



## Unsteady MHD Rear Stagnation-Point Flow of a Hybrid Nanofluid with Heat Generation/Absorption Effect

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### ABSTRACT

The study of unsteady flow is essential in various engineering systems, for instance, the periodic fluid motion and start-up process. Therefore, this numerical study focuses on examining the unsteady magnetohydrodynamics (MHD) rear stagnation-point flow in  $Al_2O_3-Cu/H_2O$  hybrid nanofluid past a permeable stretching/shrinking surface with the impact of heat generation/absorption. By choosing a suitable similarity transformation, partial differential equations are transformed into a system of nonlinear ordinary differential equations and solved using the *bvp4c* function in the MATLAB package. The effects of the solution domain's operating parameters are analyzed, and dual solutions are observable as the sheet shrinks. It is found that the addition of the suction parameter escalates the heat transfer efficiency. Eventually, the existence of the unsteadiness parameter and the heat generation/absorption effect significantly encourage heat transfer deterioration.

## 1. Introduction

In producing better heat transfer mechanisms, hybrid nanofluids, which comprehend a homogeneous suspension of more than one nanoparticle possessing chemical and physical bonds, opens up another arena. The essential idea of this new form of nanofluid is to acquire development in heat transfer, thermophysical and hydrodynamic properties because of their potential role in many thermal applications, including fuel cells, hybrid-powered engines, and pharmaceutical processes [1-3].

Recently, multiple scientific experiments and numerical studies on hybrid nanofluid have been conducted. Jana *et al.*, [4] pioneered the investigation toward the thermal conductivity of several types of nanomaterial, including mono and hybrid nanomaterials. The study revealed that the nanofluid stability was directly affected by the properties of nanoparticles. Meanwhile, Turcu *et al.*, [5] were among the first to document the synthesis and characterisation of hybrid nanocomposite particle. However, it is reported that the thermal conductivity of the single nanoparticles shows

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higher values in comparison with the hybrid nanocomposite particles due to the nanoparticle's compatibility effect. Nevertheless, Selvakumar and Suresh [6] demonstrated that the convective heat transfer coefficient in electronic heat sink is improved dramatically when  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  is operated as the working fluid. An earlier study of the heat transfer enhancement in hybrid nanofluid using numerical analysis was conducted by Balla *et al.*, [7]. In another study, Takabi and Salehi [8] found out that the use of hybrid nanofluid increases the heat transfer efficiency, resulting in improved cooling efficiency and lower heated surface temperature. Since then, the study of nanofluid and hybrid nanofluid has attracted interest from many researchers considering various effects [9-17].

Previous investigations implied that the study of stagnation point flow plays an important role in several industrial and technological processes such as extrusion activity and polymer industry [18-20]. The classic problem of stagnation point in two-dimensional flow are related to Hiemenz [21] and Homann [22]. Meanwhile, the development of the boundary layer rear stagnation point at three-dimensional flow was established by Howarth [23-24], who extended the interesting work of Proudman and Johnson [25] and Robins and Howarth [26]. Later, the MHD impact in the unsteady rear stagnation point was tackled by Katagiri [27]. Turkyilmazoglu *et al.*, [28] performed the unsteady MHD rear stagnation point in the permeable and deformable sheet, and it is reported that the inclusion of unsteadiness and magnetic parameters consequently reduced the thickness of the boundary layer. In actual applications, the magnetic field plays an important role in rearranging the field of flow. The study of MHD in boundary layer flow is very important in the industry since its demand has continued in diverse fields of science, for instance, metallurgical procedures and petroleum production [29]. Some researches that implemented nanofluid and hybrid nanofluid as working fluid to test the effect of MHD can be reviewed in the studies by Zainal *et al.*, [30-31], Abdel-Nour *et al.*, [32], Armaghani *et al.*, [33], and Ishak *et al.*, [34].

