the walls and center of the cavity as the parameter s decreases, resulting in a decrease in the viscosity of the fluid ( $s = 1, \mu = 1$ ). The influence of the parameter, s, on the temperature profiles is shown in Figure 8(c). The temperature difference decreases with decreasing values of s from (s = 1 to s = 0). In addition, the strength of heat transfer by convection is moderately enhanced by decreasing this parameter, s. Figure 7(d) shows that the effect of the values of, s, results in a slight increase with the variation of the parameter, s.

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**Fig. 8.** Impact of the ratio of infinite-to zero-shear-rate viscosities, *S*, on (a) stream-function,  $\psi$ , (b) apparent viscosity,  $\mu$ , (c) temperature, *T*, and (d) concentration, *C*, profiles for  $R_T = 50$ , n = 0.6, a = 2, E = 0.2, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

Figure 9 displays the effects of parameter, a, on the stream-function, apparent viscosity, temperature and the concentration. Figure 9(a) shows the influence of the parameter, a, on the profiles of the flow function, it was observed that when the parameter, a, decreases, the flow intensity increases very slightly. The effect of the parameter, a, on the apparent viscosity,  $\mu$ , is given in Figure 9(b) where the viscosity increases with increasing parameter, a. Furthermore, Figure 9(a) and Figure 9(d) shows that the effect of the parameter, a, leads to a slight increase in the temperature and concentration difference in the wall.

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**Fig. 9.** Effect of parameter, *a*, on: (a) stream-function,  $\psi$ , (b) apparent viscosity,  $\mu$ , (c) temperature, *T*, and (d) concentration, *C*, profiles for  $R_T = 50$ , n = 0.6, s = 0.01, E = 0.2, Le = 10, N = -0.5 and  $\Phi = 0^{\circ}$ 

Figure 10 clearly shows that the viscosity increases significantly with decreasing shear rate for different values of rheological parameters of Carreau-Yasuda. The viscosity is  $\mu$ =1 when the fluid is Newtonian n=1 as shown in Figure 10(a). In contrast, in Figure 10(b), decreasing the parameter *E* induces an increase in viscosity  $\mu$ =1 for *E*=0. This allows us to deduce that the apparent viscosity decreases with large values of *E*. We also observe that the apparent viscosity is favored by the increase of the parameter *s* when it takes a value of *s*=1. The viscosity is increased for the variation of the parameter a between 0.9 and 2.

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**Fig. 10.** Display the apparent viscosity,  $\mu$ , with the shear rate,  $\dot{\gamma}$ , on: (a) effect of, n, (b) effect of time constant parameter, E, (c) effect of, s, and (d) effect of, a, for Le = 10,  $R_T = 50$ , E = 0.2, a = 2 and s = 0.01 and  $\Phi=0^{\circ}$ 

Figure 11 shows the influence of the power-law index, n, on the flow intensity, apparent viscosity, Nusselt number and Sherwood number as a function of,  $R_T$ . The results clearly indicate that for given values of, n, there is a supercritical or subcritical Rayleigh number for a single-cell convection flow. Figure 11(a) shows that the convective flux improves with increasing, n. The same is true for the heat and mass transfer rates, which improves with increasing, n, (Figure 11(c) and Figure 11(d)). Decrease of the power-law index, n, leads to a decrease of the apparent viscosity whose main role is to reduce the viscous resistances on the one hand and to improve the convective flow on the other hand as shown in Figure 11(b). in the case of  $\psi_0 = 0$ . Nu = Sh = 1 and  $\mu = 1$ , the figure shows that the convection flux is supercritical below the critical value, the solution is purely conductive.

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**Fig. 11.** Effect of,  $R_T$ , and power-law index, n, on: (a) stream function at the center of the cavity,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, Sh, and (d) Nusselt number, Nu, for Le = 10, N = -0.5, n = 0.6, a = 2, s = 0.01 and  $\Phi=0^{\circ}$ 

Figure 12 shows the influence of parameter, E, on stream function, apparent viscosity, Sherwood number and Nusselt number versus power-law index, n. Figure 12(a) shows the flow function as a function of power-law index, n, such that the flow intensity increases with decreasing parameter, E, and increases with decreasing power-law index, n. The effect of parameter, E, on the apparent viscosity is shown in Figure 12(b) where the viscosity increases with decreasing parameter, E, from E = 0.6 (non-Newtonian fluids  $\mu$ <1) to E = 0 (Newtonian fluids  $\mu$ =1) and decreases with increasing power-law index (n). Furthermore, Figure 12(c) and Figure 12(d) show that a decrease in, E, leads to a decrease in the Sherwood number and Nusselt number, while when, n, decreases, the heat and mass exchange increases.