To the best of the authors' knowledge, the study of rear stagnation-point flow still lacks intense investigation. Hence, the purpose of this current study is to examine the unsteady MHD rear stagnation point flow in  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid with heat generation/absorption influences. The governing equations are converted into an ordinary differential equations system on the basis of the corresponding transformation. The equation scheme is then numerically explained via the boundary value problem solver (bvp4c) in the MATLAB program. The generated results are significantly in accordance with previous literature. This analysis is original, and all the collected numerical results are authentic.

## 2. Mathematical Formulation

Consider an unsteady two-dimensional rear stagnation-point flow and heat transfer of  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid with magnetic effect past a permeable sheet as demonstrated in Figure 1. Note that the  $x$ -axis moves opposite to the free-stream direction and is perpendicular to the  $y$ -axis. It is assumed that the free-stream velocity is given by  $u_\infty = -u_0x/(1-\beta t)$ , where  $u_0$  and  $\beta$  is a real number and a constant that calculate the unsteadiness strength, respectively. Also, the wall has a moving velocity along the  $x$ -axis with  $u_w = u_0x\lambda/(1-\beta t)$ , and the wall transpiration velocity in the  $y$ -axis is given by  $v_w(x,t)$ . Further, the wall temperature,  $T_w$  as well as the ambient temperature,  $T_\infty$  are considered constant. The hybrid nanofluid is utilised in this study provided that the effect of the agglomeration of nanoparticles on the thermophysical properties is ignored since the nanofluids are assumed to be synthesised as a steady combination. In addition, the size of the nanoparticles is considered to be uniform. Now, by using the standard approximations of the boundary layer, we have [31-35]

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

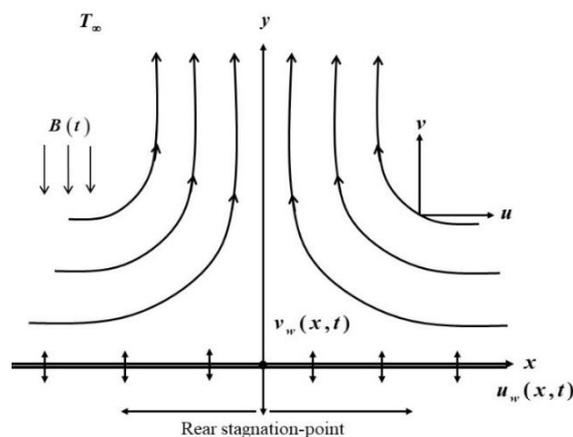
$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = u_\infty \frac{du_\infty}{dx} + \frac{\mu_{hmf}}{\rho_{hmf}} \frac{\partial^2 u}{\partial y^2} - \frac{\sigma_{hmf}}{\rho_{hmf}} B_0^2 (u - u_\infty), \tag{2}$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{k_{hmf}}{(\rho C_p)_{hmf}} \frac{\partial^2 T}{\partial y^2} + \frac{Q}{\rho C_p}, \tag{3}$$

and the boundary conditions are:

$$\begin{aligned} v = v_w(x,t), u = u_w(x,t), T = T_w(x,t), \text{ at } y = 0, \\ u \rightarrow u_\infty(x,t), T \rightarrow T_\infty(x,t), \text{ as } y \rightarrow \infty. \end{aligned} \tag{4}$$

The velocity components along the  $x$  and  $y$  axes are denoted by  $u$  and  $v$ , respectively,  $v_w(x,t)$  is the velocity of the wall mass transfer,  $\rho_{hmf}$  is the density,  $\mu_{hmf}$  is the dynamic viscosity, and  $B_0$  is the transverse magnetic field. Further,  $k_{hmf}$  is the thermal conductivity,  $(\rho C_p)_{hmf}$  is the heat capacity and  $Q$  is the heat generation/absorption coefficient. The considered thermophysical properties of the operating fluid are given in Table 1 [36]. While the correlation coefficient for the hybrid nanofluid is depicted in Table 2 [8-37].



**Fig. 1.** Description of the physical model

**Table 1**  
 The H<sub>2</sub>O, Al<sub>2</sub>O<sub>3</sub> and Cu thermophysical properties

Physical properties	H <sub>2</sub> O	Al <sub>2</sub> O <sub>3</sub>	Cu
$\rho$ (kg / m <sup>3</sup> )	997.1	3970	8933
$C_p$ (J / kgK)	4179	765	385
$k$ (W / mK)	0.613	40	400

**Table 2**  
 The alumina-copper/water (Al<sub>2</sub>O<sub>3</sub>-Cu/H<sub>2</sub>O) correlation coefficient

Properties	Al <sub>2</sub> O <sub>3</sub> -Cu/H <sub>2</sub> O
Density	$\rho_{hnf} = (1 - \phi_{hnf})\rho_f + \phi_1\rho_{s1} + \phi_2\rho_{s2}$
Thermal capacity	$(\rho C_p)_{hnf} = (1 - \phi_{hnf})(\rho C_p)_f + \phi_1(\rho C_p)_{s1} + \phi_2(\rho C_p)_{s2}$
Dynamic viscosity	$\mu_{hnf} = 1 / (1 - \phi_{hnf})^{2.5}$
Thermal conductivity	$\frac{k_{hnf}}{k_f} = \frac{\left[ \left( \frac{\phi_1 k_{s1} + \phi_2 k_{s2}}{\phi_{hnf}} \right) + 2k_f + 2(\phi_1 k_{s1} + \phi_2 k_{s2}) - 2\phi_{hnf} k_f \right]}{\left[ \left( \frac{\phi_1 k_{s1} + \phi_2 k_{s2}}{\phi_{hnf}} \right) + 2k_f - (\phi_1 k_{s1} + \phi_2 k_{s2}) + \phi_{hnf} k_f \right]}$

Thus, the following similarity variables are implemented [28-38]:

$$\psi(x, y, t) = \sqrt{\frac{u_0 v_f}{(1 - \beta t)}} x f(\eta), \quad \eta = \sqrt{\frac{u_0}{(1 - \beta t) v_f}} y, \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \quad (5)$$

$$u = \frac{u_0 x f'(\eta)}{(1 - \beta t)}, \quad v = -\sqrt{\frac{u_0 v_f}{(1 - \beta t)}} f(\eta), \quad v_w = -\sqrt{\frac{u_0 v_f}{(1 - \beta t)}} S, \quad (6)$$

where  $S$  is the constant mass flux parameter and  $v_f$  is the kinematic viscosity. Referring to the similarity variables, Eq. (5) and Eq. (6), Eq. (2) to Eq. (3) are converted into the ordinary differential equations, as such

$$\frac{\mu_{hnf} / \mu_f}{\rho_{hnf} / \rho_f} f''' + f f'' - f'^2 + 1 - \varepsilon \left( f' + \frac{\eta}{2} f'' + 1 \right) - \frac{\sigma_{hnf} / \sigma_f}{\rho_{hnf} / \rho_f} M (f' + 1) = 0, \quad (7)$$

$$\frac{1}{Pr} \frac{k_{hnf} / k_f}{(\rho C_p)_{hnf} / (\rho C_p)_f} \theta'' + f \theta' - f' \theta - \varepsilon \left( \theta + \frac{\eta}{2} \theta' \right) + \delta \theta = 0, \quad (8)$$

along with

$$f(0) = S, \quad f'(0) = \lambda, \quad \theta(0) = 1, \\ f'(\eta) \rightarrow -1, \quad \theta(\eta) \rightarrow 0, \quad (9)$$

where  $M = \sigma_f B / u_0 \rho_f$  is the magnetic coefficient with  $B = B_0 \sqrt{1 - \beta t}$ ,  $Pr = \mu_f C_p / k_f$  is the Prandtl number,  $\varepsilon$  represents the unsteadiness parameter, and  $\delta$  is the heat generation/absorption coefficient.