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**Fig. 12.** Effect of parameter, *E*, and power-law index, *n*, on: (a) stream function at the center of the cavity,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, *Sh*, and (d) Nusselt number, *Nu*, for  $R_T = 50$ , Le = 10, N = -0.5, a = 2, s = 0.01 and  $\Phi=0^{\circ}$ 

The result of the parameter, *s*, and, *n*, on the flow function, apparent viscosity, Sherwood number and Nusselt number is given in Figure 13. In Figure 13(a), the flow function decreases with increasing *n*. The viscosity increases with increasing *n*, reaching a maximum value at n = 1 (Newtonian fluids  $\mu$ =1) as shown in Figure 13(b). Figure 13(c) and Figure 13(d) show that *Sh* and *Nu* decrease with increasing *n*, from 0.4 to 1, leading to an improvement in heat and mass exchange rates.

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**Fig. 13.** Effect of the ratio of infinite-to zero-shear-rate viscosities, *S*, and power-law index, *n*, on: (a) stream function at the center of the cavity,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, *Sh*, and (d) Nusselt number, *Nu*, for  $R_T = 50$ , Le = 10, N = -0.5, E = 0.2, a = 2 and  $\Phi=0^{\circ}$ 

Figure 14 illustrates the effects of parameter, a, on stream function, apparent viscosity, Sherwood number and Nusselt number as a function of power-law index, n. Figure 14(a) shows the changes in the flow function as a function of the power-law index, n, where the flow function increases with a decrease in both parameters, a. Figure 14(b) shows that an increase in the power index, n, and the parameter, a, of a lead to an increase in the apparent viscosity from  $\mu$ <1 (non-Newtonian fluids) to  $\mu = 1$  (Newtonian fluids). In addition, the influence of parameters, a, and, n, on the Sherwood number where Sherwood decreases slightly when the number, a, decreases and increases when the power-law index, n, decreases. The same explanation with the Nusselt number in Figure 14(d).

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**Fig. 14.** Effect of parameter, a, and power-law index, n, on: (a) stream function at the center of the cavity,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, Sh, and (d) Nusselt number, Nu, for  $R_T = 50$ , Le = 10, N = -0.5, E = 0.2, s = 0.01 and  $\Phi = 0^{\circ}$ 

Figure 15 present the effects of, n, on the stream function, apparent viscosity, Sherwood and Nusselt number versus of buoyancy report, N. This covers the region where the flow becomes cooperative and dominated by solute effects (aid flow N = 5), the region where the flow is purely dominated by thermal effects (thermal flow N = 0), and the region where the forces are opposite but the flow by solute effects (reverse flow N = -5), i.e., (solutally dominated) the flow circulation is clockwise) ( $\psi < 0$ ), see the streamlines in Figure 16(b). In the case N = 0, i.e., in the case where concentration effects are absent the convective motion is induced by the temperature gradients only which leads to a counter-clockwise circulation ( $\psi > 0$ ), see the streamlines in Figure 16(a). On the other hand, the flow function increase with deceasing of the power-law index, n, as shown in Figure 15(a). In the case where N is greater than zero, the clockwise convective motion is said to be coincident, and the thermal and solute effects act in the same direction, and the flow of the current function is dominated by the buoyancy force. On the other hand, for N less than zero at 1.5 < N < 0when the thermal effect is dominant, the flow function is positive. In the same interval, the transition from the conductive to the convective regime when the number of, n, is deceased for  $R_T = 50$  is lower than the number of supercritical, N<sub>cr</sub>. Then, for large negative values, the solute effect is clear dominant and the flow becomes negative. Below the critical value, the solution is purely conductive  $(\psi = 0, Nu = Sh = 1)$  whatever the amplitude of the perturbation. The flow behavior depends strongly on the buoyancy rate, whether it is less than -1 or greater than -1, and it is found that the effect persists when the flow rate is zero. As *n* decreases from (n = 1 to n = 0.4) and, *N*, increases, we observe a slight difference in viscosity at  $\mu = 1$  (Newtonian fluids), and then decreases sharply to reach shear thinning values  $\mu < 1$ . Also, as *n* decreases and the buoyancy rate increases from -1 to 1, the number of *Sh* and *Nu* increases, confirming the improvement in thermal and mass exchange rates as shown in both Figure 16(c) and Figure 16(d).



**Fig. 15.** Influence of buoyancy ratio, N, and, n, on: (a) stream function at the center of the cavity,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, Sh, and (d) Nusselt number, Nu, for Le = 10,  $R_T = 50$ , E = 0.2, a = 2, s = 0.01 and  $\Phi=0^{\circ}$ 

![](_page_24_Figure_1.jpeg)

**Fig. 16.** Streamlines, isotherms, iso-concentrations and apparent viscosity from clockwise (N > 0) to counterclockwise (N < 0) for  $R_T = 50$ , n = 0.6, E = 0.2, S = 0.01, a = 2, Le = 10 and  $\Phi=0^{\circ}$ : (a) N = 4, (b) N = -4

The impact of Lewis number, *Le*, and, power-law index, *n*, on the stream function, apparent viscosity, Sherwood number and Nusselt numbers is presented in Figure 17. Figure 17(a) shows that the stream function increases significantly with the decrease of, *n*, to reach  $\psi_0 = 2.263$  at the domain (*Le*=10<sup>-1</sup> to *Le*=10<sup>1</sup>), and then starts to decrease gradually to remain constant. Figure 17(b) shows the changes in apparent viscosity as a function of *Le*, for different amounts of *n*. As, *n*, increases and *Le* increases, the viscosity increases to  $\mu = 1$  for n = 1 (Newtonian fluids). An increase in, *Le*, leads to an increase in *Sh* and *Nu*, and increases with decreasing power-law index. Furthermore, this confirms the improvement in mass and heat exchange, are plotted in Figure 6(c) and Figure 6(d).