The physical quantities of concern are  $Nu_x = \frac{xk_{hmf}}{k_f(T_w - T_\infty)} \left( -\frac{\partial T}{\partial y} \right)_{y=0}$ , which is the local Nusselt number and  $C_f = \frac{\mu_{hmf}}{\rho_f u_\infty^2} \left( \frac{\partial u}{\partial y} \right)_{y=0}$  is the skin friction coefficient. Using the above-mentioned information, finally, we obtain:

$$Re_x^{1/2} C_f = \frac{\mu_{hmf}}{\mu_f} f''A(0), \quad Re_x^{-1/2} Nu_x = -\frac{k_{hmf}}{k_f} \theta'(0), \quad (10)$$

where  $Re_x = u_0 x^2 / \nu_f$ .

In this study, the `bvp4c` function in the MATLAB system is implemented to solve the resulting nonlinear ordinary differential equations. The `bvp4c` function is a finite difference code that performs the three stages of the Lobatto IIIa formula. This collocation polynomial provides a C1-continuous solution, which is uniformly accurate in the fourth-order interval at which the function is integrated. For the `bvp4c` solver's execution, the similarity equations in Eq. (7) and Eq. (8) along with the boundary conditions (9) are first converted into the following codes

$$y(1) = f, \quad y(2) = f', \quad y(3) = f'', \quad y(4) = \theta, \quad y(5) = \theta'. \quad (11)$$

Hence, Eq. (7) and Eq. (8) become

$$f''' = -\frac{\rho_{hmf}/\rho_f}{\mu_{hmf}/\mu_f} \left[ ff'' - f'^2 + 1 - \varepsilon \left( f' + \frac{\eta}{2} f'' + 1 \right) - \frac{\sigma_{hmf}/\sigma_f}{\rho_{hmf}/\rho_f} M(f' + 1) \right], \quad (12)$$

$$\theta'' = -Pr \frac{(\rho C_p)_{hmf}/(\rho C_p)_f}{k_{hmf}/k_f} \left[ f\theta' - f'\theta - \varepsilon \left( \theta + \frac{\eta}{2} \theta' \right) + \delta\theta \right], \quad (13)$$

whereas the code for boundary condition is disclosed as

$$ya(1) - S, \quad ya(2) - \lambda, \quad ya(4) - 1, \quad yb(2) + 1, \quad yb(4). \quad (14)$$

At this point,  $ya$  is the condition at  $\eta = 0$  and  $yb$  is the condition at  $\eta = \infty$ . The `bvp4c` function is executed using an appropriate value of the governing parameters with the relevant boundary layer thickness  $\eta_\infty$  until the convergence criteria is accomplished.

### 3. Results Interpretation

The `bvp4c` solver in MATLAB programming is used to elucidate the resulting nonlinear ordinary differential equations presented in Eq. (7) to Eq. (8) in common with the boundary conditions (9). The expressed boundary value problem is demoted to the ordinary differential equations system of the first-order, initially. The `bvp4c` method is a prominent coder exercised by countless investigators to demonstrate the boundary value query. A preliminary forecast of the primary mesh point and the step size of variations is important for the necessary solutions guarantee. The necessary

approximation of boundary layer thickness is vital during an effort to discover more than one solution. The users also need to provide several trials in supplying an excellent preliminary guess before a necessary result is obtained. The reliability of the findings is measured with Turkyilmazoglu *et al.*, [28] and Bhattacharyya [39], as accessible in Table 3. The authors specifically found that the current results conform to the previous work remarkably. Hence, we believe that the intended computational model can be completely applied to determine dynamic fluid flow activity with substantial confidence.

**Table 3**

Approximation values of  $Re_x^{1/2} C_f$  by certain values of  $\lambda$  when  $\varepsilon = M = \delta = S = \phi_1 = \phi_2 = 0$

$\lambda$	Present result		Turkyilmazoglu <i>et al.</i> , [28]		Bhattacharyya [39]	
	First solution	First solution	First solution	Second solution	First solution	Second solution
-0.25	1.4022408	-	1.4022408	-	1.4022405	-
-0.50	1.4956698	-	1.4956670	-	1.4956697	-
-0.75	1.4892982	-	1.4892982	-	1.4892981	-
-1.00	1.3288169	0.0000000	1.3288168	0.0000000	1.3288169	0.0000000
-1.15	1.0822312	0.1167021	1.0822312	0.1167021	1.0822316	0.1167023
-1.20	0.9324733	0.2336497	0.9324733	0.2336497	0.9324728	0.2336491
-1.2465	0.5842817	0.5542962	0.5842813	0.5542947	0.5842915	0.5542856
-1.24657	0.5745257	0.5640125	0.5774525	0.5640081	0.5745268	0.5639987

The preparation of compatible conventional/hybrid nanofluids is the crucial element for measuring nanofluids' flow behaviour and the efficiency of heat transfer. The  $Al_2O_3-Cu/H_2O$  hybrid nanofluid is selected as the working fluid because of the outstanding work of Suresh *et al.*, [40] in developing an exploration practice to scrutinise the  $Al_2O_3-Cu/H_2O$  thermophysical properties. In another study, Suresh *et al.*, [41] performed the synthesis of  $Al_2O_3-Cu/H_2O$  nanocomposite powder and its characteristics for various volume concentrations. In their noteworthy findings, nanofluid stability is observed to decrease as volume concentration increases. Further, according to Arifin *et al.*, [42], the development of stable nanofluids was to optimise the thermal properties of operating fluids with the minimal use of nanoparticles. In this study, a distinct set of values for  $\phi_2$  is implemented ( $0.00 \leq \phi_2 \leq 0.02$ ), while  $\phi_1$  is fixed at 0.01. On another point, different values of the limiting parameters are defined to the preceding scope;  $-2.0 \leq \varepsilon \leq -6.0$ ,  $5.0 \leq S \leq 7.0$ , and  $0.5 \leq \delta \leq 2.5$  ensure the consistency of the solutions obtained. Since there is no experimental evidence exist, the choice of parameter values was determined by the values selected from previous researchers to ensure the establishment of the dual solutions [28]. Meanwhile, the range values for  $\phi_1 = 0.01$ , and  $0.00 \leq \phi_2 \leq 0.02$  in this study is selected based on the experimental work done by Suresh *et al.*, [41], who conducted the synthesis, characterisation of  $Al_2O_3-Cu$ /water nanocomposite powder for different volume concentrations 0.1%, 0.33%, 0.75%, 1%, and 2%. In his valuable study, the stability of the prepared nanofluids was determined by measuring the pH of the nanofluids and the nanofluid stability was found to diminish with increasing volume concentration. The values of  $M = 6.0$  is used based on the work done by Turkyilmazoglu *et al.*, [28] to ensure the existence of the dual solution while  $Pr = 6.2$  is implemented so that the results are compatible with the water-based nanofluid [11-12].

The `bvp4c` function in the MATLAB programming is utilised in this research work to solve the governing Eq. (7) and Eq. (8) along with the boundary conditions (9). The above-proposed approach is a significant technique for tackling the boundary value issues that were thoroughly defined by numerous scholars. In order to accomplish the necessary solution, a suitable preliminary estimation

and the boundary layer thickness,  $\eta_\infty$  shall be appointed according to the values of the mentioned parameter. Generally, this analysis aims to investigate the input parameter impact, including the unsteadiness parameter ( $\varepsilon$ ), the suction parameter ( $S$ ), and the heat generation/absorption parameter ( $\delta$ ) over the physical quantities of interest. The present research also focused on identifying more than one solution which exists in the system of equations. From the generated results, the non-uniqueness (dual) solutions are perceived to a particular range of  $\lambda_c$ , reflecting the meeting point of dual solutions or referred to a critical point. It is noticed that the dual solutions are seen in Figure 2 to Figure 9 as the sheet shrinks ( $\lambda < 0$ ), while only a single solution can be noticed as the sheet stretches ( $\lambda > 0$ ).