Figure 18 display the effects of inclined angel,  $\Phi$ , on stream function, apparent viscosity, Sherwood number and Nusselt number as a function of power-law index, n. The results show that a decrease in inclined angle leads to a significant increase in flow behavior as shown in Figure 18(a). Figure 18(b) shows a decrease in viscosity with an increase in,  $\gamma$ , and on the one hand, a decrease in the angle of inclination leads to a significant increase in, Sh, and, Nu, of  $\Phi$  (30° to 90°) to reach their maximum value at  $\Phi = 45^{\circ}$ . Furthermore, with a decrease in the power-law index, which led to an improvement in heat and mass, as show in Figure 18(c) and Figure 18(d). Journal of Advanced Research in Fluid Mechanics and Thermal Sciences Volume 99, Issue 2 (2022) 17-47

![](_page_25_Figure_1.jpeg)

**Fig. 17.** Effect of, *Le*, and power-law index, *n*, on: (a) stream function,  $\psi_0$ , (b) apparent viscosity,  $\mu$ , (c) Sherwood number, *Sh*, and (d) Nusselt number, *Nu*, for  $R_T = 50$ , N = -0.5, a = 2, E = 0.2, s = 0.01 and  $\Phi=0^{\circ}$ 

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![](_page_26_Figure_1.jpeg)

**Fig. 18.** Impact of inclined angel,  $\Phi$ , and, n, on: (*a*) stream function at the center of the cavity,  $\psi_0$ , (*b*) apparent viscosity,  $\mu$ , (*c*) Sherwood number, *Sh*, and (*d*) Nusselt number, *Nu*, for Le = 10, Ra = 50, E = 0.2, a = 2, s = 0.01 and N = -0.5

#### 5. Conclusions

In this paper, we have presented the effect of rheological parameters on double-diffusive convection in a square porous medium saturated by non-Newtonian power-law fluids with yield stress. While the authors' walls were thought to be adiabatic and impermeable, the active walls were subjected to uniform heat and mass fluxes. The entire governing equation was used to arrive at the asymptotic numerical solution.

For some values of the governing parameters of the problem, the Rayleigh number  $R_T$ , and the four dimensionless parameters of the Carreau-Yasuda rheological model, namely: n, E, s, a and buoyancy ratio N, Lewis number Le, and inclination angle  $\Phi$ , are obtained numerical results for the stream function, viscosity, temperature, and concentration.

As a result, the cavity's ability to transport heat is greatly impacted. The following is a summary of the investigation's principal conclusions

i. The temperature and concentration increase when the number of power-law indices, *n*, and *E* decreases. On the other hand, they increase when the parameters, *s*, decrease.

- ii. It was discovered that for a particular set of Carreau-Yasuda parameters, the intensity of the mean viscosity reduces with a decrease in n and s as well as a decrease in E and a.
- iii. The decrease in the Carreau-Yasuda parameters (n, E, s, a) and the increase in thermal Rayleigh have increased the flux density.
- iv. In the total convection regime, the flow structure and the temperature and concentration fields are sensitive to a change in all parameters of Carreau-Yassuda model. Indeed, for a given thermal Rayleigh number, both the flow intensity and heat and mass transfers are favored when increasing (decreasing) the value of *E* and decreasing (increasing) the values of *s* and *n*.
- v. For a given set of Carreau-Yasuda parameters, it was found that with an increase of  $R_T$  and a decrease of n, the mean viscosity strength decreases. Therefore, the heat transfer by convective heat transfer is enhanced with an increase in  $R_T$  and a decrease of n. For small values of the parameter, n, the flow can be oscillatory.
- vi. Heat and mass transfer rates improved as the apparent viscosity decreased with the Rayleigh number and increased with the Lewis number.
- vii. Increasing the Lewis number, *Le*, or decreasing the power-law index, *n*, increases the fluid circulation and heat and mass transfer rates. In addition, the Lewis number, Le, is found to play a role in favoring the contribution of the forced regime in the overall convection as it increases, especially when the power-law index, *n*, decreases.
- viii. Increasing the buoyancy ratio, *N*, improves heat and mass transfer due to the prevailing buoyancy force. Moreover, the transition from conductive (for low values of the buoyancy force) to convective regime (higher buoyancy forces).
- ix. The values of Nu and Sh increase as the angle of inclination decreases from 90° to 30°. Namely, the effect of the load is strongest at 45°.
- x. The present study can be further extended to analyze the more complicated rheological behavior of other shear-thinning and shear-thickening fluid in a three-dimensional cavity model.

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