The influence of  $\varepsilon$  is presented in Figure 2 to Figure 5. The skin friction coefficient ( $f''(0)$ ) of  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid ( $\phi_1 = \phi_2 = 0.01$ ) past a shrinking surface along with the heat transfer rate ( $-\theta'(0)$ ) is accessible in Figure 2 and Figure 3. Figure 2 establishes that the reduction in  $\varepsilon$  worsens  $f''(0)$ , meanwhile, the addition of  $\varepsilon$  triggers the viscosity of the working fluid to accelerate whilst the sheet is shrinking. This essentially increases the velocity of the fluid past the shrinking surface, as seen in Figure 4. The profile of velocity,  $f'(\eta)$  (see Figure 4) discloses that the thickness of the momentum boundary layer is decreased proportionally to the  $\varepsilon$ . This enhances the velocity gradient as the fluid density increases. As  $f''(0)$  declines, the finding indicates that the frictional drag applied on the unsteady  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid flow is declined toward the shrinking sheet, which can restrict separation of the boundary layer flow. In the meantime, Figure 3 illustrates a declining trend of  $-\theta'(0)$  when the values of  $\varepsilon$  decreases in both solutions, and this indicates that the heat transfer efficiency decreases in  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid. This discovery helps to defend the fact that the appearance of  $\varepsilon$  hypothetically reduces the heat transfer performance in  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid. On the other note, the temperature profiles  $\theta(\eta)$  in Figure 5 demonstrates the reduction in the temperature of  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid. The decrease in the temperature of hybrid nanofluid lessens the conductivity of heat. We understand that the occurrence of unsteady flow and the adoption of assorted parameters may trigger this behaviour. The unsteady parameter may enforce any sum of heat flow in the regulating framework, ultimately aggravating the heat transfer mechanism. Overall, both profiles, i.e.,  $f'(\eta)$  and  $\theta(\eta)$ , asymptotically fulfilled the far-field boundary conditions (9) when  $\eta_\infty = 6$  is executed.

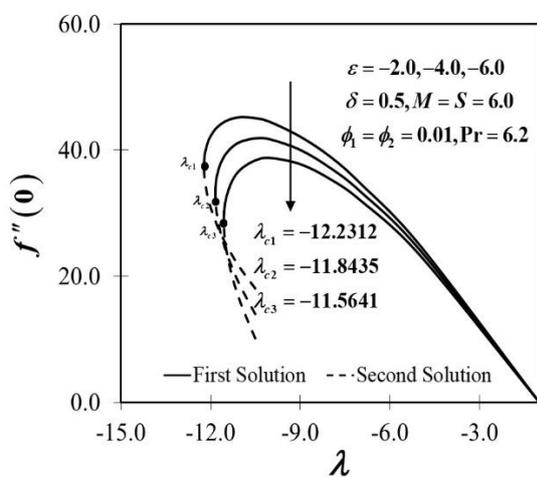


Fig. 2.  $f''(0)$  against  $\lambda$  by various  $\varepsilon$

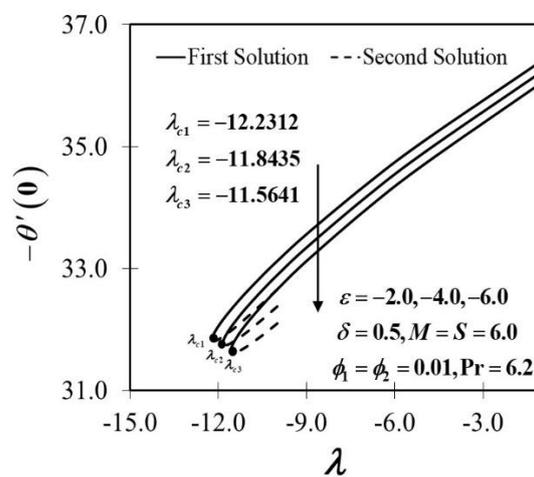


Fig. 3.  $-\theta'(0)$  against  $\lambda$  by various  $\varepsilon$

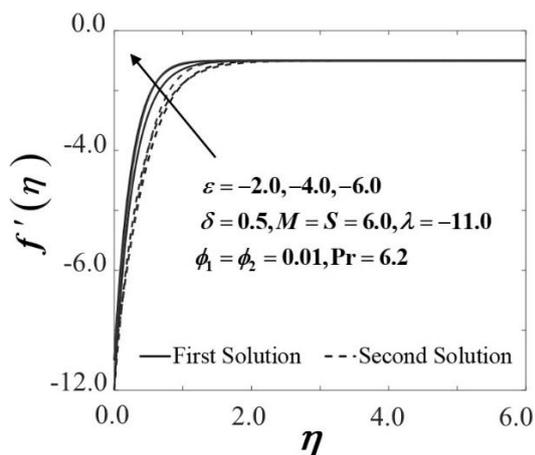


Fig. 4.  $f'(\eta)$  with  $\lambda = -11.0$

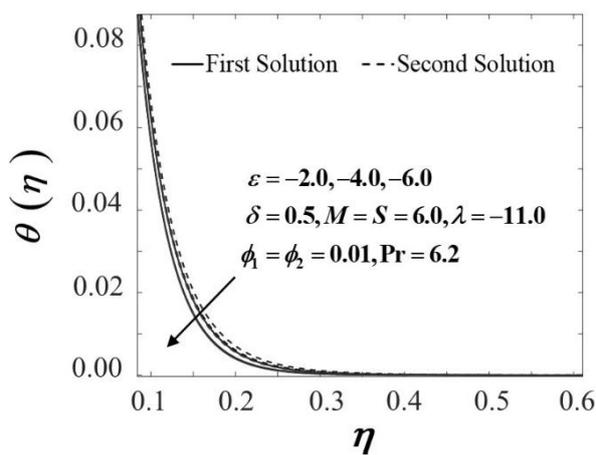


Fig. 5.  $\theta(\eta)$  with  $\lambda = -11.0$

Figure 6 and Figure 7 demonstrate the impact of  $S$  toward  $\lambda$  as the suction values are varied. The hybrid  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  nanofluid behaviour is depicted in Figure 6 concerning the skin friction coefficient,  $f''(0)$  as the sheet shrinks. Figure 6 captures that both solutions depicted an improvement in  $f''(0)$  as  $S$  increased. The existence of suction on a permeable surface will potentially promote stabilisation of the boundary layer. Also, the suction reduces the pressure on the bodies, thereby magnifying the velocity gradient. Moreover, according to the generated results in Figure 7,  $-\theta'(0)$  is amplified in the first and second solution, which is proportional to the rate of heat transfer when  $S$  increases. Realise that the suction effect permits  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid molecules to occupy the surface and then physically improve the heat transfer rate at the permeable surface. From the current and existing evidence, the authors may conclude that the suction parameter greatly facilitates heat transfer improvement.

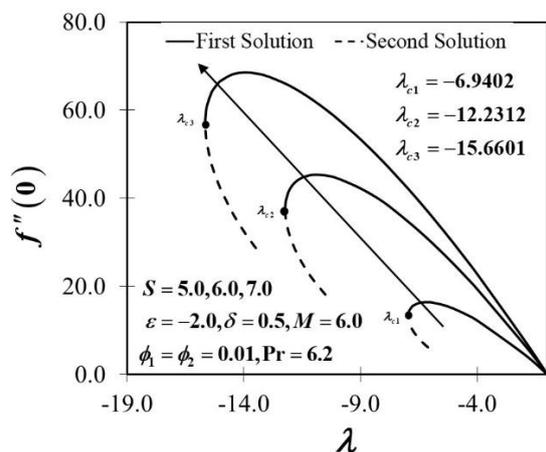


Fig. 6.  $f''(0)$  against  $\lambda$  by various  $S$

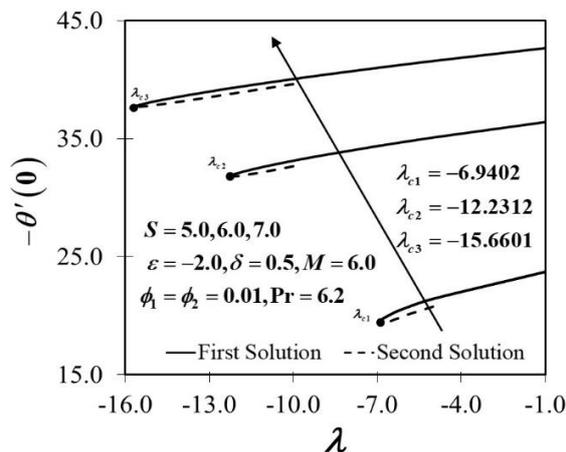


Fig. 7.  $-\theta'(0)$  against  $\lambda$  by various  $S$

Figure 8 and Figure 9 are prepared to reveal the effect of  $\delta$  in relation to  $\lambda$  when  $\delta = 0.5, 1.5, 2.5$  which represents the heat generation influences toward the shrinking surface. Figure 8 highlights that as  $\delta$  increase,  $-\theta'(0)$  decreases in  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid. Physically, the additional heat provided to the  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid triggers temperature to rise, thereby reducing the efficiency of heat transfer. On the other note, the temperature profiles  $\theta(\eta)$  in Figure 9 support the trend seen in Figure 8, which demonstrates the changes in temperature of the  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$

hybrid nanofluid. The increase in the heat generation parameter allows the thermal layer thickness and thermal gradient to increase because energy is generated at the thermal boundary layer.

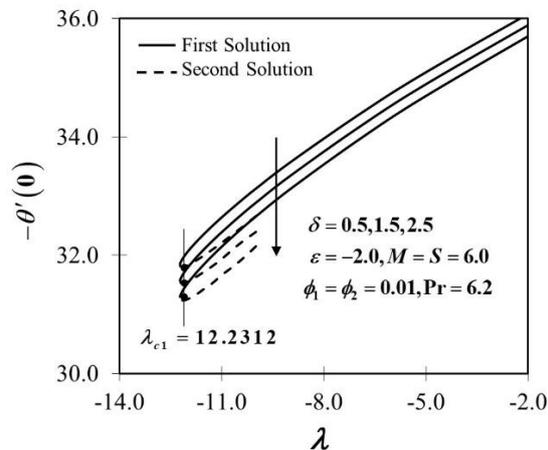


Fig. 8.  $-\theta'(0)$  with  $\delta = 0.5, 1.5, 2.5$

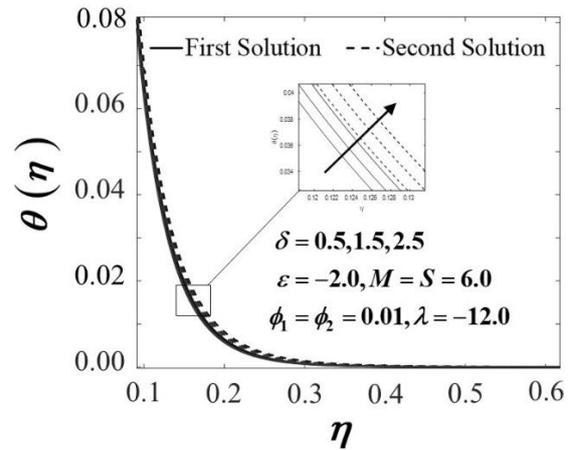


Fig. 9.  $\theta(\eta)$  with  $\delta = 0.5, 1.5, 2.5$

#### 4. Conclusion

The current study reflects the impact of suction and unsteadiness parameters in  $\text{Al}_2\text{O}_3\text{-Cu}/\text{H}_2\text{O}$  hybrid nanofluid with heat generation/absorption. The numerical results for the skin friction coefficient and the local Nusselt number are deduced with the aid of bvp4c features in the MATLAB package. A decrease in the unsteadiness parameter reduces the skin friction coefficient over the shrinking permeable sheet. The findings of the local Nusselt number suggest that the unsteadiness parameter greatly facilitates the degradation of heat transfer. Further, the rise in the suction parameter encourages stabilisation of the boundary layer and increases thermal efficiency as well. The inclusion of heat generation/absorption in the operating fluid generates a greater temperature profile, which reduces the heat transfer performance.

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